

REVIEWED FOR COMPLIANCE WITH THE ONTARIO BUILDING CODE AND THE APPLICABLE ZONING BY-LAW

20.130122.000.00.CM

LAMPONE INVESTMENT INCONSTRUCTION SHALL COMPLY WITH THE ONTARIO BUILDING CODE.

CITY OF MARKHAM

FLOOR JOISTS SHOP DRAWINGS

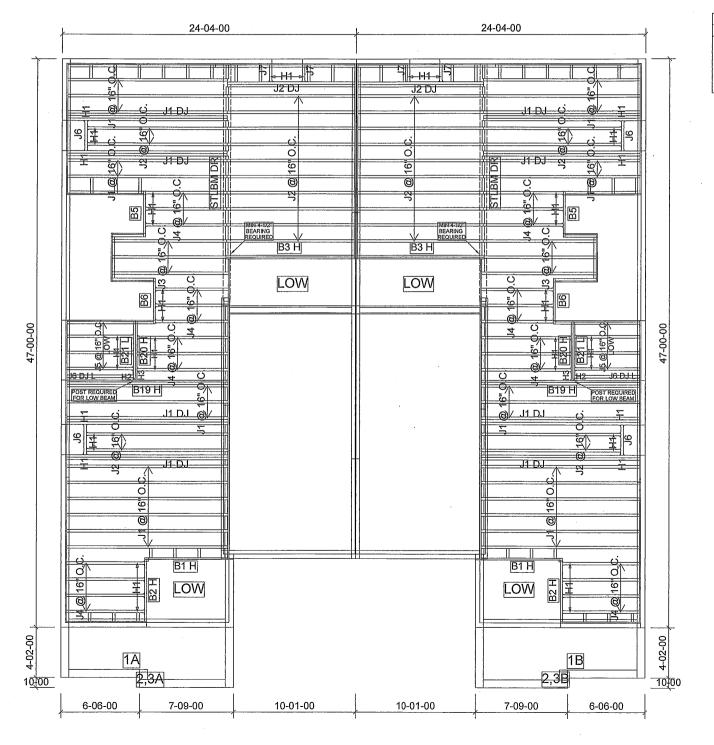
MODEL NAME: PEYTON 3

ELEV 1A, 1B, 2, 3A & 3B

		1A,2,3A			
PlotID	Length	Product	Plies	Net Qty	Fab Type
J1	14-00-00	9 1/2" NI-40x	1	14	MFD
J1 DJ	14-00-00	9 1/2" NI-40x	2	8	MFD
J2	12-00-00	9 1/2" NI-40x	1	14	MFD
J2 DJ	12-00-00	9 1/2" NI-40x	2	2	MFD
J3	10-00-00	9 1/2" NI-40x	1	3	MFD
]4	8-00-00	9 1/2" NI-40x	1	13	MFD
J5	6-00-00	9 1/2" NI-40x	1	4	MFD
J6 DJ L	6-00-00	9 1/2" NI-40x	2	2	MFD
J6	4-00-00	9 1/2" NI-40x	1	2	MFD
J7	2-00-00	9 1/2" NI-40x	1	2	MFD
B19 H	14-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B3 H	12-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2	MFD
B1 H	8-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B2 H	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B20 H	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B21 L	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B5	4-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B6	4-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD

		1B,2,3B			
PlotID	Length	Product	Plies	Net Qty	Fab Type
J1	14-00-00	9 1/2" NI-40x	1	14	MFD
J1 DJ	14-00-00	9 1/2" NI-40x	2	8	MFD
J2	12-00-00	9 1/2" NI-40x	1	14	MFD
J2 DJ	12-00-00	9 1/2" NI-40x	2	2	MFD
J3	10-00-00	9 1/2" NI-40x	1	3	MFD
34	8-00-00	9 1/2" NI-40x	1	13	MFD
J5	6-00-00	9 1/2" NI-40x	1	4	MFD
J6 DJ L	6-00-00	9 1/2" NI-40x	2	2	MFD
J6	4-00-00	9 1/2" NI-40x	1	2	MFD
J7	2-00-00	9 1/2" NI-40x	1	2	MFD
B19 H	14-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B3 H	12-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2	MFD
B1 H	8-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B2 H	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B20 H	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B21 L	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	.1	1	MFD
B5	4-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B6	4-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD

	1A,2	2,3A
Qty	Manuf	Product
16	H1	IUS2.56/9.5
6	H1	IUS2.56/9.5
4	H1	IUS2.56/9.5
1	H2	HU310-2
1	Н3	HUS1.81/10



	1B,2,3B				
Qty	Manuf	Product			
16	H1	IUS2.56/9.5			
6	H1	IUS2.56/9.5			
4	H1	IUS2.56/9.5			
1	H2	HU310-2			
1	H3	HUS1.81/10			



BUILDER: GREENPARK HOMES

SITE: LAMPONE INVESTMENTS

MODEL: PEYTON 3

ELEVATION: 1,2,3

LOT:

CITY: MARKHAM

SALESMAN: WILL GARCIA

DESIGNER: L.D. REVISION: L.D.

NOTES:

REFER TO THE **NORDIC INSTALLATION**GUIDE FOR PROPER STORAGE AND

INSTALLATION.

SQUASH BLOCKS OF 2x4, 2x6, 2x8 #2 S.P.F.
REQ'D UNDER INTERIOR UNIFORM LOAD
BEARING WALLS. MULTIPLE SQUASH
BLOCKS REQ'D UNDER CONCENTRATED
LOADS. SEE FIGURE 1. CANTILEVERED
JOISTS INCLUDING CANT' OVER BRICK REC
I-JOIST BLOCKING ALONG BEARING AND
RIMBOARD CLOSURE AT ENDS. SEE
FIGURES 4 & 5 FOR REINFORCEMENT
REQUIREMENTS. FOR HOLES INCLUDING
DUCT CHASE AND FIELD CUT OPENINGS
SEE FIGURE 7, TABLES 1 & 2. CERAMIC TIL
APPLICATION AS PER O.B.C 9.30.6.

LOADING:

DESIGN LOADS: L/480.000 LIVE LOAD: 40.0 lb/ft² DEAD LOAD: 15.0 lb/ft² TILE LOAD: 20.0 lb/ft²

SUBFLOOR: 3/4" GLUED AND NAILED

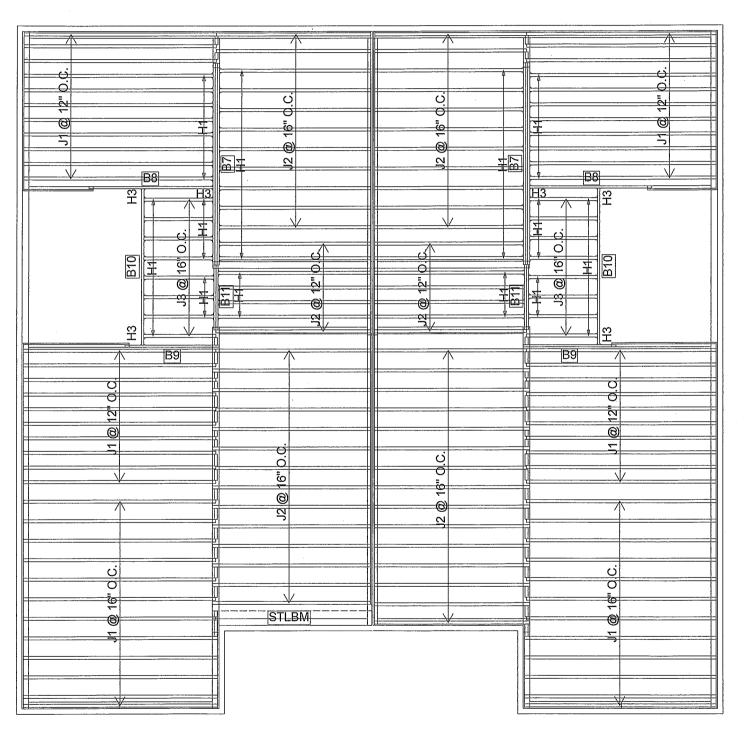
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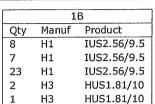
1st FLOOR

1A						
PlotID	Length	Product	Plies	Net Qty	Fab Type	
J1	14-00-00	9 1/2" NI-40x	1	33	MFD	
J2	12-00-00	9 1/2" NI-40x	1	32	MFD	
J3	6-00-00	9 1/2" NI-40x	1	8	MFD	
B7	14-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	3	3	MFD	
B10	12-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
B8	10-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
B9	8-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
B11	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2	MFD	

1B						
PlotID	Length	Product	Plies	Net Qty	Fab Type	
J1	14-00-00	9 1/2" NI-40x	1	33	MFD	
J2	12-00-00	9 1/2" NI-40x	1	32	MFD	
J3	6-00-00	9 1/2" NI-40x	1	8	MFD.	
В7	14-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	3	3	MFD	
B10	12-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
В8	10-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
В9	8-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
B11	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2	MFD	

ĺ		1	A
	Qty	Manuf	Product
	8	H1	IUS2.56/9.5
	7	H1	IUS2.56/9.5
	23	H1	IUS2.56/9.5
	2	Н3	HUS1.81/10
	1	НЗ	HUS1.81/10







BUILDER: GREENPARK HOMES

SITE: LAMPONE INVESTMENTS

MODEL: PEYTON 3

ELEVATION: 1

LOT:

CITY: MARKHAM

SALESMAN: WILL GARCIA

DESIGNER: L.D. REVISION: L.D.

NOTES:

REFER TO THE NORDIC INSTALLATION **GUIDE** FOR PROPER STORAGE AND INSTALLATION. **SQUASH BLOCKS** OF 2x4, 2x6, 2x8 #2 S.P.F. REQ'D UNDER INTERIOR UNIFORM LOAD BEARING WALLS. MULTIPL SQUASH BLOCKS REQ'D UNDER CONCENTRATED LOADS, SEE FIGURE 1. CANTILEVERED JOISTS INCLUDING CANT' OVER BRICK REQ. I-JOIST BLOCKING ALON BEARING AND RIMBOARD CLOSURE AT ENDS. SEE FIGURE 7 TABLES 4 & 5 FOR REINFORCEMENT REQUIREMENTS. FOR HOLES INCLUDING DUCT CHASE AND FIEL **CUT OPENINGS** SEE FIGURE 7 TABLES 1 & OF THE INSTALLATION GUIDE. CERAMIC TI APPLICATION AS PER O.B.C. 9.30.6

LOADING:

DESIGN LOADS: L/480.000 LIVE LOAD: 40.0 lb/ft² DEAD LOAD: 15.0 lb/ft² TILE LOAD: 20.0 lb/ft²

SUBFLOOR: 5/8" GLUED AND NAILED

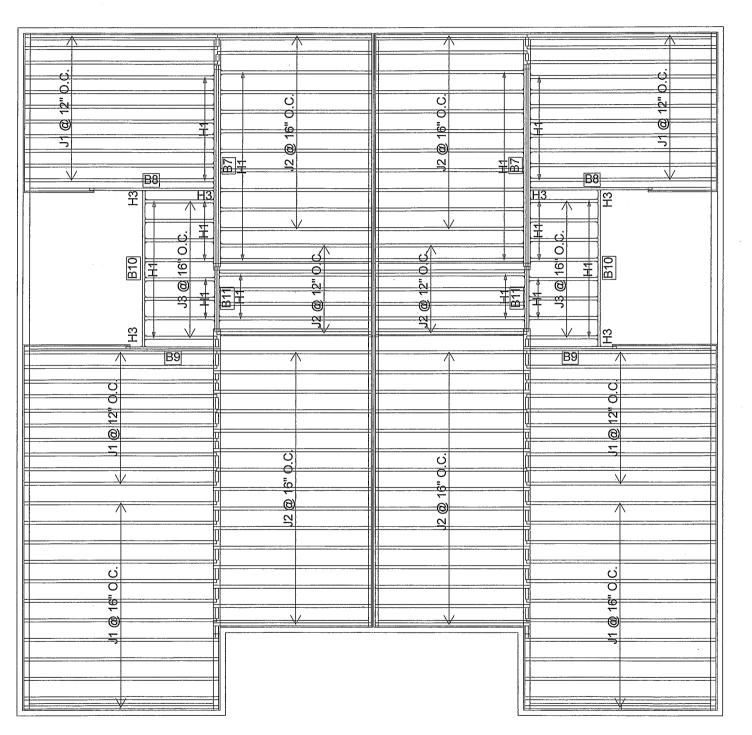
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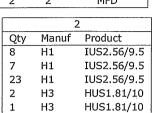
2nd FLOOR

2						
PlotID	Length	Product	Plies	Net Qty	Fab Type	
J1	14-00-00	9 1/2" NI-40x	1	33	MFD	
J2	12-00-00	9 1/2" NI-40x	1	32	MFD	
J3	6-00-00	9 1/2" NI-40x	1	8	MFD	
B7	14-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	3	3	MFD	
B10	12-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
B8	10-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
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B11	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2	MFD	

		2 .			
PlotID	Length	Product	Plies	Net Qty	Fab Type
J1	14-00-00	9 1/2" NI-40x	1	33	MFD
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B10	12-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
В8	10-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
В9	8-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD
B11	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2	MFD

	2	2
Qty	Manuf	Product
8	H1	IUS2.56/9.5
7	H1	IUS2.56/9.5
23	H1	IUS2.56/9.5
2	H3	HUS1.81/10
1	Н3	HUS1.81/10







BUILDER: GREENPARK HOMES

SITE: LAMPONE INVESTMENTS

MODEL: PEYTON 3

ELEVATION: 2

LOT:

CITY: MARKHAM

SALESMAN: WILL GARCIA

DESIGNER: L.D. **REVISION:** L.D.

NOTES:

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SUBFLOOR: 5/8" GLUED AND NAILED

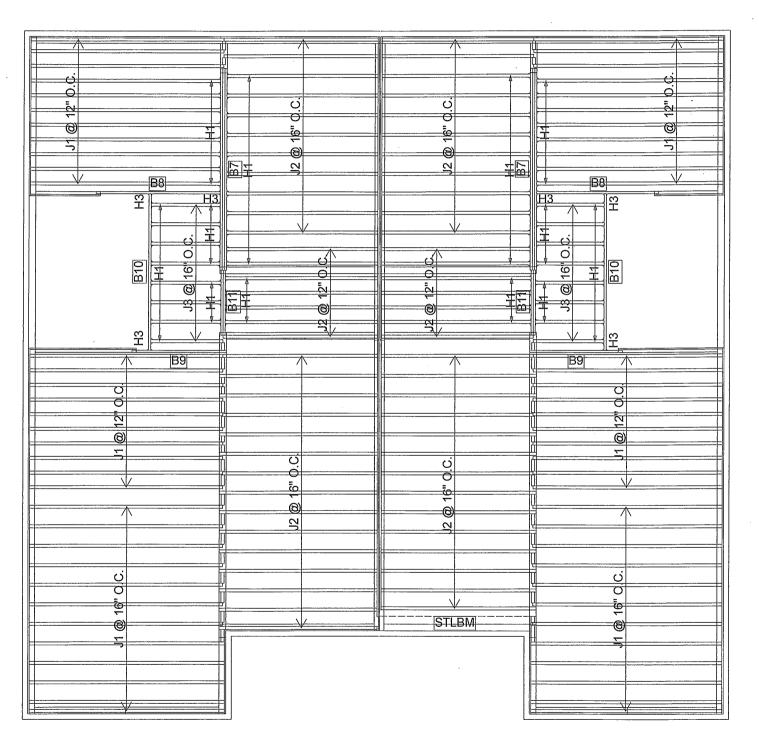
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2nd FLOOR

3A						
PlotID	Length	Product	Plies	Net Qty	Fab Type	
J1	14-00-00	9 1/2" NI-40x	1	33	MFD	
J2	12-00-00	9 1/2" NI-40x	1	32	MFD	
J3	6-00-00	9 1/2" NI-40x	1	8	MFD	
B7	14-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	3	3	MFD	
B10	12-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
B8	10-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
B9	8-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD	
B11	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2	MFD	

ЗВ							
PlotID	Length	Product	Plies	Net Qty	Fab Type		
J1	14-00-00	9 1/2" NI-40x	1	33	MFD		
J2	12-00-00	9 1/2" NI-40x	1	32	MFD		
J3 ·	6-00-00	9 1/2" NI-40x	1	8	MFD		
B7	14-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	3	3	MFD		
B10	12-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD		
B8	10-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1	MFD		
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B11	6-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2	MFD		

		3	Δ
	Qty	Manuf	Product
ĺ	8	H1	IUS2.56/9.5
	7	H1	IUS2.56/9.5
	23	H1	IUS2.56/9.5
	2	НЗ	HUS1.81/10
	1	Н3	HUS1.81/10



	3	В
Qty	Manuf	Product
8	H1	IUS2.56/9.5
7	H1	IUS2.56/9.5
23	· H1	IUS2.56/9.5
2	H3	HUS1.81/10
1	Н3	HUS1.81/10



BUILDER: GREENPARK HOMES

SITE: LAMPONE INVESTMENTS

MODEL: PEYTON 3

ELEVATION: 3

LOT:

CITY: MARKHAM

SALESMAN: WILL GARCIA

DESIGNER: L.D. **REVISION:** L.D.

NOTES:

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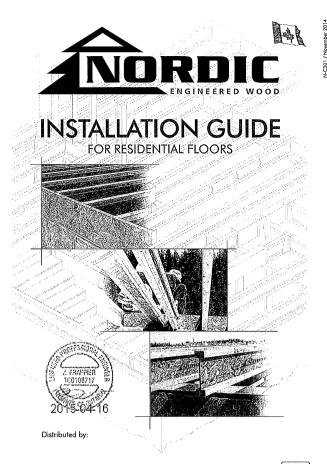
LOADING:

DESIGN LOADS: L/480.000 LIVE LOAD: 40.0 lb/ft² DEAD LOAD: 15.0 lb/ft² TILE LOAD: 20.0 lb/ft²

SUBFLOOR: 5/8" GLUED AND NAILED

DATE: 2020-07-29

2nd FLOOR



SAFETY AND CONSTRUCTION PRECAUTIONS



Do not walk on 1-joists until fully fastened and braced, or serious inju-



Never stack building unsheathed I-joists.
Once sheathed, do not

I-joists are not stable until completely installed, and will not carry any load until full braced and sheathed. Avoid Accidents by Following these Important Guidelines

 Brace and nail each I-joist as it is installed, using hangers, blocking panels, rim board, and/or cross-bridging at joist ands. When I-joists are applied confinuous over interior supports and a load-bearing wall is planned at that location, blocking will be required at the interior support. When the building is completed, the floor sheathing will provide lateral support for the top flanges of the Lipists. Until this sheathing is applied, temporary bracing, often called struts, or temporary sheathing must be opp to prevent Lipist rollover or buckling.

- Temporary bracing or struts must be 1x4 inch minimum, at least 8 feet long and spaced no more than 8 feet on centre, and must be secured with a minimum of two 2-1/2" nails festend to the top surface of each I-pists. No
- Or, shoothing (temporary or permanent) can be nailed to the top flange of the first 4 feet of l-joists at the end of the boy.
- For cantilevered I-joists, brace top and bottom flanges, and brace ends with closure panels, rim board, or cross-bridging.
- 4. Install and fully nail permanent sheathing to each I-joist before placing loads on the floor system. Then, stack building materials over beams or walls only. 5. Never install a damaged I-joist.

Improper storage or installation, failure to follow applicable building codes, failure to follow span ratings for Nordic I-joists, failure to follow allowable hole sizes and locations, or failure to use web stiffeners when required can result in serious accidents. Follow these installation guidelines carefully.

MAXIMUM FLOOR SPANS

- Maximum clear spans applicable to simple-span or multiple-span residential floor construction with a design live load of 40 pcf and dead load of 15 pcf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The servicability limit states include the consideration for floor vibration and a live load deflection limit of 1/480. For multiple-span applications, the end spans shall be 40% or more of the adjacent span.
- On more of the acqueent spain.

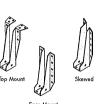
 Spans are based on a composite floor with glued-nailed oriented strand board (CSB) sheathing with a minimum thickness of 5/8 linch for a joist spacing of 19-2 linches or less, or 3/4 inch for joist spacing of 24 inches. Adhesive shall meet the requirements given in CGBS-71.26
 Standard. No concrete topping or bridging element was assumed. Increased spans may be achieved with the used of gypsum and/or a row of blocking at mid-span.
- Minimum bearing length shall be 1-3/4 inches for the end bearings, and 3-1/2 inches for the intermediate bearings.
- Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.
- This span chart is based on uniform loads. For applications with other than uniform loads, an engineering analysis may be required based on the use of the design properties.
- 6. Tables are based on Limit States Design per CAN/CSA O86-09 Standard, and NBC 2010.
- 7. SI units conversion: 1 inch = 25.4 mm 1 foot = 0.305 m

MAXIMUM FLOOD SPANS FOR NORDIC I. IOISTS SIMPLE AND MULTIPLE SPANS

2000000	ENG-22 (1990)	T. C. S.			30.500 400 800	SPECIAL STATE		11.00	(2000)343
Joist Depth	Joist Series		On centre	spacing			On centre	spacing	
		12*	16"	19.2	24	12	16"	19.2	245
	NI-20	15'-1"	14'-2	13'-9'	13'-5	16'-3'	15'-4	14'-10	14'-7
	NI-40x -	16'-1"	15'-2'	14'-8"	14'-9"	17'-5"	16'-5"	15'-10"	15'-5"
9-1/2	NJ-60	16'-3"	15'-4'	14-10	14'-11'	17'-7'	16'-7"	16'-0"	16'-1"
	NI-70	17'-1"	16'-1"	15'-6"	15'-7"	18'-7'	17'-4"	16'-9"	16'-10"
100	NI-80	17'-3"	16'-3"	15'-8"	15'-9"	18'-10"	17'-6"	16'-11'	17'-0"
art of a feet	NI-20	16'-11"	16'-0'	15'-5	15'-6"	18'-4	17'-3"	16'-8	16'-7"
3000	NI-40x	18'-1	17'-0"	16'-5	16'-6"	20'-0	18'-6"	17'-9	17'-7"
1.75 pt 7	NI-60	18'-4"	17'-3"	16'-7"	16'-9"	20'-3"	18'-9"	18'-0"	18'-1"
11-7/8*	NI-70	19'-6"	18'-0"	17'-4"	17'-5"	21'-6"	19'-11'	19'-0"	19'-1"
400	NI-80	19'-9"	18'-3'	17'-6"	17'-7"	21'-9*	20'-2"	19'-3"	19'-4"
10 7 6	NI-90	20'-2*	18'-7	17'-10	17'-11"	22'-3"	20'-7	19'-8"	19'-9
1000	NI-90x	20'-4"	18'-9	17:-11"	18'-0	22'-5"	20'-9	19'-10"	19'-11'
1485 (118)	NI-40x	20'-1"	18'-7"	17'-10"	17'-11"	22'-2"	20'-6"	19'-8"	19'-4"
	NI-60	20'-5"	18'-11"	18'-1"	18'-2"	22'-7'	20'-11"	20'-0"	20'-1"
	NI-70	21'-7"	20'-0"	19'-1"	19'-2'	23'-10"	22'-1"	21'-1"	21'-2"
14"	NI-80	21'-11"	20'-3"	19'-4"	19'-5"	24'-3'	22'-5"	21'-5"	21'-6"
THE PERSON	NI-90	22'-5	20'-8"	19'-9	19'-10'	24'-9-	22'-10"	21'-10"	21'-10'
1757 / 186	NI-90x	22'-7'	20'-11"	19'-11"	20'-0"	25'-0"	23'-1"	22'-0"	22'-2"
191. W	NI-60	22'-3'	20'-8"	19'-9'	19'-10'	24'-7"	22'-9"	21'-9"	21'-10"
400	NI-70	23'-6"	21'-9"	20'-9"	20'-10'	26'-0"	24'-0"	22'-11'	23'-0"
16"	NI-80	23'-11	22'-1"	21'-1'	21'-2'	26'-5*	24'-5"	23'-3"	23'-4"
Mark V	NI-90	24'-5"	22'-6	21'-5'	21'-6	26'-11"	24'-10"	23'-9"	231-9
124 (28.5)	NI-90x	24'-8"	22'-9"	21'-9"	21-10	27'-3"	25'-2"	24'-0"	24'-1'

I-JOIST HANGERS

- Hangers shown illustrate the three most commonly used metal hangers to support I-joists.
 - 2. All nailing must meet the hanger
- Hangers should be selected based on the joist depth, flange width and load capacity based on the maximum spans.
- Web stiffeners are required when the sides of the hangers do not laterally brace the top flange of the I-joist.



CCMC EVALUATION REPORT 13032-P

STORAGE AND HANDLING GUIDELINES

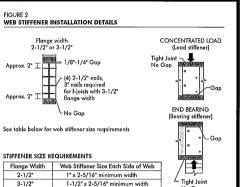
- 1. Bundle wrap can be slippery when wet. Avoid walking on wrapped
- 2. Store, stack, and handle I-joists vertically and level only. 3. Always stack and handle 1-joists in the upright position only. --
- 4. Do not store I-joists in direct contact with the ground and/or flatwise.
- 5. Protect I-joists from weather, and use spacers to separate bundles. 6. Bundled units should be kept intact until time of installation.
- 7. When handling I-joists with a crane on the job site, take a few simple precautions to prevent damage to the I-joists and injury
- Pick I-joists in bundles as shipped by the supplier
- Orient the bundles so that the webs of the I-joists are vertical.
- Pick the bundles at the 5th points, using a spreader bar if necessary.
- 8. Do not handle l-joists in a horizontal orientation.
- 9. NEVER USE OR TRY TO REPAIR A DAMAGED I-JOIST.

WEB STIFFENERS

- A bearing stiffener is required in all engineered applications with factored reactions greater than shown in the l-joist properties table found of the *l-joist* Construction Guide (1010). The gap betwee the stiffener and the flange is at the top.
- A bearing stiffener is required when sides of the hanger do not extend up to, and support, the top flange. The gap between the stiffener and flange is at the top.
- smeere and longe is a time long.

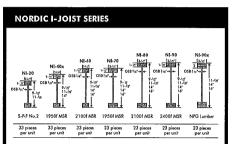
 **A load stiffener is required at localions where a factored concentrated load greater than 2,370 lbs is applied to the top flang between supports, or in the case of a contillever, anywhere between the contillever tip and the support. These values are for standard term load duration, and may be adjusted for other load durations as permit by the code, the gap between the stiffener and the flange is at the bottom.

(1e)



(1g)

2-1/2" nails at -



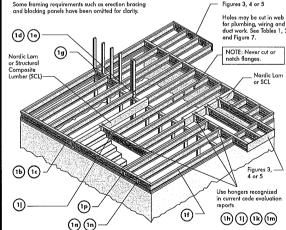
Chantiers Chibougamau Ltd. harvests its own trees, which enables Nazdic

nantiers Chibougamau roducts to adhere to strict quality controt proving the control p 2015-04-16

INSTALLING NORDIC I-JOISTS

- 1. Before laying out floor system components, verify that I-joist flange widths match hanger widths. If not, continued 2. Except for cutting to length, I-joist flanges should never be cut, drilled, or notched.
- 3. Install I-joists so that top and bottom flanges are within 1/2 inch of true vertical alignment.
- 4. I-joists must be anchored securely to supports before floor sheathing is attached, and supports to be level.
- 5. Minimum bearing lengths: 1-3/4 inches for end bearings and 3-1/2 inches for intermediate bearings 2015-04-16 6. When using hangers, seat 1-joists firmly in hanger bottoms to minimize settlement.
- 7. Leave a 1/16-inch gap between the 1-joist end and a header. 8. Concentrated loads greater than those that can normally be expected in residential construction should only be applied to the top surface of the top flonge. Normal concentrate loads include track lighting fixtures, audio equipment and security cameras. Never suspend unusual or heavy loads from the I-joist's bottom flonge. Whenever possible, suspend all concentrated loads from the top of the I-joist, Or, attach the load to blocking that has been securely fastened to the I-joist was the concentrated loads from the top of the I-joist of the I-joist was the concentrated loads from the top of the I-joist. Or, attach the load to blocking that has been securely fastened to the I-joist was the I-Jo
- 9. Never install I-joists where they will be permanently exposed to weather, or where they will remain in direct contact with
- 10. Restrain ends of floor joists to prevent rollover. Use rim board, rim joists or I-joist blocking panels.
- 11. For I-joists installed over and beneath bearing walls, use full depth blocking panels, rim board, or squash blocks (cripple members) to transfer gravity loads through the floor system to the wall or foundation below. 12. Due to shrinkage, common framing lumber set on edge may never be used as blocking or rim boards. I-joist blocking panels or other engineered wood products – such as rim board – must be cut to fit between the I-joists, and an I-joists-compatible depth selected.
- 13. Provide permanent lateral support of the bottom flange of all Lipists at interior supports of multiple-span joists. Similarly, support the bottom flange of all contilevered Lipists at the end support next to the contilever extension. In the completed structure, the gypsum valiboard ceiling provides this lateral support. Until the final finished ceiling is applied, temporary bracing or strukts must be used.
- 15. Nail spacing: Space nails installed to the flange's top face in accordance with the applicable building code require approved building plans.

TYPICAL NORDIC I-JOIST FLOOR FRAMING AND CONSTRUCTION DETAILS

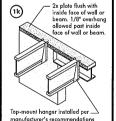


All nails shown in the above details are assumed to be common wire nails unless otherwise noted. 3° (0.122° dia) common spiral nails may be substituted for 2-1/2° (0.128° dia) common wire nails. Framing lumber assumed to be Spruce-Tinne-Tin No. 2 or better. Individual components not shown to scale for daring

Transfer load from above to bearing below. Install squas blocks per detail 1d. Match Rim board may be used in lieu of I-joists. Backer is not required when rim board is used. Bracing per code shall be carried to the foundation. bearing area of blocks below to post above. (1)

Top- or face-mount hanger -installed per manufacturer's For nailing schedules for multiple beams, see the manufacturer's

Note: Unless hanger sides laterally support the top flange, bearing stiffeners shall be used.



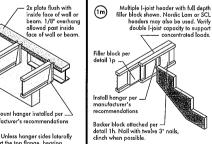
3-1/2"

Use single I-joist for loads up to 3,300 plf, double I-joists for loads up to 6,600 plf (filler block not

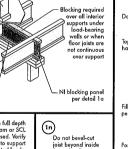
Note: Unless hanger sides laterally support the top flange, bearing stiffeners shall be used.

1. Support back of I-joist web during nailing to

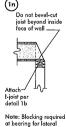
prevent damage to web/flange conn



Maximum support capacity = 1,620 lbs.

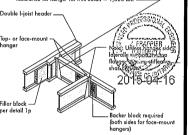


such as offset bearing walls, are no covered by this detail



Note: Blocking required at bearing for lateral support, not shown for clarity.



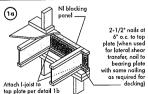


For hanger capacity see hanger manufacturer's recomment Verify double I-joist capacity to support concentrated loads.

BACKER BLOCKS (8locks must be long enough to permit required

Flange Width	Material Thickness Required*	Minimum Depth**
2-1/2*	1"	5-1/2"
3-1/2"	1-1/2"	7-1/4"

- Minimum grade for backer block material shall be S-P.F.No. 2 or better for solid sawn lumber and wood structural panels conforming to CAN/CSA-023's CAN/CSA-043's Standard.
 For face-mouth langers use net joil depth minus 3-1/4' for joists with 1-1/2' thick flanges. For 2' thick flanges use net depth



Blocking Panel Maximum Factored Uniform or Rim Joist Vertical Load* (plf) 3,300 NI Joists

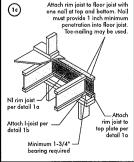
*The uniform vertical load is limited to a joist depth of 16 inches or less and is based on standard term load duratio. It shall not be used in the design of a bending member, such as joist, header, or rafter. For concentrated vertical load transfer, see detail 1d.

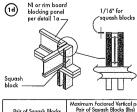


—Attach rim board to top plate using 2-1/2" wire o spiral toe-nails at 6" o.c

Minimum bearing length shall be 1-3/4" for the end bearings, and 3-1/2" for the intermediate bearings when applicable 1-1/8" Rim Board Plus 8,090

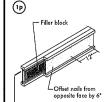
*The uniform vertical load is limited to a rim board depth of 16 inches or less and is based on standard term load duration. It shall not be used in the design of a bending member, such as joist, header, or rafter. For concentrated vertical load transfer, see detail 1d.





Maximum Factored Vertical pe Pair of Squash Blocks (lbs)
 2x Lumber
 5,500
 8,500

 1-1/8* Rim Board Plus
 4,300
 6,600
 ovide lateral bracing per detail 1a, 1b, or 1c

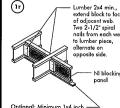


-1/8" to 1/4" gap between top flange and filler block

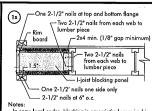
 Filler block is required between joists for full length of span. Nail joists together with two rows of 3" nails at 12 inches o.c. (clinched when possible) on each side of the double I-joist. Total of four nails per foot required. If nails can be clinched, only two nails per foot are required.

The maximum factored load that may be applied to one side of the double joist using this detail is 860 lbf/ft. Verify double 1-joist capacity.

FILLER BLOCK REQUIREMENTS FOR DOUBLE I-JOIST CONSTRUCTION Flange Size Joist Filler Depth Block Size 9-1/2" 11-7/8" 2-1/8" x 6" 2-1/8" x 12" 9-1/2" 11-7/8" 14" 16" 3" x 6" 3" x 8" 3" x 10" 3" x 12" 3-1/2" x



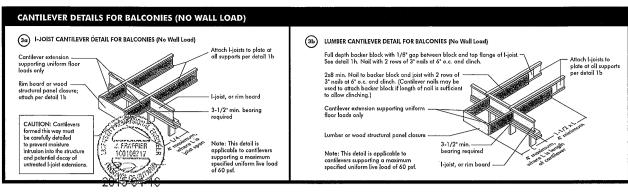
strap applied to underside of joist at blocking line or 1/2 inch minimum gypsum ceiling attached to underside of joists.

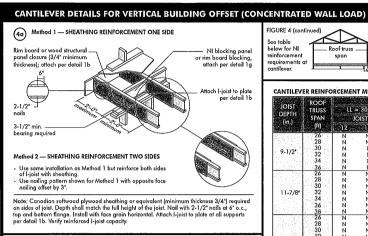


Notes:

- In some local codes, blocking is prescriptively required in the first joist space (or first and second joist space) next to the stater joist. Where required, see local code requiremen for spacing of the blocking.

- All nails are common spiral in this detail.





(4b) Alternate Method 2 — DOUBLE I-JOIST –NI blocking panel or rim board blocking, attach per detail 1g Rim board, or wood structural panel closure (3/4" minimum thickness); attach per detail 1b Face nail two rows of 3" nails at race noil two rows of 3" noils of 12" o.c. each side through one I-joist web and the filler block to other I-joist web. Offset noils from opposite face by 6".

Clinch if possible (four noils per foot required, except two noils per foot two noils per foot to the per foot the per foot to the per foot to the per foot the per foot to the per foot the per foot to the per foot to the per foot the

Block Ljoists together with filler blocks for the full length of the reinforcement.

For Ljoist flange widths greater than 3 inches place an additional row of 3" nails along the centreline of the reinforcing panel from each side. Clinch when possible.

Attach I-joists to top plate at all supports per detail 1b, 3-1/2"

Verify girder joist capacity if the back span exceeds the joist spacing.

Attach double I-joist per detail 1p, if required.

For hip roofs with the jack trusses running parallel to the cantilevered floor joists, the I-joist reinforcement requirements for a span of 26 ft. shall be permitted to be used. FIGURE 4 (continued) Roof trusses Roof truss Roof truss Roof truss Span 2-0* — Roof truss span — Roof truss -span CANTILEVER REINFORCEMENT METHODS ALLOWED

JOIST DEPTH	TRUSS SPAN				pst			DL = 15 CING (in				ŲL = 15 CING (in	
(in.)	(ft)	12						19:2				19.2	
	26	N .	N	1	2	N	1	2	Х	N	2	X	Х
	28	N	N	1	X	N	1	. 2	X	N	2	Х	Х
9-1/2"	30	N	1	1	Х	N	1	2	Х	1	2	Х	Х
′*′′*	32	N	1	2	- X	N	2	Х	Х	- 1	Х	Х	Х
200	34	N	3	2	Х	N	2	Х	Х	- 1	Х	Х	Х
2022	36	N	1	2	X	_1_	2	Х	X	1	X	X	X
0.4-036	26	N	N	N	1	N	N	1	2	N	N	1	2
37.35	28	N	N	N	1	N	N	1	2	N	. !	1	X
	30	N	N	N	ı	N	N	!	2	N	1	2	X
11-7/8	32	N	N	!	i	N	N	!	2	N	. !	2	X
	34	N	N	!	2	N	!	ļ	X	N	!	2	X
	36 38	N	N	!	2	N N	!	2		N N		2	X
114 2 11	26	N N	N N		<u>2</u>	N	N	Z	X	N	<u>2</u>	-	- ^-
	28	N	N		N	l N	N	N	- ;	N	IN.	IN 1	- !
	30	N	N	N ·	N	N	IN N	N	- ;	N N	N M	,	
100	32	N	N	N N	18	l n	N NI	N N	- ; 1	N	N N	,	2
14"	34	N	Ň	N	,	N N	N N	1		N	N	í	2
	36	N	N	N	i i	l 'n	N	,	1	N	ï	í	2
	38	N	N	N	i	l n	Ň	i	2	N	- 1	í	Ý
	40	N	N	N	,	l ii	N	i	2	N	i	ò	Ŷ
1,5000	26	N	N	N	Ń	N	N	Ň	Ñ	N	Ň	Ň	
	28	Ň	Ň	N	·N	l ii	Ñ	Ñ	ïl	N	Ñ	Ň	i
11.7	30	N	Ñ	N	N	l ii	Ñ	N	i l	N	N	N	i
1000	32	N	N	N	N	l ii	Ñ	N	i	N	N	1	i
16'	34	N.	N	N	N	N	N	N	i	N	N	1	2
	36	N	N	N	1	N	N	N	1	N	N	1	2
5 - 17	38	N	N	N	1	N	N	N	1	N	N	1	2
	40	N	N	N	1	N	N	1	2	N	N	1	2
1.00	42	N	N	N	1	N	N	1	2	N	1	1	Х

- 1 = NI reinforced with 3/4" wood structural ganel on one side only.
 2 = NI reinforced with 3/4" wood structural ganel on both sides, or double Ljoist.
 X = Try a desper joist or doner spacing.
 2. Maximum design load shall be: 15 p4 road doud, 55 p4 floor total load, and 80 pfl wall load. Wall load is based on 3'-0" maximum width window or door openings.

. N = No reinforcement required.
1 = NI reinforced with 3/4" wood structural

1 = NI reinforced with 3/4" wood structural panel on one side only.
2 = NI reinforced with 3/4" wood structural panel on both sides, or doubtle 1-joist.
X = Try a deeper joist or closer spacing.
2. Maximum design load shall be: 15 pst roof deed load, 5/5 pst floor total load, and 80 pf wall load. Wall load is based on 3:0"

wall load. Wall load is based on 3:0"

- tional joists beneath the opening's cripple study may be required.

 3. Table applies to joists 12 to 24 °o.c. that meet the floor open requirements for a design live load of 40 psf and dead load of 15 psf, and all reload deflection limit of 1/490. Use 12°o.c. requirements for I service.

the floor span requirements for a design live load of 40 psf and dead load of 15 psf, and a live load deflection limit of L/480. Use 12" o.c. requirements for lesser spacing.

the supporting wall and the ridge beam.

When the roof is framed using a ridge board,
the Roof Truss Span is equivalent to the
distance between the supporting walls as if a truss is used.

5. Cantilevered joists supporting girder trusse or roof beams may require additional

For hip roofs with the jack trusses running parallel to the cantilevered floor joists, the I-joist reinforcement

requirements for a span of 26 ft. shall be permitted to

BRICK CANTILEVER DETAILS FOR VERTICAL BUILDING OFFSET (CONCENTRATED WALL LOAD) Girder Roof trusses FIGURE 5 (continued (5a) SHEATHING REINFORCEMENT __ Roof truss ___ Roof truss -----span —Nail reinforcement to toy and bottom joist flanges with 2-1/2" nails at 6" o.c. (offset opposite face nailing by 3" when using reinforcement on both plywood sheathing or equivalent (minimum BRICK CANTILEVER REINFORCEMENT METHODS ALLOWED equivalent (minimum thickness 34/7 required on sides of joist. Depth shall match the full height of the joist. Nail with 2-1/2* noils of 6° o.c., top and bottom flange. Install with face grain horizontal. Attach I-joist to plate at all supports per detail 1b. Verify reinforced I-joist capacity. sides of I-joist) JOIST LL = 30 psf, DL = 15 psf TRUSS SPAN (ft) 3-1/2* 16 19.2 24 12 16 19.2 24 100108717 2224 (5b) SET-BACK DETAIL 201004 Rim board or wood structural panel closure (3/4" minimum thickness), attach per detail 1b. 11-7/8 Provide full denth blocking between joists over support (not shown for clarity) 14 (not snown for clarity) - Attach I-joist to plate at all supports per detail 1 b. - 3-1/2" minimum I-joist bearing required. Attach joists to girder joist per detail 5c. (5c) SET-BACK CONNECTION ... Nail joist end using 3" nails, toe-nail at top and bottom flanges. Vertical solid sawn blocks (2x6 S-P-F No. 2 or better) nailed through joist web and web of girder using 2-1/2" nails. Alternate for opposite side. Hanger may bused in lieu of solid sawn blo 4. For conventional roof construction using a ridge beam, the Roof Trues Span column above is equivalent to the distance between the supporting well and the ridge beam. When the root is formed using a ridge board, the Roof Truss Span is equivalent to the distance between the supporting wells as if a truss is used. 5. Confilewered joists supporting girder trusses or roof beams may require additional reinforcing. For larger openings, or multiple 3'.0" width openings spaced less than 6'-0" o.c., additional joists beneath the opening's cripple studs may be required. 3. Table applies to joists 12" to 24" o.c. that meet

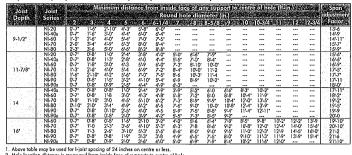
WEB HOLES

RULES FOR CUTTING HOLES AND DUCT CHASE OPENINGS:

- 2. I-joist top and bottom flanges must NEVER be cut, notched, or otherwise modified. 3. Whenever possible, field-cut holes should be centred on the middle of the web.
- 4. The maximum size hole or the maximum depth of a duct chase opening that can be cut into an I-joist web shall equal the clear distance between the flanges of the I-joist mixus 1/4 inch. A minimum of 1/2 inch should drowys be maintained between the top or bottom of the hole or opening and the adjacent I-joist flange.
- The sides of square holes or longest sides of rectangular holes should not exceed 3/4 of the diameter of the maximum round hole permitted at that location.
- are or me atometer of the maximum round hole permitted at that location.

 6. Where more than one hole is necessary, the distance between adjacent hole edges shall exceed twice the diameter of the largest round hole or twice the size of the largest square hole for twice the length of the largest side of the largest square hole or duct chase opening) and each hole and duct chase opining shall be sized and located in compliance with the requirements of Tables 1 and 2, respectively.
- A knockout is not considered a hole, may be utilized anywhere it occurs, and
 may be ignored for purposes of calculating minimum distances between holes
 and/or duct chase openings.
- Holes measuring 1-1/2 inches or smaller shall be permitted anywhere in a cantilevered section of a joist. Holes of greater size may be permitted subje-
- 9 A 1-1/2 inch hole or smaller can be placed anywhere in the web provided that it meets the requirements of rule number 6 above.
- All holes and duct chase openings shall be cut in a workman-like manner in accordance with the restrictions listed above and as illustrated in Figure 7.
- 11. Limit three maximum size holes per span, of which one may be a duct chase
- 12. A group of round holes at approximately the same location shall be permitted if they meet the requirements for a single round hole circumscribed around them.

TABLE 1
LOCATION OF CIRCULAR HOLES IN JOIST WEBS
Simple or Multiple Span for Dead Loads up to 15 psf and Live Loads up to 40 psf

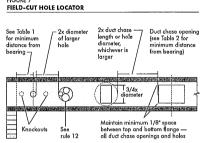


- Above table may be used for I-joist spacing of 24 inches on centre or less.
 Hole location distance is measured from inside face of supports to centre of hole.
 Distances in this chart are based on uniformly lo

The above table is based on the I-joists used at their maximum span. If the I-joists are placed at less than their full maximum span (see the minimum distance from the centreline of the hole to the face of any support (D) as given above may be reduced as follows: Dreduced = Lactual x D

Disduced by the control of the contr

DUCT CHASE OPENING SIZES AND LOCATIONS — Simple Span Only



Knockouts are prescored holes provided for the contractor's convenience to instal electrical or small plumbing lines. They are 1-1/2 inches in diameter, and are



Holes in webs should be cut with a sharp saw.

For rectangular holes, avoid over-cutting

For rectangular holes, avoid over-cutting the corners, as this can cause unnecessar stress concentrations. Slightly rounding the corners is recommended. Starting the rectangular hole by drilling a 1-inch diameter hole in each of the four corners and then making the cuts between the holes is another good method to minimize damage to the 1-joist.

Minimum distance from inside face of any support to Duct chase length (in.) 9-1/2 11-7/8 8-10 9-6 10-1 9-10 10-1 10-6 10-7 11-6 11-6 11-9 11-9 12-0 10'-1' 10'-6' 10'-4' 10'-7' 10'-11' 11'-1 12'-1 11'-10 12'-1' 12'-6' 12'-10' 10-7 11'-1' 10'-8' 11'-1'

13'-3'

2015-04-16

1. Above table may be used for I-joint spacing of 24 inches on cantre or less.
2. Dust chase opening location distance is measured from inside face of supports to centre of epening.
3. The above table is to send on simple-typen joist only. For other applications, context your local distributor.
4. Distances are based on uniformly located floor joist had meet be span requirements for a design live load of 40 pst and dead load of 13 pst, and a live lead defection limit of U/480. For other applications, context your local distributor.

INSTALLING THE GLUED FLOOR SYSTEM

- 1. Wipe any mud, dirt, water, or ice from I-joist flanges before gluing
- Snap a chalk line across the I-joists four feet in from the wall for panel edge alignment and as a boundary for spreading glue.
- Spread only enough glue to lay one or two panels at a time, or follow specific recommendations from the glue manufacturer.
- 4. Lay the first panel with tangue side to the wall, and nail in place. This protects the tangue of the next panel from damage when tapped into place with a block and sledgehammer.
- 5. Apply a continuous line of glue (about 1/4-inch diameter) to the top flange of a single I-joist. Apply glue in a winding pattern on wide areas, such as with double I-joists. 6. Apply two lines of glue on I-joists where panel ends butt to assure proper gluing of each end.
- 7. After the first row of panels is in place, spread glue in the groove of one or two panels at a time before laying the next row. Glue line may be continuous or spaced, but avoid squeeze-out by applying a thinner line (1/8 inch) than used on 1-joint flanges.
- 8. Tap the second row of panels into place, using a block to protect groove edges.
- Stagger end joints in each succeeding row of panels. A 1/8-inch space between all end joints and 1/8-inch at all edges, including 18.6 edges, is recommended. (Use a spacer tool or an 2-1/2" commendit to assure accurate and consistent spacing.)
- 10. Complete all nailing of each panel before glue sets. Check the manufacturer's recommendations for cure time. (Warm weather accelerates glue setting.) Use 2" ring- or screw-shank nails for panels 3/4-inch thick or less, and 2-1/2" ring- or screw-shank nails for linker panels. Space nails per the table below. Closer nail spacing may be required by some codes, or for diaphragm construction. The finished deck can be walked on right away and will carry construction loads without damage to the glue bond.

FASTENERS FOR SHEATHING AND SUBFLOORING(1)

Joist	Panel	Common	Ring Thread		of Fasteners		
Spacing (in.)	Thickness (in.)	Wire or Spiral Nails	Nails or Screws	Staples	Edges	Interm. Supports	
16	5/8	2"	1-3/4"	2*	6'	12"	
20	5/8	2*	1-3/4'	2"	6'	12"	
24	3/4	2*	1-3/4"	2.	6.	12"	

- ners of sheathing and subflooring shall conform to the above table
- 2. Staples shall not be less than 1/16-inch in diameter or thickness, with not less than a 3/8-inch grown
- 3. Flooring screws shall not be less than 1/8-inch in diameter.
- 4. Special conditions may impose heavy traffic and concentrated loads that require construction in excess
- Use only adhesives conforming to CAN/CGSB-71.26 Standard, Adhesives for Field-Gluing Plywood to Lumber Framing for Floor System, applied in accordance with the manufacturer's recommendations. If CSB panels with se

Ref.: NRC-CNRC, National Building Code of Canada 2010, Table 9.23.3.5.

IMPORTANT NOTE:

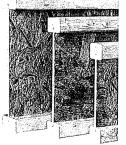
Floor sheathing must be field glued to the I-joist flanges in order to achieve the maximum spans shown in this document. If sheathing is nailed only, I-joist spans must be verified with

RIM BOARD INSTALLATION DETAILS (8a) ATTACHMENT DETAILS WHERE RIM BOARDS ABUT Rim board Joint Between Floor Joists 2-1/2" nails at 6" o.c. (typical) Rim board Joint at Corner top and bottom 2-1/2" toe-nails at 6" o.c. (typical) (8b) TOE-NAIL CONNECTION AT RIM BOARD 8c) 2X LEDGER TO RIM BOARD ATTACHMENT DETAIL Existing stud wall -Remove siding at ledger Continuous flashing extending at least 3" pas Top or sole plate — joist hange $\ell_{/3}$ 2" min. >1-5/8" min. Staggered 1/2" diameter lag screws or thru-bolts with 1-5/8* min. 5* max. 2' min. ---- Deck ioist (40188197₃₇

2x ledger board (pr



Z PRAPPIER 100100717



rative-treated); must be areater than or equal to the depth of the deck joist FSC ANTISONS SCY COSTISTY

NI Macking

· NI or rim board blocking

panel per detail la

For 2° thick flanges use net depth minus 4-1/4".

FILLER BLOCK REQUIREMENTS FOR DOUBLE 1-JOIST CONSTRUCTION

- 2x plate flush with inside face of wall

or beam. 1/8" overhang allowed past inside face of wall or beam.

NOTE: Unless hange

sides laterally support

the top flange, begring

installed per manufacturer

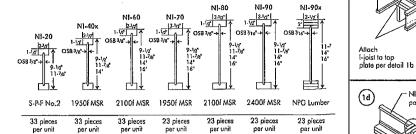
or Rim Joist

NI loists



www.nordicewp.com

Refer to the Installation Guide for Residential Floors for additional information CCMC EVALUATION REPORT 13032-R



WEB HOLE SPECIFICATIONS

Series

NI-40x NI-60

NI-40x NI-60

NI-70 NI-80 NI-90

NI-60 NI-70

NI-80 NI-90

9-1/2"

11-7/B

- 1. The distance between the inside edge of the support and the centreline of any hole or duct chase opening shall be in compliance with the requirements of Table 1 or 2, respectively.

 2. I-joist top and bottom flonges must NEVER be cut, notched, or otherwise modified.
- 3. Whenever possible, field-out holes should be centred on the middle of the web.
 4. The maximum size hole or the maximum depth of a duct chose opening that can be cut into an I-joist web shall equal the clear distance between the flances of the Lipist minus 1/4 inch. A minimum of 1/8 inch should always be maintained between the top or bottom of the hole or opening and the adjacent Lipist flaggs.

LOCATION OF CIRCULAR HOLES IN JOIST WEBS

Simple or Multiple Span for Dead Loads up to 15 psf and Live Loads up to 40 psf

- 5. The sides of square holes or longest sides of rectangular holes should not exceed 3/4 of the diameter of the maximum round hale nermitted at that location.
- More more than one hole is necessary, the distance between adjacent hole edges shall exceed twice the diameter of the largest round hole or twice the size of the largest. square hole (or twice the length of the longest side of the longest rectangular hole or duct chose opening) and each hole and duct chose opening shall be sized and located in compliance with the requirements of Tables 1 and 2, respectively.
- A knockout is not considered a hole, may be utilized anywhere it occurs, and may be ignored for purposes of calculating minimum distances between hales and/or duct
- Holes measuring 1-1/2 inches or smaller are permitted anywhere in a cantilevered section of a joist. Holes of greater size may be permitted subject to verification.
- 9. A 1-1/2 inch hole or smaller can be placed anywhere in the web
- 10. All holes and duct chase openings shall be out in a workman-like manner in accordance with the restrictions listed above and as lustrated in Figure 7.
- 11. Limit three maximum size holes per span, of which one may be
- a duct chase opening.

 12. A group of round holes at approximately the same location shall be permitted if they meet the requirements for a single round hole circumscribed around them.

Simple Span Only

М	inimun	Distar	ice from	n Insid	e Face	of Any	Support	to Cer	ntre of	Hole (ft	- in.)			,		Minim
				Rou	nd Hole	Diame	ter (in.)	·						Joist Depth	Joist Series	
	4	5	6	6-1/4	7	8	8-5/8	9	10	10-3/4	11	12	12-3/4	Dopin	00,100	- 8
<u>۲</u> "	2'-10"	4'-3"	5'-8"	6'-0"											NI-20	4'-1"
5"	3'-0"	4-4	6'-0"	6'-4"											NI-40x	5'-3"
6"	4'-0"	5'-4"	7'-0"	7'-5"	***									9-1/2"	NI-60	5'-4"
4"	41-9"	6'-3"	8'-0"	8'-4"											NI-70	5'-1"
6"	5'-0"	6'-6"	8'-2"	8'-8"											NI-80	5'-3'
B"	1'-0"	2'-4"	3'-8"	4'-0"	5'-0"	6'-6"	7'-9"		•		***		-40		NI-20	5-9"
8"	1'-3"	2'-8"	4'-0"	4-4	5'-5*	7'-0"	8'-4"							!	NI-40x	6'-8"
8"	3'-0"	4'-3"	5'-9"	6'-0"	7'-3"	8'-10"	10-0								NI-60	7'-3"
6"	4'-0"	5'-4"	6'-9"	7'-2*	8'-4"	10'-0"	11'-2"							11-7/8"	NI-70	7'-1"
10°	4'-2"	5'-6"	7'-0"	7'-5'	8'-6"	10'-3"	11'-4"			***				1	NI-80	7'-2'
8"	1-5	3'-2"	4'-10"	5'-4"	6'-9"	8'-9"	10'-2"							1	NI-90	7'-6"
8"	0'-9"	2'-5"	4'-4"	4'-9"	6'-3"	***	•••			***					NI-90x	7'-7'
8"	0'-8"	1'-0"	2'-4"	21-91	3'-9"	5-2"	6'-0°	6'-6"	8,-3,	10'-2"				i i	NI-40x	8'-1"
8™	1'-8"	3'-0"	4-3	4'-8"	5'-8"	7'-2"	8'-0"	8'-8"	10'-4"					1	NI-60	8'-9'
10"	3'-0"	4'-5"	5'-10"	6'-2"	7'-3"	8-9	91-9"	10'-4"						14*	NI-70	81-7"
٥"	3'-4"	4'-9"	6'-2"	6'-5"	7-6	9'-0"	10'-0"	10'-8"						'''	NI-80	9'-0"
8"	0'-10"	2'-5"	4'-0"	4'-5"	5'-9"	7'-5"	8'-8"	9'-4"	11'-4"					1 !	NI-90	9'-2"
B°	Ω'-8"	2'-0"	3'-9*	4'-2'	5'-5"	7'-3"	8'-5"	9'-2"							NI-90x	9'-4"
8"	0'-8"	1'-6"	2'-10"		4'-2"	5'-6"	6'-4"	7'-0"	8'-5"	9'-8'	10'-2"		13'-9"	1 I	NI-60	10'-3"
O"	2'-3"	3'-6"	4'-10'	5'-3"	6-3	7'-8"	8'-6"	9-2	10'-8"		12'-4"		15'-6"	ا ا	NI-70	10'-1"
3"	2-6"	3'-10"	5'-3"	5'-6"	6'-6"	8'-0"	9'-0"	9-5	11'-0"		12'-9"		16'-0"	16"	NI-80	10'-4' 10'-9'
8"	0'-8"	1'-9"	3'-3"	3,-8	4'-9"	6'-5"	7'-5"	8'-0" 8'-4"	9'-10"			13'-9"	15'-4"	1)	NI-90 NI-90x	1371
8"	0'-9"	2'-0"	3'-6"	4'-0"	5'-0"	61-91	7'-9"	8-4	10'-2"	11'-6°	12'-0"			<u>. </u>	M-AOX	17-1

- Above table may be used for Lipist spacing of 24 inches on centre or less.
 Hole location distance is measured from inside face of supports to centre of hole.
 Distances in this chart are based on uniformly loaded joists.
 The above table is based on the Lipists being used at their maximum spans. The minimum distance as given above may be reduced for shorter spans; contact your local distributor.

DUCT CHASE OPENING SIZES AND LOCATIONS

1.7.4	Joist	Minimi	ım distan	ce from in	side tace	of suppo	ons to ce	entre of c	pening (# - ID.)
Joist Depth	Series				Duct Ch	ase Leng	th (in.)			
Dopin	00,100	8	10	12	14	16	18	20	22	24
	NI-20	4'-1"	4'-5"	4'-10"	5'-4"	5'-8"	6'-1"	6'-6"	7'-1"	7'-5"
	NI-40x	5'-3"	5'-8"	6'-0"	6'-5"	6'-10"	7'-3"	7'-8"	8'-2"	8'-6"
9-1/2"	NI-60	5'-4"	5'-9"	6'-2"	6'-7"	7'-1"	7'-5"	8'-0"	8'-3"	8'-9"
	NI-70	5'-1"	5'-5"	5'-10"	6'-3"	6'-7"	7'-1"	7'-6"	8'-1"	8'-4"
	NI-80	5'-3'	5'-8"	6'-0"	6'-5"	6'-10"	7'-3"	7'-8"	8'-2"	8'-6"
	NI-20	5-9"	6'-2"	6'-6"	7'-1'	7'-5'	7'-9"	8'-3"	8'-9"	9'-4"
	NI-40x	6'-8"	7'-2°	7'-6"	8'-1"	8'-6"	9'~1"	9'-6"	10'-1"	10'-9"
	NI-60	7'-3"	7'-8"	8'-0"	B'-6"	9'-0"	9'-3"	9'-9"	10'-3"	11'-0"
11-7/8"	NI-70	7'-1"	7'-4"	7'-9'	8'-3"	8'-7"	9'-1°	9'-6"	10'-1"	10'-4"
-	NI-80	7'-2"	71-74	8'-0"	8'-5"	8'-10"	9'-3"	9'-8"	10'-2"	10'-8"
	NI-90	7'-6"	74111	8'-4"	8'-9"	9'-2"	9'-7"	10'-1"	10'-7"	10:11*
	NI-90x	7'-7"	8'-1"	8'-5"	8'-10"	9'-4"	9'-8"	10'-2"	10'-8"	11-2"
	NI-40x	8'-1"	8'-7"	9'-0"	9'-6"	10'-1°	10'-7"	111-2"	12'-0"	12'-8"
	NI-60	8'-9"	9'-3"	9'-8"	10'-1"	10'-6"	11'-1"	11'-6"	13'-3"	13'-0"
14*	NI-70	8'-7"	9'-1"	9'-5"	9'-10"	10-4*	10'-8"	1142	11'-7"	12'-3'
14	NI-80	9'-0"	91-3×	9-9	10'-1"	10'-7"	11'-1"	11'-6"	12'-1"	12-6
	NI-90	9'-2"	9'-8"	10'-0"	10'-6"	10'-11'		11'-9"	12'-4"	12411*
	NI-90x	9'-4"	9'-9"	10'-3"	10'-7°	11'-1"	11'-7'	12'-1"	12'-7"	13-2"
	NI-60	10'-3"	10'-8"	111-2"	11'-6"	12'-1"	12-6	13'-2"	14'-1"	145-10"
	NI-70	10'-1"	10'-5"	11'-0"	11'-4"	11'-10'		12'-8"	13'-3"	14'-0"
16"	NI-80	10'-4'	10'-9"	11'-3"	11'-9"	12'-1"	12'-7"	13'-1"	13'-8"	14-4
	NI-90	10-9	11'-2"	11'-8"	12'-0"	12'-6"	13'-0°	13'-6"	14-2	14'-10"
	NI-90x	13'-1"	11'-5"	114-10*	12'-4"	12'-10'	13'-2"	13'-9"	14-4	15'-2"

- Above table may be used for I-joist spacing of 24 inches on centre or less.

 Duct chase opening location distance is measured from inside face of supports to centre of opening.

 The above table is based on simple-span joists only. For other applications, contact your local distributor.

 Distances are based on uniformly loaded floor joists that meet the span requirements for a design live load of 40 pst and dead load of 15 pst, and a live load deflection limit of L/480.

 The above table is based on the 1-joist being used of their maximum spans. The minimum distance as given above may be reduced for shorter spans; contact your local distributor.

-1/8" to 1/4" gap between top flange and filler block

block

Flance Width

2-1/2*

3-1/2*

Offset nails from opposite face by 6°

clinched, only two nails per foot are required.

The maximum factored load that may be applied to one side of the double joist using this detail is 860 lbf/ft. Verify double 1-joist capacity.

Flange Size Net Depth Filler Block Size 1. Support stack or Flash were outing fatting to prevent damage to web/flange connection. 2. Leave a 1/8 to 1/4-inch gap between top of filler block and bottom of top I-joist flange. 3. Filler block is required between joists for full length 2-1/8" x 6" 2-1/8" x 8" 2-1/2°x 11-7/8° 1-1/2* 2-1/8" × 10" 2-1/8" x 12" 9-1/2" Nail joists together with two rows of 3" nails at 12 inches o.c. (clinched when possible) on each side of the double 3-1/2° x I-1/2° 1-joist. Total of four nails per foot required. If nails can be 1-7/8° 3-1/2° x

-One 2-1/2" noil at top and bottom flance (15) ~2x4 min. (1/8" gap minimum) Two 2-1/2" nails from each web to lumber piece nails at 6° a.c.-- I-joist blocking panel One 2-1/2" nail one side only NOTES:

(1r)

Maximum Factored Uniform

1-1/8" Rim Board Plus

One 2-1/2' wire or spiral nail at top and bottom flange

Minimum bearing length shall be 1-3/4° for the end bearings, and 3-1/2° for the intermediate bearings when applicable.

2-1/2° nails 3

at 6" o.c.

Double Ligist header

NOTE: Unless hanger

eides laterally support

Bocker block required

(both sides for face-

mount hangers)

– Do nat bevel-cut

per detail 1b

NOTE: Blacking required at

bearing for lateral support, not shown for clarity.

to top plate

from above to

bearing below

Install squash

Match bearing

area of blocks below to post

recommendations. Verity double I-joist capacity to suppor

(1n)

blocks per

Top- or face-mount

Filler block -

Multiple I-joist header with full depth filler

block shown, Nordic Lam or SCL headers may also be used. Verify double 1-jois

Ancker block attached per

detail 1 h. Nail with twelve 3"

Install hanger per

manutaciurer's

nails, clinch when possible

- Attach rim board to top plate using 2-1/2" wire or spiral toe-nails at 6" o.c.

To avoid splitting flange, start nails at least 1-1/2" from end of I-joist

Nails may be driven at an angle to avoid splitting of bearing plate

Vertical Load* (plf)

8.090

The uniform vertical load is limited to a rim board depth of 16 inches or less and is based on

standard term load duration. It shall not be used in the design of a bending member, such as joist, header, or rafter. For concentrated vertical load transfer, see detail 1d.

Load bearing wall above shall align vertically

with the bearing below. Other conditions, such

as offset bearing walls, are not covered by

Blocking required over all interior supports under

Structural Composite Lumber (SCL)

For nailing schedules for multiple

beams, see the manufacturer's

Top- or face-mount hanger

Lumber 2x4 min., extend block to face of adjacent web. Two 2-1/2" spirol nails

from each web to lumber piece, alternate

OPTIONAL: Minimum 1x4 inch strap

applied to underside of joist at blocking line or 1/2 inch minimum gypsum

ceiling attached to underside of joists.

installed per manufacturer's

continuous over support

Nordic Lam or

-NI blocking panel per detail 1a

NOTE: Unless hanger sides laterally support the top flange,

on opposite side.

bearing stiffeners shall be used.

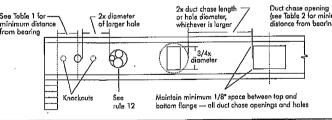
load-bearing walls or when floor joists are not

In some local codes, blocking is prescriptively required in the first joist space (or first and second joist space) next to the starter joist. Where required, see to requirements for spacing of the blocking. All nails are common spiral in this detail.

All nails shown in the above details are assumed to be mon wire nails noted. 3" (0.122" dia.) common spiral nails may be substituted f 2-1/2" (0.128" dia.) assumed to be Spruce-Pine-Fir No. 2 or better. Individual ate not show

FIGURE 7

FIELD-CUT HOLE LOCATOR





Knockauts are prescored holes provided for the contractor's convenience to install electrical or small plumbing lines. They are 1-1/2 inches in diameter, and are spaced 15 inches on centre along the length of the I-joist. Where possible, it is preferable to use knockouts instead of field-cut hales.

lever drill, cut or notch the flange, or over-cut the web.

Holes in webs should be cut with a sharp saw

For rectangular hales, avoid over-cutting the corners, as this can cause non-ceasing views cover-coming me conters, as this con cause unnecessory stress concentrations. Slightly rounding the corners is recommended. Starting the rectangular hole by drilling a 1-inch diameter hole in each of the four corners and then making the cuts between the holes is another good method to minimize damage to the I-joist.

SAFETY AND CONSTRUCTION PRECAUTIONS



Do not walk on I-joists until fully fastened and braced, or



Never stock building materia over unsheathed Lipists. Once sheathed, do not over-stress WARNING: I-joists are not stable until completely installed, and will not carry any load until fully braced and sheathed.

AVOID ACCIDENTS BY FOLLOWING THESE IMPORTANT GUIDELINES:

- Brace and noil each I-joist as it is installed, using hangers, blocking panels, rim board, and/or cross-bridging at joist ends.
 When I-joists are applied continuous over interior supports and a load-bearing wall is planned at that location, blocking will
- 2. When the building is completed, the floor sheathing will provide lateral support for the top flanges of the L-joists. Until this sheathing is applied, temporary bracing, often called struts, or temporary sheathing must be applied to prevent L-joist rollover or buckling.

 I approve
- or buckling.

 ** Temporary bracing or struts must be 1x4 inch minimum, at least 8 feet long and spaced no more than 8 feet on centre, and must be secured with a minimum of two 2-1/2" noils fastened to the top surface of each i-joist. Noil the bracing to a lateral restraint at the end of each boy. Lop ends of adjoining bracing over at least two I-joists.

 **Or, sheathing (temporary or permanent) can be noiled to the top flange of the first 4 feet of I-joist at the end of the boy.
- 3. For contilevered Lipists, brace top and bottom flanges, and brace ends with closure panels, rim board, or cross-bridging.
- Install and fully nail permanent sheathing to each I-joist before placing loads on the floor system. Then, stack building materials over beams or walls only.
- 5. Never install a domoged l-joist. Improper storage or installation, failure to follow applicable building codes, failure to follow span ratings for Nordic I-joists, failure to fallow allowable hole sizes and locations, or failure to use web stiffeners when required can result in serious occidents. Follow these installation guidelines carefully.

CHANTIERS PRODUCT WARRANTY Chansiers Chibongaman guarantees that, in accordance with our specifications, Nordic products are free from manufacturing defects in material and workmanship. Furthermore, Chantiers Chibougaman warrants that our products, ien utilized in accordance with our handling and installation instruction will meet or exceed our specifications for the lifetime of the structure.

WEB STIFFENERS

RECOMMENDATIONS:

- A bearing stiffener is required in all engineered applications with factored reactions greater than shown in the I-joist properties table found of the I-joist Construction Guide (C101). The gap between the stiffener and the flange is at
- A bearing stiffener is required when the I-joist is supported in a hange and the sides of the hanger do not extend up to, and support, the top flange. The gap between the stiffener and flange is at the top.
- A load stiffener is required at locations where a factored concentrated load greater than 2,370 lbs is applied to the top flonge between supports, or in the case of a cantilever, anywhere between the confilever tip and the support. These volues are for standard term load duration, and may be adjusted for other load durations as permitted by the code. The gap between

Maximum Factored Uniform

Vertical Load* (plf)

Maximum Factored

Vertical Load per Pair of Squash Blocks (lbs

3-1/2" 5-1/2 wide wide

5,500 8,500

4,300 6,600

face nail at each side at bearing

3 300

*The uniform vertical load is limited to a joist death of 16

inches or less and is based on standard term load duration

It shall not be used in the design of a bending member, such as joist, header, or rafter. For concentrated vertical load

2-1/2" nails at 6" o.c. to top plate (when used for lateral

shear transfer, noil to bearing plate with same nailing as required for decking)

Provide lateral bracing per detail 1g or 1b

Minimum Depth**

5.1/2"

7-1/4*

conacity = 1.620 the

Support back of I-joist web during nailing to prevent

2x Lumber

Backer black (use if hanger load exceeds 360 lbs). Before installing a backer black to a double I-joist, drive three additional 3° nails through the webs and filler block where the

Minimum grade for backer black material shall be S-P-F No. 2 or better for solid sawn lumber and

wood structural panels conforming to CAN/CSA-O325 or CAN/CSA-O437 Standard.
*For face-mount hangers use net joist depth minus 3-1/4" for joists with 1-1/2" thick flanges

BACKER BLOCKS (Blocks must be long enough to permit required nailing without splitting)

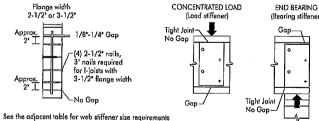
Material Thickness Required*

backer block will fit. Clinch, Install backer tight to top flange. Use twelve 3° nails, clinched

factored resistance for hunger for this detail = 1,620 lbs.

(Im)

WEB STIFFENER INSTALLATION DETAILS



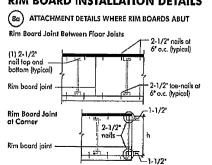
STIFFENER SIZE REQUIREMENTS Web Stiffener Size Each Side of Web 1" x 2-5/16" 2-1/2 minimum width 1.1/2° x 2.5/16° 3-1/2°

CANTILEVER DETAILS FOR VERTICAL BUILDING OFFSET

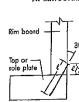


NOTE: Canadian softwood plywood sheathing or equivalent (minimum thickness 3/4") required on sides of joist. Depth shall match the full height of the joist. Nail with 2-1/2" nails at 6" o.c., top and bottom flange. Install with face grain horizontal. Attach I-joist to plate at all supports per detail 1b. Verify reinforced I-joist capacity.

RIM BOARD INSTALLATION DETAILS



8b TOE-NAIL CONNECTION AT RIM BOARD



NORDIC STRUCTURES

COMPANYJune 12, 2020 15:39

PROJECT
J1 - 1ST FLOOR

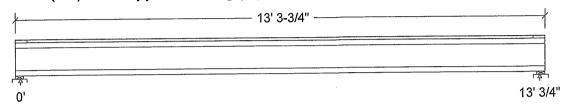
Design Check Calculation Sheet

Nordic Sizer - Canada 7.2

Loads:

Load	Type	Distribution	Pat-	Location	[ft]	Magnitu	de	Unit
Boad	1150	1	tern	Start	End	Start	End	
Load1	Dead	Full Area				20.00		psf
Load2	Live	Full Area				40.00		psf

Maximum Reactions (lbs) and Support Bearing (in):



Unfactored: Dead Live	174 348		174 348
Factored: Total	740		740
Bearing:			
Capacity		·	
Joist	1865		1865
Support	3981		3981
Des ratio			0 40
Joist	0.40		0.40
Support	0.19		0.19
Load case	#2		#2
Length	2-3/8		2-3/8
Min req'd	1-3/4		1-3/4
Stiffener	No		No
KD	1.00		1.00
KB support	1.00		1.00
fcp sup	769		769
Kzcp sup	1.09		1.09

Nordic Joist 9-1/2" NI-40x Floor joist @ 16" o.c.

Supports: All - Lumber Sill plate, No.1/No.2

Total length: 13' 3-3/4"; Clear span: 12' 11"; 3/4" nailed and glued OSB sheathing

This section PASSES the design code check.

Limit States Design using CSA 086-14 and Vibration Criterion:

	-			
Criterion	Analysis Value	Design Value	Unit	Analysis/Design
Shear	Vf = 740	Vr = 1895	lbs	Vf/Vr = 0.39
Moment (+)	Mf = 2417	Mr = 4824	lbs-ft	Mf/Mr = 0.50
Perm. Defl'n	0.07 = < L/999	0.44 = L/360	in ,	0.17
Live Defl'n	$0.15 = \langle L/999$	0.33 = L/480	in growth	0.46
Total Defl'n	0.22 = L/702	0.65 = L/240	in 🎉	2300 0.34
Bare Defl'n	0.18 = L/860	0.44 = L/360	in /2 (0.42
Vibration	Lmax = 13'-0.8	Lv = 16'-2.1	ft w	KATSOULAKOS \$0.81
Defl'n	= 0.027	= 0.052	in [% S	KATSOULAKUS 50, 51
L DOLL 11	L	L	20 1122	Character 1

STRUCTURAL COMPONENT ONLY

WoodWorks® Sizer

for NORDIC STRUCTURES

J1 - 1ST FLOOR

Nordic Sizer - Canada 7.2

Page 2

### Additional Data: FACTORS:											
Vr 1895 1.00 1.00 #2 Mr+ 4824 1.00 1.00 - 1.000 #2 EI 218.1 million #2 CRITICAL LOAD COMBINATIONS: Shear : LC #2 = 1.25D + 1.5L Moment(+): LC #2 = 1.25D + 1.5L Deflection: LC #1 = 1.0D (permanent)	Additional	Data:									
Mr+ 4824 1.00 1.00 - 1.000 #2 EI 218.1 million #2 CRITICAL LOAD COMBINATIONS: Shear : LC #2 = 1.25D + 1.5L Moment(+) : LC #2 = 1.25D + 1.5L Deflection: LC #1 = 1.0D (permanent)	FACTORS:	f/E	KD	KH	KZ	KL	KT	KS	KN		
CRITICAL LOAD COMBINATIONS: Shear : LC #2 = 1.25D + 1.5L Moment(+) : LC #2 = 1.25D + 1.5L Deflection: LC #1 = 1.0D (permanent) LC #2 = 1.0D + 1.0L (live) LC #2 = 1.0D + 1.0L (total) LC #2 = 1.0D + 1.0L (bare joist) Bearing : Support 1 - LC #2 = 1.25D + 1.5L Support 2 - LC #2 = 1.25D + 1.5L Load Types: D=dead W=wind S=snow H=earth,groundwater E=earthquake L=live(use,occupancy) Ls=live(storage,equipment) f=fire Load Patterns: s=S/2 L=L+Ls =no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	Vr	1895	1.00		-	_	-	-	-		
CRITICAL LOAD COMBINATIONS: Shear : LC #2 = 1.25D + 1.5L Moment(+) : LC #2 = 1.25D + 1.5L Deflection: LC #1 = 1.0D (permanent) LC #2 = 1.0D + 1.0L (live) LC #2 = 1.0D + 1.0L (total) LC #2 = 1.0D + 1.0L (bare joist) Bearing : Support 1 - LC #2 = 1.25D + 1.5L Support 2 - LC #2 = 1.25D + 1.5L Load Types: D=dead W=wind S=snow H=earth, groundwater E=earthquake L=live(use, occupancy) Ls=live(storage, equipment) f=fire Load Patterns: s=S/2 L=L+Ls =no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	Mr+	4824	1.00	1.00	-	1.000	-	-	-		
Shear : LC #2 = 1.25D + 1.5L Moment(+) : LC #2 = 1.25D + 1.5L Deflection: LC #1 = 1.0D (permanent) LC #2 = 1.0D + 1.0L (live) LC #2 = 1.0D + 1.0L (total) LC #2 = 1.0D + 1.0L (bare joist) Bearing : Support 1 - LC #2 = 1.25D + 1.5L Support 2 - LC #2 = 1.25D + 1.5L Load Types: D=dead W=wind S=snow H=earth, groundwater E=earthquake L=live(use,occupancy) Ls=live(storage,equipment) f=fire Load Patterns: s=S/2 L=L+Ls _=no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012				_		-	-	-	_	#2	
Shear : LC #2 = 1.25D + 1.5L Moment(+) : LC #2 = 1.25D + 1.5L Deflection: LC #1 = 1.0D (permanent) LC #2 = 1.0D + 1.0L (live) LC #2 = 1.0D + 1.0L (total) LC #2 = 1.0D + 1.0L (bare joist) Bearing : Support 1 - LC #2 = 1.25D + 1.5L Support 2 - LC #2 = 1.25D + 1.5L Load Types: D=dead W=wind S=snow H=earth, groundwater E=earthquake L=live(use,occupancy) Ls=live(storage,equipment) f=fire Load Patterns: s=S/2 L=L+Ls _=no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	CRITICAL LO	DAD COMB	INATIONS	S:							
Moment(+): LC #2 = 1.25D + 1.5L Deflection: LC #1 = 1.0D (permanent) LC #2 = 1.0D + 1.0L (live) LC #2 = 1.0D + 1.0L (total) LC #2 = 1.0D + 1.0L (bare joist) Bearing: Support 1 - LC #2 = 1.25D + 1.5L Support 2 - LC #2 = 1.25D + 1.5L Load Types: D=dead W=wind S=snow H=earth,groundwater E=earthquake L=live(use,occupancy) Ls=live(storage,equipment) f=fire Load Patterns: s=S/2 L=L+Ls _=no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	Shear	: LC #2	= 1.2	5D + 1.5	L						
Deflection: LC #1 = 1.0D (permanent) LC #2 = 1.0D + 1.0L (live) LC #2 = 1.0D + 1.0L (total) LC #2 = 1.0D + 1.0L (bare joist) Bearing: Support 1 - LC #2 = 1.25D + 1.5L Support 2 - LC #2 = 1.25D + 1.5L Load Types: Dedead Wewind Sesnow Hearth, groundwater Eearthquake Lelive(use, occupancy) Lselive(storage, equipment) fefire Load Patterns: s=S/2 L=L+Ls = no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: Eleff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	Moment(+)) : LC #2	= 1.2	5D + 1.5	L						
LC #2 = 1.0D + 1.0L (total) LC #2 = 1.0D + 1.0L (bare joist) Bearing: Support 1 - LC #2 = 1.25D + 1.5L Support 2 - LC #2 = 1.25D + 1.5L Load Types: D=dead W=wind S=snow H=earth,groundwater E=earthquake L=live(use,occupancy) Ls=live(storage,equipment) f=fire Load Patterns: s=S/2 L=L+Ls _=no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	Deflection	on: LC #1	= 1.0	D (perm	anent)						*
LC #2 = 1.0D + 1.0L (bare joist) Bearing: Support 1 - LC #2 = 1.25D + 1.5L		LC #2	= 1.0	D + 1.0L	(live	:)					
Bearing: Support 1 - LC #2 = 1.25D + 1.5L Support 2 - LC #2 = 1.25D + 1.5L Load Types: D=dead W=wind S=snow H=earth,groundwater E=earthquake L=live(use,occupancy) Ls=live(storage,equipment) f=fire Load Patterns: s=S/2 L=L+Ls _=no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012		LC #2	= 1.0	D + 1.0L	(tota	.1)					
Support 2 - LC #2 = 1.25D + 1.5L Load Types: D=dead W=wind S=snow H=earth,groundwater E=earthquake L=live(use,occupancy) Ls=live(storage,equipment) f=fire Load Patterns: s=S/2 L=L+Ls =no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012		LC #2	= 1.0	D + 1.0L	(bare	: joist)					
Load Types: D=dead W=wind S=snow H=earth, groundwater E=earthquake L=live(use,occupancy) Ls=live(storage,equipment) f=fire Load Patterns: s=S/2 L=L+Ls =no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	Bearing	: Suppo	rt 1 -	LC #2 =	1.25D +	1.5L					
L=live(use,occupancy) Ls=live(storage,equipment) f=fire Load Patterns: s=S/2 L=L+Ls _=no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012		Suppo	rt 2 - 1	LC #2 = 1	1.25D +	1.5L					
Load Patterns: s=S/2 L=L+Ls _=no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: Eleff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	Load Type										
All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: Eleff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012									f=fire		
All Load Combinations (LCs) are listed in the Analysis output CALCULATIONS: Eleff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	Load Pati	terns: s=	s/2 L=	L+Ls ==	no patt	ern load	in this	s span			
CALCULATIONS: EIeff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012	All Load	Combinat	ions (L	Cs) are	listed	in the An	alysis	output			
Eleff = 275.77 lb-in^2 K= 4.94e06 lbs "Live" deflection is due to all non-dead loads (live, wind, snow) CONFORMS TO OBC 2012											
"Live" deflection is due to all non-dead loads (live, wind, snow) GONFORMS TO UBG 2012	Eleff = 2	275.77 lb	-in^2	K = 4.94	e06 lbs						*** ***
	"Live" de	eflection	is due	to all	non-dea	d loads (live, v	wind, sn	.ow)	canforms to	UBG 2012
AMENDED 2020										писиось	2020

Design Notes:

AMENDED 2020

- 1. WoodWorks analysis and design are in accordance with the 2015 National Building Code of Canada (NBC), Division B, Part 4, and the CSA 086-14 Engineering Design in Wood standard, Update No. 2 (June 2017).
- 2. Please verify that the default deflection limits are appropriate for your application.
- 3. Refer to Nordic Structures technical documentation for installation guidelines and construction details.
- 4. Nordic I-joists are listed in CCMC evaluation report 13032-R.
- 5. Joists shall be laterally supported at supports and continuously along the compression edge.
- 6. The design assumptions and specifications have been provided by the client. Any damages resulting from faulty or incorrect information, specifications, and/or designs furnished, and the correctness or accuracy of this information is their responsibility. This analysis does not constitute a record of the structural integrity of the building nor suitability of the design assumptions made. Nordic Structures is responsible only for the structural adequacy of this component based on the design criteria and loadings shown.

S. KATSOULAKOS S.

OWO NO. TAM ///88-20 STRUCTURAL COMPONENT ONLY



COMPANYJune 12, 2020 15:41

PROJECT
J1 - 2ND FLOOR

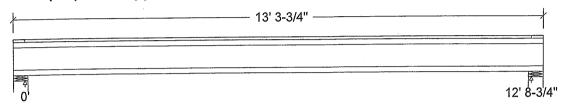
Design Check Calculation Sheet

Nordic Sizer - Canada 7.2

Loads:

ĺ	Load	Type	Distribution	Pat-	Location	[ft]	Magnitude		Unit
	Поаа	-71-		tern	Start	End	Start	End	
1	Load1	Dead	Full Area				20.00		psf
	Load2	Live	Full Area				40.00		psf

Maximum Reactions (lbs) and Support Bearing (in):



Unfactored: Dead Live	170 339	170 339
Factored: Total	721	721
Bearing: Capacity Joist Support	1893 7744	1893 7744
Des ratio Joist Support	0.38	0.38 0.09 #2
Load case Length Min req'd	#2 4-3/8 1-3/4	4-3/8 1-3/4
Stiffener KD	No 1.00	No 1.00
KB support fcp sup	I	769 -
Kzcp sup	1	

Bearing for wall supports is perpendicular-to-grain bearing on top plate. No stud design included.

Nordic Joist 9-1/2" NI-40x Floor joist @ 16" o.c.

Supports: All - Lumber Wall, No.1/No.2

Total length: 13' 3-3/4"; Clear span: 12' 7"; 5/8" nailed and glued OSB sheathing with 1/2" gypsum ceiling

This section PASSES the design code check.

Limit States Design using CSA O86-14 and Vibration Criterion:

Criterion	Analysis Value	Design Value	Unit	Analysis/Design
Shear	Vf = 721	Vr = 1895	lbs	Vf/Vr = 0.38
Moment (+)	Mf = 2295	Mr = 4824	lbs-ft	Mf/Mr = 0.48
Perm. Defl'n	0.07 = < L/999	0.42 = L/360	in	0.16
Live Defl'n	0.14 = < L/999	0.32 = L/480	in 🖋	OFESSION 0.44
Total Defl'n	0.21 = L/734	0.64 = L/240	in #	0.33
Bare Defl'n	0.17 = L/923	0.42 = L/360	in 🕼	23020 0.39
Vibration	Lmax = 12'-8.8	Lv = 15'-9.3	ft /3 (70.81
Defl'n	= 0.028	= 0.054	ın ju	1.51
			1 434	I WHOUSE

JOWN NO. TAM 11/89 - 20 STRUCTURAL CONFONENT ONLY

WoodWorks® Sizer

for NORDIC STRUCTURES

J1 - 2ND FLOOR

Nordic Sizer - Canada 7.2

Page 2

			· · · · · · · · · · · · · · · · · · ·									
Additional	Data:											
FACTORS:	f/E	KD	KH	KZ	KL	KT	KS	KN	LC#			
Vr	1895	1.00	1.00		_	-	-	-	#2			
Mr+	4824	1.00	1.00	_	1.000	-	-	-	#2			
EI	218.1 m	nillion	-	-	_	-	-	-	#2			
CRITICAL LO	OAD COME	SINATIONS	S:									
Shear	: LC #2	2 = 1.2	5D + 1.5I	J								
Moment (+)) : LC #2	= 1.25	5D + 1.5I	J								
Deflection	on: LC #1	= 1.01	D (perma	anent)								
	LC #2	= 1.01	D + 1.0L	(live)							
			D + 1.0L									
	LC #2	2 = 1.01	D + 1.0L	(bare	joist)							
Bearing	: Suppo	ort 1 - :	LC #2 = 3	L.25D +	1.5L							
	Suppo	ort 2 - :	LC #2 = 3	L.25D +	1.5L							
Load Type	es: D=dea	ad W=wi	nd S=sno	ow H=e	arth,grou	ndwate	r E=ear	thquake				
	L=liv	re(use,o	ccupancy)	Ls=l	ive(stora	.ge,equ:	ipment)	f=fire				
Load Pat	terns: s=	=S/2 L=:	L+Ls _=r	no patt	ern load	in this	s span	-				
All Load	Combinat	cions (L	Cs) are 1	listed	in the An	alysis	output					
CALCULATI	ONS:											
ETeff =	267.73 lk	o-in^2	K= 4.94	e06 lbs					ant coults.	MI es		
"Live" d	eflectior	n is due	to all m	non-dea	d loads (live, v	wind, sn	ow)	COMPORMS	IJ	UBC	2012
									REPER	17 h		

Design Notes:

AMENDED 2020

1. WoodWorks analysis and design are in accordance with the 2015 National Building Code of Canada (NBC), Division B, Part 4, and the CSA O86-14 Engineering Design in Wood standard, Update No. 2 (June 2017).

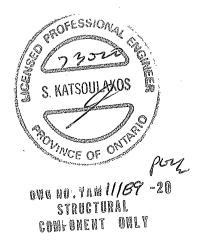
2. Please verify that the default deflection limits are appropriate for your application.

3. Refer to Nordic Structures technical documentation for installation guidelines and construction details.

4. Nordic I-joists are listed in CCMC evaluation report 13032-R.

5. Joists shall be laterally supported at supports and continuously along the compression edge.

6. The design assumptions and specifications have been provided by the client. Any damages resulting from faulty or incorrect information, specifications, and/or designs furnished, and the correctness or accuracy of this information is their responsibility. This analysis does not constitute a record of the structural integrity of the building nor suitability of the design assumptions made. Nordic Structures is responsible only for the structural adequacy of this component based on the design criteria and loadings shown.







City, Province, Postal Code: MARKHAM

Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1ST FLR FRAMING\Flush Beams\B1 H(i3375) (Flush Beam)

PASSED

June 12, 2020 15:19:25

BC CALC® Member Report

Build 7493

Job name: Address:

Customer:

Dry | 1 span | No cant.

PEYTON 3 - EL 1,2,3.mmdl File name:

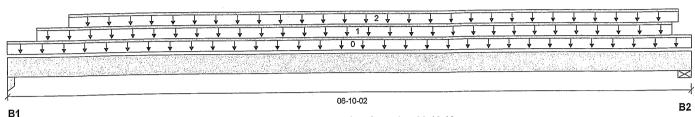
1ST FLR FRAMING\Flush Beams\B1 H(i3375) Description:

Specifier:

L.D.

Designer: Company:

CCMC 12472-R Code reports:



Total Horizontal Product Length = 06-10-02

Snow

Reaction Summary (Down / Uplift) (lbs)

Bearing	Live	` Dead
B1, 3-1/2"	832 / 0	433 / 0
B2, 2-3/8"	831 / 0	431 / 0

1.0	od Cummani						Live	Dead	Snow	1.15	Tributary
	ad Summary Description	Load Type	Ref.	Start	End	Loc.	1.00	0.65	1.00	1.15	
nag	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	06-10-02	Тор		5			00-00-00
1	STAIRS	Unf. Lin. (lb/ft)	L	00-03-08	06-07-12	Тор	240	120			n\a
2	FC4 Floor Material	Unf. Lin. (lb/ft)	L	00-07-04	06-08-08	Тор	21	10			n\a

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	2941 ft-lbs	11610 ft-lbs	25.3%	1	03-05-12
End Shear	1366 lbs	5785 lbs	23.6%	1	01-01-00
Total Load Deflection	L/999 (0.063")	n\a	n\a	4	03-05-12
Live Load Deflection	L/999 (0.041")	n\a	n\a	5	03-05-12
Max Defl.	0.063"	n\a	n\a	4	03-05-12
Span / Depth	8.2				

Bearing	Supports	Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B1		3-1/2" x 1-3/4"	1789 lbs	36.0%	23.9%	Unspecified
B2		2-3/8" x 1-3/4"	1785 lbs	69.8%	35.2%	Spruce-Pine-Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

GUNFORMS TO OBG 2012

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86. AMENDED 2020 BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86.

Design based on Dry Service Condition.

Importance Factor : Normal Part code : Part 9



STRUCTURAL COMPONENT ONLY

Disclosure

Use of the Boise Cascade Software is subject to the terms of the End User License Agreement (EULA). Completeness and accuracy of input must be reviewed and verified by a qualified engineer or other appropriate expert to assure its adequacy, prior to anyone relying on such output as evidence of suitability for a particular application. The output here is based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call (800)232-0788 before installation.

BC CALC®, BC FRAMER®, AJS™ ALLJOIST® , BC RIM BOARD $^{\mathsf{TM}}$, BCI® , BOISE GLULAM™, BC FloorValue®, VERSA-LAM®, VERSA-RIM PLUS®,





City, Province, Postal Code: MARKHAM

Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

June 12, 2020 15:19:25

1ST FLR FRAMING\Flush Beams\B2 H(i3287) (Flush Beam)

Dry | 1 span | No cant.

BC CALC® Member Report

Build 7493 Job name: Address: File name:

Des

PEYTON 3 - EL 1,2,3.mmdl

1ST FLR FRAMING\Flush Beams\B2 H(i3287)

Description: 1ST FLR FRAMING\FI

Wind

Specifier:

Designer: L.D.

Design

Customer: Code reports:

CCMC 12472-R

Company:

05-01-06

B1

Total Horizontal Product Length = 05-01-06

Snow

Reaction Summary (Down / Uplift) (lbs)

Bearing	Live	Dead
B1, 2-3/8"	296 / 0	161 / 0
B2. 1-3/4"	385 / 0	206 / 0

1 0	ad Summary						Live	Dead	Snow	Wind	Tributary
LO:		Load Type	Ref.	Start	End	Loc.	1.00	0.65	1.00	1.15	
0	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	05-01-06	Тор		5			00-00-00
1	Smoothed Load	Unf. Lin. (lb/ft)	L	01-05-14	05-01-06	Top	146	74			n\a
2	.14(i3286)	Conc. Pt. (lbs)	L	00-09-14	00-09-14	Top	150	75			n\a

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	866 ft-lbs	11610 ft-lbs	7.5%	1	02-01-14
End Shear	572 lbs	5785 lbs	9.9%	1	00-11-14
Total Load Deflection	L/999 (0.01")	n\a	n\a	4	02-06-14
Live Load Deflection	L/999 (0.007")	n\a	n\a	5	02-06-14
Max Defl.	0.01"	n\a	n\a	4	02-06-14
Span / Depth	6.2				

Bearing Suppo	O rts Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B1 Wall/Pla	ate 2-3/8" x 1-3/4"	645 lbs	25.2%	12.7%	Spruce-Pine-Fir
B2 Column		834 lbs	33.6%	22.3%	Unspecified

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

CONFORMS TO OBG 2012

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86. AMENDED 2020 BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9



DWG NO. TAW 71191-20 STRUGTURAL

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BC CALC®, BC FRAMER®, 'AJS™, ALLJOIST®, BC RIM BOARD™, BCI®, BOISE GLULAM™, BC FloorValue®, VERSA-LAM®, VERSA-RIM PLUS®,





Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

1ST FLR FRAMING\Flush Beams\B3 H(i3204) (Flush Beam)

Dry | 1 span | No cant.

June 12, 2020 15:19:25

Build 7493

Job name:

Address:

BC CALC® Member Report

City, Province, Postal Code: MARKHAM

Customer: Code reports:

CCMC 12472-R

File name:

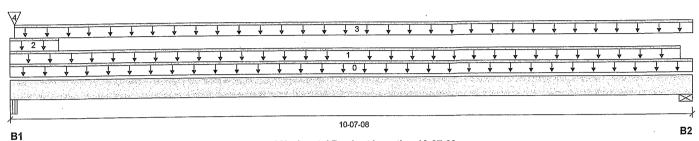
PEYTON 3 - EL 1,2,3.mmdl

Description: 1ST FLR FRAMING\Flush Beams\B3 H(i3204)

Specifier:

Designer: L.D.

Company:



Total Horizontal Product Length = 10-07-08

ction Summary (Down / Unlift) (lbs)

Reaction Jun	Illialy (Down of	Jilit) (185)			
Bearing	Live	Dead	Snow	Wind	
B1, 4-3/8"	3442 / 0	2345 / 0			
B2. 2-3/8"	177 / 0	546 / 0			

Los	ad Summary						Live	Dead	Snow	Wind	Tributary
	Description	Load Type	Ref.	Start	End	Loc.	1.00	0.65	1.00	1.15	
0	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	10-07-08	Тор		10			00-00-00
1	29(i2648)	Unf. Lin. (lb/ft)	L	00-00-00	10-05-02	Тор		81			n\a
2	29(i2648)	Unf. Lin. (lb/ft)	L	00-00-00	00-08-14	Top	759	404			n\a
3	FC4 Floor Material	Unf. Lin. (lb/ft)	L	00-00-14	10-07-08	Top	33	16			n\a
4	29(i2648)	Conc. Pt. (lbs)	L	00-00-14	00-00-14	Тор	2716	1475			n\a

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	1966 ft-lbs	15093 ft-lbs	13.0%	0	05-04-12
End Shear	1372 lbs	11571 lbs	11.9%	1	01-01-14
Total Load Deflection	L/999 (0.07")	n\a	n\a	4	05-04-12
Live Load Deflection	L/999 (0.017")	n\a	n\a	5	05-03-03
Max Defl.	0.07"	n\a	n\a	4	05-04-12
Span / Depth	12.9				

Deevi	an Supports	Div. (L.181)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
bearii	ng Supports	Dim. (LXVV)				
B1	Beam	4-3/8" x 3-1/2"	8094 lbs	99.0%	43.3%	Unspecified
D I					4.4.007	O D: F:
B2	Wall/Plate	2-3/8" x 3-1/2"	765 lbs	23.0%	11.6%	Spruce-Pine-Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced. Resistance Factor phi has been applied to all presented results per CSA O86.

CONFORMS TO OBG 2012

Resistance Factor phi has been applied to all presented results per CSA O86. AMENDED 2020 BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9



DWW NO. TAN 11192-20 STRUCTURAL COMPONENT ONLY



BC CALC® Member Report



Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1ST FLR FRAMING\Flush Beams\B3 H(i3204) (Flush Beam)

PASSED

Dry | 1 span | No cant.

June 12, 2020 15:19:25

Build 7493

Job name:

Customer:

Code reports:

Address:

City, Province, Postal Code: MARKHAM

CCMC 12472-R

File name:

PEYTON 3 - EL 1,2,3.mmdl

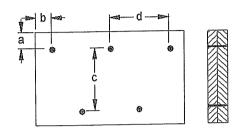
1ST FLR FRAMING\Flush Beams\B3 H(i3204) Description:

Specifier:

L.D. Designer:

Company:

Connection Diagram: Full Length of Member



a minimum = 2" b minimum = 3"

c = 5-1/2" d = 20' 6 4

Connectors are:

ાં હેંગ Nails

ARDOX SPIKAL



OWE NO. TAM 1/19220 STRUCTURAL COMPONENT ONLY

Disclosure

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BC CALC®, BC FRAMER®, AJS™, ALLJOIST®, BC RIM BOARD™, BCI®, BOISE GLULAM™, BC FloorValue®, VERSA-LAM®, VERSA-RIM PLUS®,





Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

June 12, 2020 15:19:25

1ST FLR FRAMING\Flush Beams\B4 L(i3488) (Flush Beam)

BC CALC® Member Report

Build 7493 Job name:

Address:

City, Province, Postal Code: MARKHAM

Customer:

Code reports:

Dry | 1 span | No cant.

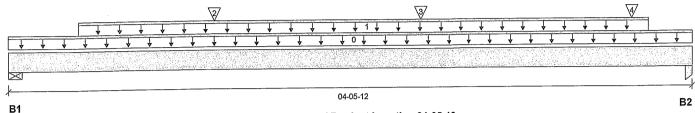
PEYTON 3 - EL 1,2,3.mmdl

File name: 1ST FLR FRAMING\Flush Beams\B4 L(i3488) Description:

Specifier:

Designer: L.D.

Company:



Total Horizontal Product Length = 04-05-12

Snow

Reaction Summary (Down / Uplift) (lbs)

Reaction Sum	IIII IIII Y	
Bearing	Live	Dead
B1, 5-1/2"	771 / 0	397 / 0
B2. 3-1/2"	888 / 0	455 / 0

CCMC 12472-R

1.00	ad Summary						Live	Dead	Snow	Wind	Tributary
Tag		Load Type	Ref.	Start	End	Loc.	1.00	0.65	1.00	1.15	
nag	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	04-05-12	Тор		5			00-00-00
1	STAIRS	Unf. Lin. (lb/ft)	L	00-05-08	04-02-04	Top	240	120			n\a
2	J2(i3492)	Conc. Pt. (lbs)	L	01-04-00	01-04-00	Top	267	134			n\a
2	, ,	Conc. Pt. (lbs)	1.	02-08-00	02-08-00	Top	267	134			n\a
3	J2(i3631)	Conc. Pt. (lbs)	ī	04-00-15	04-00-15	Top	230	115	7080FE	351()A	n\a
4	-	COILC. F.L. (103)	L	04.00.10	010010	. 00			The state of the s		91

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	1735 ft-lbs	11610 ft-lbs	14.9%	1	02-06-08
End Shear	1242 lbs	5785 lbs	21.5%	1	01-03-00
Total Load Deflection	L/999 (0.013")	n\a	n∖a	4	02-04-00
Live Load Deflection	L/999 (0.009")	n\a	n\a	5	02-04-00
Max Defl.	0.013"	n\a	n\a	4	02-04-00
Span / Depth	4.9				

Rearing	ı Supports	Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B1	Wall/Plate	5-1/2" x 1-3/4"	1653 lbs	27.9%	14.1%	Spruce-Pine-Fir
B2	Column	3-1/2" x 1-3/4"	1901 lbs	38.2%	25.4%	Unspecified

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

CONFORMS TO OBC 2012

Calculations assume unbraced length of Top: 01-01-08, Bottom: 01-01-08.

Resistance Factor phi has been applied to all presented results per CSA O86. AMENDED 2020 BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

COMPONENT ONLY Disclosure

Use of the Boise Cascade Software is subject to the terms of the End User License Agreement (EULA). Completeness and accuracy of input must be reviewed and verified by a qualified engineer or other appropriate expert to assure its adequacy, prior to anyone relying on such output as evidence of suitability for a particular application. The output here is based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call (800)232-0788 before installation.

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DWG NO. TAM [/] STRUCTURAL



BC CALC® Member Report



Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

1ST FLR FRAMING\Flush Beams\B6(i3294) (Flush Beam)

Dry I 1 span | No cant.

June 12, 2020 15:19:25

Build 7493

Job name:

Address:

City, Province, Postal Code: MARKHAM

Customer: Code reports:

CCMC 12472-R

File name:

PEYTON 3 - EL 1,2,3.mmdl

Description:

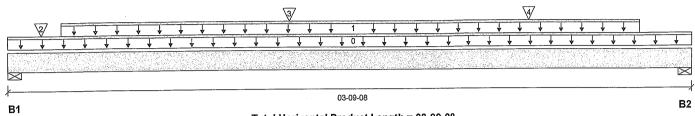
Wind

1ST FLR FRAMING\Flush Beams\B6(i3294)

Specifier:

Designer: L.D.

Company:



Total Horizontal Product Length = 03-09-08

Reaction Summary (Down / Uplift) (lbs)

Dead Live Bearing 412 / 0 772 / 0 B1, 3-1/2" 296 / 0 575 / 0 B2, 3-1/2"

10	ad Summary						Live	Dead	Snow	Wind	Tributary
	Description	Load Type	Ref.	Start	End	Loc.	1.00	0.65	1.00	1.15	
0	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	03-09-08	Тор		5			00-00-00
1	STAIRS	Unf. Lin. (lb/ft)	L	00-03-08	03-06-00	Тор	240	120			n\a
2	-	Conc. Pt. (lbs)	L	00-02-03	00-02-03	Top	254	144			n\a
3	J4(i3355)	Conc. Pt. (lbs)	L	01-06-08	01-06-08	Тор	159	79			n\a
<i>∆</i>	14(13373)	Conc. Pt. (lbs)	L	02-10-08	02-10-08	Тор	157	78			n\a

Controls Summary	Factored Demand	Resistance	Resistance	Case	Location
Pos. Moment	1059 ft-lbs	11610 ft-lbs	9.1%	1	01-09-02
End Shear	751 lbs	5785 lbs	13.0%	1	02-08-08
Total Load Deflection	L/999 (0.006")	n\a	n\a	4	01-10-14
Live Load Deflection	L/999 (0.004")	n\a	n\a	5	01-10-14
Max Defl.	0.006"	n\a	n\a	4	01-10-14
Span / Depth	4.2				

Bearing	g Supports	Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B1	Wall/Plate	3-1/2" x 1-3/4"	1673 lbs	44.4%	22.4%	Spruce-Pine-Fir
B2	Wall/Plate	3-1/2" x 1-3/4"	1233 lbs	32.7%	16.5%	Spruce-Pine-Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

CAMPORMS TO OBC 2012

Calculations assume member is fully braced.

AMENDED 2020 Resistance Factor phi has been applied to all presented results per CSA O86. BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9



Disclosure ONLY

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Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

June 12, 2020 15:19:25

1ST FLR FRAMING\Flush Beams\B5(i3330) (Flush Beam)

BC CALC® Member Report

Build 7493

Code reports:

Job name:

Address: City, Province, Postal Code: MARKHAM

Customer:

CCMC 12472-R

Dry | 1 span | No cant.

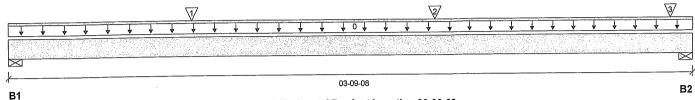
PEYTON 3 - EL 1,2,3.mmdl File name:

Description: 1ST FLR FRAMING\Flush Beams\B5(i3330)

Specifier:

L.D.

Designer: Company:



Total Horizontal Product Length = 03-09-08

Snow

Reaction Summary (Down / Uplift) (lbs)

Bearing	Live	Dead		
B1, 3-1/2"	208 / 0	113 / 0		
B2, 3-1/2"	339 / 0	179 / 0		

١.	ad Cummary						Live	Dead	Snow	Wind	Tributary
Tag	ad Summary Description	Load Type	Ref.	Start	End	Loc.	1.00	0.65	1.00	1.15	
∩	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	03-09-08	Тор		5			00-00-00
1	J4(i3301)	Conc. Pt. (lbs)	L	01-00-00	01-00-00	Top	180	90			n\a
2	J4(i3346)	Conc. Pt. (lbs)	L	02-04-00	02-04-00	Top	180	90			n\a
3	J4(i3335)	Conc. Pt. (lbs)	L	03-08-00	03-08-00	Тор	179	90			n\a

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	417 ft-lbs	11610 ft-lbs	3.6%	1	02-04-00
End Shear	405 lbs	5785 lbs	7.0%	1	01-01-00
Total Load Deflection	L/999 (0.002")	n\a	n\a	4	01-10-13
Live Load Deflection	L/999 (0.002")	n\a	n\a	5	01-10-13
Max Defl.	0.002"	n\a	n\a	4	01-10-13
Span / Depth	4.2				

Rearing	g Supports	Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B1	Wall/Plate	3-1/2" x 1-3/4"	453 lbs	12.0%	6.1%	Spruce-Pine-Fir
B2	Wall/Plate	3-1/2" x 1-3/4"	732 lbs	19.4%	9.8%	Spruce-Pine-Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86. AMENDED 2020 BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86. Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

CONFORMS TO OBG 2012

Disclosure ONLY Use of the Boise Cascade Software is subject to the terms of the End User License Agreement (EULA). Completeness and accuracy of input must be reviewed and verified by a qualified engineer or other appropriate expert to assure its adequacy, prior to anyone relying on such output as evidence of suitability for a particular application. The output here is based on building code-accepted design properties and analysis methods.

Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call (800)232-0788 before installation.

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Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 2ND FLR FRAMING\Flush Beams\B10(i3463) (Flush Beam)

PASSED

June 12, 2020 15:19:25

BC CALC® Member Report

Build 7493

Job name:

Address: City, Province, Postal Code: MARKHAM

Customer:

Code reports:

Dry | 1 span | No cant.

PEYTON 3 - EL 1,2,3.mmdl

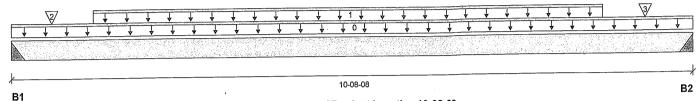
File name: Description: 2ND FLR FRAMING\Flush Beams\B10(i3463)

Wind

Specifier:

Designer: L.D.

Company:



Total Horizontal Product Length = 10-08-08

Snow

Reaction Summary (Down / Uplift) (lbs)

Bearing	Live	Dead		
B1, 3"	512 / 0	282 / 0		
B2, 3"	503 / 0	278 / 0		

CCMC 12472-R

8	and Crimensons						Live	Dead	Snow	Wind	Tributary
	.oad Summary ag Description	Load Type	Ref.	Start	End	Loc.	1.00	0.65	1.00	1.15	
<u> </u>	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	10-08-08	Тор		5			00-00-00
4	Smoothed Load	Unf. Lin. (lb/ft)	L	01-03-08	09-03-08	Top	100	50			n\a
1		Conc. Pt. (lbs)	1	00-07-09	00-07-09	Top	103	51			n\a
2	J3(i3852)			09-11-08	09-11-08	Top	108	54			n\a
3	J3(i3671)	Conc. Pt. (lbs)	L	09-11-00	09-11-00	τορ	100	0-7	2.00	والمعارضة المعارضة	

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	2908 ft-lbs	11610 ft-lbs	25.0%	1	05-11-04
End Shear	1010 lbs	5785 lbs	17.5%	1	09-08-00
Total Load Deflection	L/782 (0.159")	n\a	30.7%	4	05-03-06
Live Load Deflection	L/999 (0.102")	n\a	n\a	5	05-03-06
Max Defl.	0.159"	n\a	n\a	4	05-03-06
Span / Depth	13.1				

Rearin	g Supports	Dim (LXW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B1	Hanger	3" x 1-3/4"	1121 lbs	n\a	17.5%	HUS1.81/10
B2	Hanger	3" x 1-3/4"	1101 lbs	n\a	17.2%	HUS1.81/10

Header for the hanger HUS1.81/10 is a Single 1-3/4" x 9-1/2" LVL Beam.

Hanger model HUS1.81/10 and seat length were input by the user. Hanger has not been analyzed for adequate capacity.

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume unbraced length of Top: 00-00-00, Bottom: 00-00-00:

Hanger Manufacturer: Unassigned

Resistance Factor phi has been applied to all presented results per CSA O86.

AWENDED 2020

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9



DWG NO. TAM LI STRUCTURAL COMPONENT ONLY

Disclosure

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Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

June 12, 2020 15:19:25

2ND FLR FRAMING\Flush Beams\B11(i3616) (Flush Beam)

BC CALC® Member Report

Build 7493

Job name:

Address:

City, Province, Postal Code: MARKHAM

Customer: Code reports:

CCMC 12472-R

Dry | 1 span | No cant.

File name:

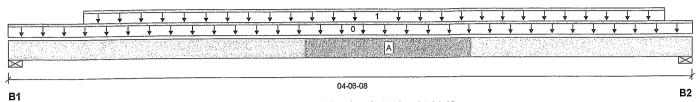
PEYTON 3 - EL 1,2,3.mmdl

Description: 2ND FLR FRAMING\Flush Beams\B11(i3616)

Specifier:

Designer: L.D.

Company:



Total Horizontal Product Length = 04-06-08

Snow

Reaction Summary (Down / Uplift) (lbs)

Bearing	Live	Dead			
B1, 3-1/2"	581 / 0	312 / 0			
B2, 2-3/4"	671 / 0	357 / 0			

	ad Summary Description	Load Type	Ref.	Start	End	Loc.	Live 1.00	Dead 0.65	Snow 1.00	Wind 1.15	Tributary
0	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	04-06-08	Тор		10			00-00-00
1	Smoothed Load	Unf. Lin. (lb/ft)	L	00-06-00	04-04-04	Top	324	162			n\a

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	1497 ft-lbs	23220 ft-lbs	6.4%	1	02-04-04
End Shear	1178 lbs	11571 lbs	10.2%	1	01-01-00
Total Load Deflection	L/999 (0.006")	n\a	n\a	6	02-03-11
Live Load Deflection	L/999 (0.004")	n\a	n\a	8	02-03-11
Max Defl.	0.006"	n\a	n\a	6	02-03-11
Span / Depth	5.2				

B	searing Supports	Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
В		3-1/2" x 3-1/2"	1262 lbs	16.7%	8.4%	Spruce-Pine-Fir
В	2 Wall/Plate	2-3/4" x 3-1/2"	1454 lbs	24.6%	12.4%	Spruce-Pine-Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

CONFORMS TO OBC 2012

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

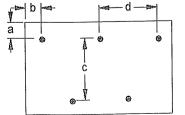
AMENDED 2020

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

Connection Diagram: Full Length of Member











Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

2ND FLR FRAMING\Flush Beams\B11(i3616) (Flush Beam)

Dry | 1 span | No cant.

June 12, 2020 15:19:25

Build 7493

Job name:

Address: City, Province, Postal Code: MARKHAM

BC CALC® Member Report

Customer: Code reports:

CCMC 12472-R

File name:

PEYTON 3 - EL 1,2,3.mmdl

Description: 2ND FLR FRAMING\Flush Beams\B11(i3616)

Specifier:

Designer:

Company:

Connection Diagram: Full Length of Member

a minimum = 2"

c = 5-1/2"

b minimum = 3"

d = 2 8"

Calculated Side Load = 225.3 lb/ft

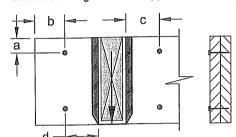
Connectors are:

e: 3%" ARDOX SPIRAL

Connection Diagrams: Concentrated Side Loads

Connection Tag: A

Applies to load tag(s): 4+5+6



a minimum = 2"

b minimum = 4"

c minimum = 4"

d maximum = 12"

Connectors are: Nails

31/2" ARDOX SPIKAL



Disclosure

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BC CALC® Member Report



Triple 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

2ND FLR FRAMING\Flush Beams\B7(i3851) (Flush Beam)

Dry I 1 span I No cant.

June 12, 2020 15:19:25

Build 7493

Job name:

Customer:

Code reports:

Address: City, Province, Postal Code: MARKHAM

CCMC 12472-R

File name:

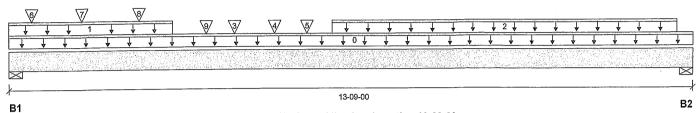
PEYTON 3 - EL 1,2,3.mmdl

Description: 2ND FLR FRAMING\Flush Beams\B7(i3851)

Specifier:

Designer:

L.D. Company:



Total Horizontal Product Length = 13-09-00

Reaction Summary (Down / Uplift) (lbs)

Bearing	Live	Dead
B1, 2-3/4"	2722 / 0	1478 / 0
B2, 3-1/2"	3150 / 0	1686 / 0

l o	ad Summary						Live	Dead	Snow	Wind	Tributary
	Description	Load Type	Ref.	Start	End	Loc.	1.00	0.65	1.00	1.15	
0	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	13-09-00	Тор		14			00-00-00
1	Smoothed Load	Unf. Lin. (lb/ft)	L	00-00-00	03-03-00	Тор	127	63			n\a
2	Smoothed Load	Unf. Lin. (lb/ft)	L	06-05-00	13-05-00	Тор	505	253			n\a
3	J3(i3671)	Conc. Pt. (lbs)	L	04-05-12	04-05-12	Тор	111	55			n\a
4	-	Conc. Pt. (lbs)	L	05-03-06	05-03-06	Top	611	337			n\a
5	J1(i3850)	Conc. Pt. (lbs)	L	05-11-00	05-11-00	Top	215	107			n\a
6	J2(i3764)	Conc. Pt. (lbs)	Ĺ	00-05-08	00-05-08	Top	213	107			n\a
7	J2(i3763)	Conc. Pt. (lbs)	L	01-05-08	01-05-08	Top	226	113			n\a
8	J2(i3674)	Conc. Pt. (lbs)	L	02-07-00	02-07-00	Top	262	131			n\a
9	J2(i3807)	Conc. Pt. (lbs)	L	03-11-00	03-11-00	Top	284	142			n\a

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	21945 ft-lbs	36222 ft-lbs	60.6%	1	06-11-00
End Shear	6192 lbs	17356 lbs	35.7%	1	12-08-00
Total Load Deflection	L/244 (0.657")	n\a	98.4%	4	06-11-00
Live Load Deflection	L/376 (0.427")	n\a	95.8%	5	06-11-00
Max Defl.	0.657"	n\a	n\a	4	06-11-00
Span / Depth	16.9		•		

Bea	aring Supports	Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material	_
B1	Wall/Plate	2-3/4" x 5-1/4"	5932 lbs	66.8%	33.7%	Spruce-Pine-Fir	-
B2	Wall/Plate	3-1/2" x 5-1/4"	6832 lbs	60.4%	30.5%	Spruce-Pine-Fir	

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

CONFORMS TO OBC 2012

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

AMENDED 2020

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA 086.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

OVINCE OF ON THE DWB HO. TAN 1/198 -20 STRUCTURAL COMPONENT ONLY



BC CALC® Member Report



Triple 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 2ND FLR FRAMING\Flush Beams\B7(i3851) (Flush Beam)

Passed

Dry I 1 span I No cant.

June 12, 2020 15:19:25

Build 7493

Job name:

Address:

City, Province, Postal Code: MARKHAM

Customer:

Code reports:

CCMC 12472-R

File name:

PEYTON 3 - EL 1,2,3.mmdl

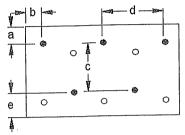
Description: 2ND FLR FRAMING\Flush Beams\B7(i3851)

Specifier:

Designer: L.D.

Company:

Connection Diagram: Full Length of Member





a minimum = 🛍 " b minimum = 3"

c = 6.1/2" d = @ B" e minimum = 2"

Calculated Side Load = 873.6 lb/ft Nailing applies to both sides of the member Connectors are: 16d A : Nails

36" ARDOX SPIKAL



DVB NO. YAN 11198-20 STRUCTURAL COMPONENT ONLY

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Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

2ND FLR FRAMING\Flush Beams\B8(i3415) (Flush Beam)

Dry I 1 span I No cant.

June 12, 2020 15:19:25

Build 7493

Job name:

Address: City, Province, Postal Code: MARKHAM

BC CALC® Member Report

File name: Description:

Specifier:

Designer: L.D.

Wind

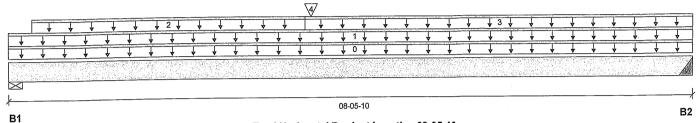
PEYTON 3 - EL 1,2,3.mmdl

2ND FLR FRAMING\Flush Beams\B8(i3415)

Customer: Code reports:

CCMC 12472-R

Company:



Total Horizontal Product Length = 08-05-10

Reaction Sun	nmary (Down / O	piiit) (ibə)	
Bearing	Live	Dead	Snow
B1. 3-1/2"	385 / 0	228 / 0	
B2, 3"	332 / 0	198 / 0	

(Down / Unlift) (lbe)

10	ad Summary						Live	Dead	Snow	Wind	Tributary
LO ₆	•	Load Type	. Ref.	Start	End	Loc.	1.00	0.65	1.00	1.15	
0	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	08-05-10	Тор		5			00-00-00
1	FC6 Floor Material	Unf. Lin. (lb/ft)	L	00-00-00	08-05-10	Тор	12	6			n\a
2	FC6 Floor Material	Unf. Lin. (lb/ft)	L	00-03-08	03-07-08	Top	9	4			n\a
2	FC6 Floor Material	Unf. Lin. (lb/ft)	L	03-07-08	08-05-10	Тор	16	8		distance of the second	n\a
3 ⊿	B10(i3463)	Conc. Pt. (lbs)	Ĺ	03-08-06	03-08-06	Тор	503	278	AST TO SEE	HOLES	SIOA/q _e n\a
•	2.0(.0.00)	, ,	.	D	a.a.d1				10	in the same of the	

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	2655 ft-lbs	11610 ft-lbs	22.9%	1	03-08-06
End Shear	810 lbs	5785 lbs	14.0%	1	01-01-00
Total Load Deflection	L/999 (0.074")	n\a	n\a	4	04-01-04
Live Load Deflection	L/999 (0.047")	n\a	n\a	5	04-01-04
Max Defl.	0.074"	n\a	n\a	4	04-01-04
Span / Depth	10.2			,	

Bearing	a Supports	Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B1	Wall/Plate	3-1/2" x 1-3/4"	863 lbs	22.9%	11.5%	Spruce-Pine-Fir
B2	Hanger	3" x 1-3/4"	746 lbs	n\a	11.6%	HUS1.81/10

Cautions

Header for the hanger HUS1.81/10 is a Triple 1-3/4" x 9-1/2" LVL Beam.

Hanger model HUS1.81/10 and seat length were input by the user. Hanger has not been analyzed for adequate capacity.

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

CONFORMS TO OBC 2012

Hanger Manufacturer: Unassigned AMENDED 2020 Resistance Factor phi has been applied to all presented results per CSA O86. BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86.

Design based on Dry Service Condition.

1.4

Importance Factor: Normal Part code: Part 9

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COMPONENT



BC CALC® Member Report



Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

PASSED

2ND FLR FRAMING\Flush Beams\B9(i3785) (Flush Beam)

Dry | 1 span | No cant.

June 12, 2020 15:19:25

Build 7493

Job name:

Address: City, Province, Postal Code: MARKHAM

Customer: Code reports:

CCMC 12472-R

File name:

PEYTON 3 - EL 1,2,3.mmdl

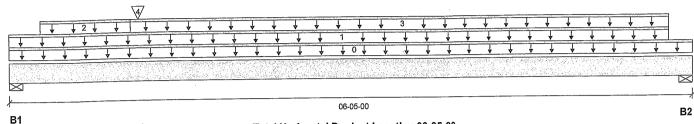
2ND FLR FRAMING\Flush Beams\B9(i3785) Description:

Wind

Specifier:

Designer: L.D.

Company:



Total Horizontal Product Length = 06-05-00

Snow

Reaction Summary (Down / Uplift) (lbs)

Live Dead Bearing 278/0 482 / 0 B1, 3-1/2" 94/0 147 / 0 B2. 5-1/2"

١٠٠	ad Summary						Live
	_	Load Type	Ref.	Start	End	Loc.	1.00
0	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	06-05-00	Top	
1	FC6 Floor Material	Unf. Lin. (lb/ft)	L	00-00-00	06-02-04	Top	6
1	FC6 Floor Material	Unf. Lin. (lb/ft)	L	00-03-08	01-01-08	Top	9
2		Unf. Lin. (lb/ft)	Ī	01-01-08	06-02-04	Top	14
3	FC6 Floor Material	•	-		01-02-06	Top	512
4	B10(i3463)	Conc. Pt. (lbs)	L	01-02-00	01-02-00	ιυρ	312

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	1014 ft-lbs	11610 ft-lbs	8.7%	1	01-02-06
End Shear	1033 lbs	5785 lbs	17.9%	1	01-01-00
Total Load Deflection	L/999 (0.014")	n\a	n\a	4	02-09-12
	L/999 (0.009")	n\a	n\a	5	02-09-12
Live Load Deflection	0.014"	n\a	n\a	4	02-09-12
Max Defl.	***	ma	1710		
Span / Depth	7.3				

Bearing Suppo	orts Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B1 Wall/Pla B2 Wall/Pla	ate 3-1/2" x 1-3/4		28.4% 5.7%	14.3% 2.9%	Spruce-Pine-Fir Spruce-Pine-Fir

Notes

Span / Depth

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

CONFORMS TO OBC 2012

Calculations assume member is fully braced.

AMENDED 2020 Resistance Factor phi has been applied to all presented results per CSA O86. BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2015 and CSA O86.

Design based on Dry Service Condition. Importance Factor: Normal Part code: Part 9

Dead Snow Wind **Tributary** 0.65 1.00 1.15 00-00-00 5 3 n∖a n\a 7 n\a 282 n∖a POWNICE OF ONIFE

DWG NO. TAM 1/200-20 STRUCTURAL COMPONENT ONLY

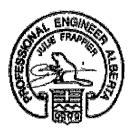
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Live Load = 40 psf, Dead Load = 15 psf Simple Spans, L/480 Deflection Limit 5/8" OSB G&N Sheathing







			Ва	are		1	1/2" Gyps	sum Ceiling	
Depth	Series		On Centr	e Spacing			On Centi	re Spacing	
		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	NI-20	15'-1"	14'-2"	13'-9"	N/A	15'-7"	14'-8"	14'-2"	N/A
	NI-40x	16'-1"	15'-2"	14'-8"	N/A	16'-7"	15'-7"	15'-1"	N/A
9-1/2"	NI-60	16'-3"	15'-4"	14'-10"	N/A	16'-8"	15'-9"	15'-3"	N/A
•	NI-70	17'-1"	16'-1"	15'-6"	N/A	17'-5"	16'-5"	15'-10"	N/A
	NI-80	17'-3"	16'-3"	15'-8"	N/A	17'-8"	16'-7"	16'-0"	N/A
	NI-20	16'-11"	16'-0"	15'-5"	N/A	17'-6"	16'-6"	16'-0"	N/A
	NI-40x	18'-1"	17'-0"	16'-5"	N/A	18'-9"	17'-6"	16'-11"	N/A
- 1- 11	NI-60	18'-4"	17'-3"	16'-7"	N/A	19'-0"	17'-8"	17'-1"	N/A
11-7/8"	NI-70	19'-6"	18'-0"	17'-4"	N/A	20'-1"	18'-7"	17'-9"	N/A
	NI-80	19'-9"	18'-3"	17'-6"	N/A	20'-4"	18'-10"	17'-11"	N/A
	NI-90x	20'-4"	18'-9"	17'-11"	N/A	20'-10"	19'-3"	18'-5"	N/A
	NI-40x	20'-1"	18'-7"	17'-10"	N/A	20'-10"	19'-4"	18'-6"	N/A
	NI-60	20'-5"	18'-11"	18'-1"	N/A	21'-2"	19'-7"	18'-9"	N/A
14"	NI-70	21'-7"	20'-0"	19'-1"	N/A	22'-3"	20'-7"	19'-8"	N/A
	NI-80	21'-11"	20'-3"	19'-4"	N/A	22'-7"	20'-11"	20'-0"	N/A
	NI-90x	22'-7"	20'-11"	19'-11"	N/A	23'-3"	21'-6"	20'-6"	N/A
	NI-60	22'-3"	20'-8"	19'-9"	N/A	23'-1"	21'-5"	20'-6"	N/A
	NI-70	23'-6"	21'-9"	20'-9"	N/A	24'-3"	22'-5"	21'-5"	N/A
16"	NI-80	23'-11"	22'-1"	21'-1"	N/A	24'-8"	22'-10"	21'-9"	N/A
	NI-90x	24'-8"	22'-9"	21'-9"	N/A	25'-4"	23'-5"	22'-4"	N/A

			Mid-Spar	n Blocking		Mid-S	pan Blocking ar	id 1/2" Gypsum	Ceiling	
Depth	Series	Series On Centre Spacing				On Centre Spacing				
		12"	16"	19.2"	24"	12"	16"	19.2"	24"	
	NI-20	16'-8"	15'-3"	14'-5"	N/A	16'-8"	15'-3"	14'-5"	N/A	
	NI-40x	17'-11"	16'-11"	16'-1"	N/A	18'-5"	17'-1"	16'-1"	N/A	
9-1/2"	NI-60	18'-2"	17'-1"	16'-4"	N/A	18'-7"	17'-4"	16'-4"	N/A	
, -	NI-70	19'-2"	17'-10"	17'-2"	N/A	19'-7"	18'-3"	17'-7"	N/A	
	NI-80	19'-5"	18'-0"	17'-4"	N/A	19'-10"	18'-5"	17'-8"	N/A	
	NI-20	19'-6"	18'-1"	17'-3"	N/A	19'-11"	18'-3"	17'-3"	N/A	
	NI-40x	21'-0"	19'-6"	18'-8"	N/A	21'-7"	20'-2"	19'-2"	N/A	
	NI-60	21'-4"	19'-9"	18'-11"	N/A	21'-11"	20'-4"	19'-6"	N/A	
11-7/8"	NI-70	22'-6"	20'-10"	19'-11"	N/A	23'-0"	21'-5"	20'-5"	N/A	
	NI-80	22'-9"	21'-1"	20'-1"	N/A	23'-3"	21'-7"	20'-8"	N/A	
	NI-90x	23'-4"	21'-8"	20'-8"	N/A	23'-10"	22'-2"	21'-2"	N/A	
	NI-40x	23'-7"	21'-11"	20'-11"	N/A	24'-3"	22'-7"	21'-7"	N/A	
	NI-60	24'-0"	22'-3"	21'-3"	N/A	24'-8"	22'-11"	21'-11"	N/A	
14"	NI-70	25'-3"	23'-4"	22'-3"	N/A	25'-10"	24'-0"	22'-11"	N/A	
	NI-80	25'-7"	23'-8"	22'-7"	N/A	26'-2"	24'-4"	23'-2"	N/A	
	NI-90x	26'-4"	24'-4"	23'-3"	N/A	26'-10"	24'-11"	23'-9"	N/A	
	NI-60	26'-5"	24'-6"	23'-4"	N/A	27'-2"	25'-3"	24'-2"	N/A	
_	NI-70	27'-9"	25'-8"	24'-6"	N/A	28'-5"	26'-5"	25'-2"	N/A	
16"	NI-80	28'-2"	26'-1"	24'-10"	N/A	28'-10"	26'-9"	25'-6"	N/A	
	NI-90x	29'-0"	26'-10"	25'-7"	N/A	29'-7"	27'-5"	26'-2"	N/A	

^{1.} Maximum clear span applicable to simple-span residential floor construction with a design live load of 40 psf and dead load of 15 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration for floor vibration, a live load deflection limit of L/480 and a total load deflection limit of L/240.

^{2.} Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum thickness of 5/8 inch for a joist spacing of 19.2 inches or less. The composite floor may include 1/2 inch gypsum ceiling and/or one row of blocking at mid-span with strapping. Strapping shall be minimum 1x4 inch strap applied to underside of joists at blocking line or 1/2 inch gypsum ceiling attached to joists.

^{3.} Minimum bearing length shall be 1-3/4 inches for the end bearings.

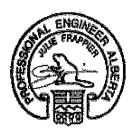
^{4.} Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.

^{5.} This span chart is based on uniform loads. For applications with other than uniformly distributed loads, an engineering analysis may be required based on the use of the design properties. Tables are based on Limit States Design per CSA O86-09, NBC 2010, and OBC 2012.

^{6.} Joists shall be laterally supported at supports and continuously along the compression edge. Refer to technical documentation for installation guidelines and construction details. Nordic I-joists are listed in CCMC evaluation report 13032-R and APA Product Report PR-L274C.



Live Load = 40 psf, Dead Load = 15 psf Simple Spans, L/480 Deflection Limit 3/4" OSB G&N Sheathing







Depth	Series		Ва	are		1/2" Gypsum Ceiling On Centre Spacing				
			On Centr	e Spacing						
		12"	16"	19.2"	24"	12"	16"	19.2"	24"	
	NI-20	15'-10"	15'-0"	14'-5"	13'-5"	16'-4"	15'-5"	14'-6"	13'-5"	
	NI-40x	17'-0"	16'-0"	15'-5"	14'-9"	17'-5"	16'-5"	15'-10"	15'-2"	
9-1/2"	NI-60	17'-2"	16'-2"	15'-7"	14'-11"	17'-6"	16'-7"	15'-11"	15'-3"	
- ,	NI-70	18'-0"	16'-11"	16'-3"	15'-7"	18'-5"	17'-3"	16'-7"	15'-11"	
	NI-80	18'-3"	17'-1"	16'-5"	15'-9"	18'-8"	17'-5"	16'-9"	16'-1"	
	NI-20	17'-10"	16'-10"	16'-2"	15'-6"	18'-6"	17'-4"	16'-9"	16'-1"	
	N1-40x	19'-4"	17'-11"	17'-3"	16'-6"	19'-11"	18'-6"	17'-9"	17'-0"	
	NI-60	19'-7"	18'-2"	17'-5"	16'-9"	20'-2"	18'-9"	17'-11"	17'-2"	
11-7/8"	NI-70	20'-9"	19'-2"	18'-3"	17'-5"	21'-4"	19'-9"	18'-10"	17'-10"	
	NI-80	21'-1"	19'-5"	18'-6"	17'-7"	21'-7"	20'-0"	19'-0"	18'-0"	
	NI-90x	21'-8"	20'-0"	19'-1"	18'-0"	22'-2"	20'-6"	19'-6"	18'-6"	
	NI-40x	21'-5"	19'-10"	18'-11"	17'-11"	22'-1"	20'-6"	19'-7"	18'-7"	
	NI-60	21'-10"	20'-2"	19'-3"	18'-2"	22'-5"	20'-10"	19'-11"	18'-10"	
14"	NI-70	23'-0"	21'-3"	20'-3"	19'-2"	23'-8"	21'-11"	20'-10"	19'-9"	
	NI-80	23'-5"	21'-7"	20'-7"	19'-5"	24'-0"	22'-3"	21'-2"	20'-0"	
	NI-90x	24'-1"	22'-3"	21'-2"	20'-0"	24'-8"	22'-10"	21'-9"	20'-7"	
	NI-60	23'-9"	22'-0"	20'-11"	19'-10"	24'-6"	22'-9"	21'-8"	20'-6"	
	NI-70	25'-1"	23'-2"	22'-0"	20'-10"	25'-9"	23'-10"	22'-9"	21'-6"	
16"	NI-80	25'-6"	23'-6"	22'-4"	21'-2"	26'-1"	24'-2"	23'-1"	21'-10"	
	NI-90x	26'-4"	24'-3"	23'-1"	21'-10"	26'-11"	24'-11"	23'-8"	22'-5"	

	Series		Mid-Spar	n Blocking		Mid-Span Blocking and 1/2" Gypsum Ceiling				
Depth			On Centr	e Spacing	On Centre Spacing					
		12"	16"	19.2"	24"	12"	16"	19.2"	24"	
	NI-20	16'-10"	15'-5"	14'-6"	13'-5"	16'-10"	15'-5"	14'-6"	13'-5"	
	NI-40x	18'-8"	17'-2"	16'-3"	15'-2"	18'-10"	17'-2"	16'-3"	15'-2"	
9-1/2"	NI-60	18'-11"	17'-6"	16'-6"	15'-5"	19'-2"	17'-6"	16'-6"	15'-5"	
3 2,2	NI-70	20'-0"	18'-7"	17'-9"	16'-7"	20'-5"	18'-11"	17'-10"	16'-7"	
	N1-80	20'-3"	18'-10"	17'-11"	16'-10"	20'-8"	19'-3"	18'-2"	16'-10"	
	NI-20	20'-1"	18'-5"	17'-5"	16'-2"	20'-1"	18'-5"	17'-5"	16'-2"	
	N1-40x	21'-10"	20'-4"	19'-4"	17'-8"	22'-5"	20'-6"	19'-4"	17'-8"	
	NI-60	22'-1"	20'-7"	19'-7"	18 - 4"	22'-8"	20'-10"	19'-8"	18'-4"	
11-7/8"	NI-70	23'-4"	21'-8"	20'-8"	19'-7"	23'-10"	22'-3"	21'-2"	19'-9"	
	NI-80	23'-7"	21'-11"	20'-11"	19'-9"	24'-1"	22'-6"	21'-5"	20'-0"	
	NI-90x	24'-3"	22'-6"	21'-6"	20'-4"	24'-8"	23'-0"	22'-0"	20'-9"	
	NI-40x	24'-5"	22'-9"	21'-8"	19'-5"	25'-1"	23'-2"	21'-9"	19'-5"	
	NI-60	24'-10"	23'-1"	22'-0"	20'-10"	25'-6"	23'-8"	22'-4"	20'-10"	
14"	NI-70	26'-1"	24'-3"	23'-2"	21'-10"	26'-8"	24'-11"	23'-9"	22'-4"	
4.7	NI-80	26'-6"	24'-7"	23'-5"	22'-2"	27'-1"	25'-3"	24'-1"	22'-9"	
	NI-90x	27'-3"	25'-4"	24'-1"	22'-9"	27'-9"	25'-11"	24'-8"	23'-4"	
	NI-60	27'-3"	25'-5"	24'-2"	22'-10"	28'-0"	26'-2"	24'-9"	23'-1"	
	NI-70	28'-8"	26'-8"	25'-4"	23'-11"	29'-3"	27'-4"	26'-1"	24'-8"	
16"	NI-80	29'-1"	27'-0"	25'-9"	24'-4"	29'-8"	27'-9"	26'-5"	25'-0"	
	NI-90x	29'-11"	27'-10"	26'-6"	25'-0"	30'-6"	28'-5"	27'-2"	25'-8"	

^{1.} Maximum clear span applicable to simple-span residential floor construction with a design live load of 40 psf and dead load of 15 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration for floor vibration, a live load deflection limit of L/480 and a total load deflection limit of L/240.

^{2.} Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum thickness of 3/4 inch for a joist spacing of 24 inches or less. The composite floor may include 1/2 inch gypsum ceiling and/or one row of blocking at mid-span with strapping. Strapping shall be minimum 1x4 inch strap applied to underside of joists at blocking line or 1/2 inch gypsum ceiling attached to joists.

3. Minimum bearing length shall be 1-3/4 inches for the end bearings.

^{4.} Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.

^{5.} This span chart is based on uniform loads. For applications with other than uniformly distributed loads, an engineering analysis may be required based on the use of the design properties. Tables are based on Limit States Design per CSA O86-09, NBC 2010, and OBC 2012.

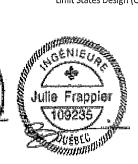
^{6.} Joists shall be laterally supported at supports and continuously along the compression edge. Refer to technical documentation for installation guidelines and construction details. Nordic I-joists are listed in CCMC evaluation report 13032-R and APA Product Report PR-L274C.



Live Load = 40 psf, Dead Load = 30 psf Simple Spans, L/480 Deflection Limit 5/8" OSB G&N Sheathing







	Series		Ва	are	1/2" Gypsum Ceiling On Centre Spacing				
Depth			On Centr	e Spacing					
		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	NI-20	15'-1"	14'-1"	13'-3"	N/A	15'-7"	14'-1"	13'-3"	N/A
	NI-40x	16'-1"	15'-2"	14'-8"	N/A	16'-7"	15'-7"	15'-1"	N/A
9-1/2"	NI-60	16'-3"	15'-4"	14'-10"	N/A	16'-8"	15'-9"	15'-3"	N/A
	NI-70	17'-1"	16'-1"	15'-6"	N/A	17'-5"	16'-5"	15'-10"	N/A
	NI-80	17'-3"	16'-3"	15'-8"	N/A	17'-8"	16'-7"	16'-0"	N/A
	NI-20	16'-11"	16'-0"	15'-5"	N/A	17'-6"	16'-6"	16'-0"	N/A
	NI-40x	18'-1"	17'-0"	16'-5"	N/A	18'-9"	17'-6"	16'-11"	N/A
	NI-60	18'-4"	17'-3"	16'-7"	N/A	19'-0"	17'-8"	17'-1"	N/A
11-7/8"	NI-70	19'-6"	18'-0"	17'-4"	N/A	20'-1"	18'-7"	17'-9"	N/A
	NI-80	19'-9"	18'-3"	17'-6"	N/A	20'-4"	18'-10"	17'-11"	N/A
	NI-90x	20'-4"	18'-9"	17'-11"	N/A	20'-10"	19'-3"	18'-5"	N/A
	NI-40x	20'-1"	18'-7"	17'-10"	N/A	20'-10"	19'-4"	18'-6"	N/A
	NI-60	20'-5"	18'-11"	18'-1"	N/A	21'-2"	19'-7"	18'-9"	N/A
14"	NI-70	21'-7"	20'-0"	19'-1"	N/A	22'-3"	20'-7"	19'-8"	N/A
	NI-80	21'-11"	20'-3"	19'-4"	N/A	22'-7"	20'-11"	20'-0"	N/A
	NI-90x	22'-7"	20'-11"	19'-11"	N/A	23'-3"	21'-6"	20'-6"	N/A
	NI-60	22'-3"	20'-8"	19'-9"	N/A	23'-1"	21'-5"	20'-6"	N/A
	NI-70	23'-6"	21'-9"	20'-9"	N/A	24'-3"	22'-5"	21'-5"	N/A
16"	NI-80	23'-11"	22'-1"	21'-1"	N/A	24'-8"	22'-10"	21'-9"	N/A
•	NI-90x	24'-8"	22'-9"	21'-9"	N/A	25'-4"	23'-5"	22'-4"	N/A

Depth	Series		Mid-Spar	n Blocking	Mid-Span Blocking and 1/2" Gypsum Ceiling On Centre Spacing				
			On Centr	e Spacing					
1		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	NI-20	15'-7"	14'-1"	13'-3"	N/A	15'-7"	14'-1"	13'-3"	N/A
	NI-40x	17'-9"	16'-1"	15'-1"	N/A	17'-9"	16'-1"	15'-1"	N/A
9-1/2"	NI-60	18'-1"	16'-4"	15'-4"	N/A	18'-1"	16'-4"	15'-4"	N/A
-,-	NI-70	19'-2"	17'-10"	16'-9"	N/A	19'-7"	17'-10"	16'-9"	N/A
	NI-80	19'-5"	18'-0"	17'-1"	N/A	19'-10"	18'-3"	17'-1"	N/A
	NI-20	18'-9"	17'-0"	16'-0"	N/A	18'-9"	17'-0"	16'-0"	N/A
	NI-40x	21'-0"	19'-3"	17'-9"	N/A	21'-3"	19'-3"	17'-9"	N/A
	NI-60	21'-4"	19'-8"	18'-5"	N/A	21'-8"	19'-8"	18'-5"	N/A
11-7/8"	NI-70	22'-6"	20'-10"	19'-11"	N/A	23'-0"	21'-4"	20'-0"	N/A
	NI-80	22'-9"	21'-1"	20'-1"	N/A	23'-3"	21'-7"	20'-5"	N/A
	NI-90x	23'-4"	21'-8"	20'-8"	N/A	23'-10"	22'-2"	21'-2"	N/A
	NI-40x	23'-7"	21'-5"	19'-6"	N/A	24'-1"	21'-5"	19'-6"	N/A
	NI-60	24'-0"	22'-3"	21'-0"	N/A	24'-8"	22'-5"	21'-0"	N/A
14"	NI-70	25'-3"	23'-4"	22'-3"	N/A	25'-10"	24'-0"	22'-9"	N/A
	NI-80	25'-7"	23'-8"	22'-7"	N/A	26'-2"	24'-4"	23'-2"	N/A
	NI-90x	26'-4"	24'-4"	23'-3"	N/A	26'-10"	24'-11"	23'-9"	N/A
	NI-60	26'-5"	24'-6"	23'-4"	N/A	27'-2"	24'-10"	23'-4"	N/A
	NI-70	27'-9"	25'-8"	24'-6"	N/A	28'-5"	26'-5"	25'-2"	N/A
16"	NI-80	28'-2"	26'-1"	24'-10"	N/A	28'-10"	26'-9"	25'-6"	N/A
	NI-90x	29'-0"	26'-10"	25'-7"	N/A	29'-7"	27'-5"	26'-2"	N/A

^{1.} Maximum clear span applicable to simple-span residential floor construction with a design live load of 40 psf and dead load of 30 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration for floor vibration, a live load deflection limit of L/480 and a total load deflection limit of L/240.

^{2.} Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum thickness of 5/8 inch for a joist spacing of 19.2 inches or less. The composite floor may include 1/2 inch gypsum ceiling and/or one row of blocking at mid-span with strapping. Strapping shall be minimum 1x4 inch strap applied to underside of joists at blocking line or 1/2 inch gypsum ceiling attached to joists.

3. Minimum bearing length shall be 1-3/4 inches for the end bearings.

^{4.} Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.

^{5.} This span chart is based on uniform loads. For applications with other than uniformly distributed loads, an engineering analysis may be required based on the use of the design properties. Tables are based on Limit States Design per CSA O86-09, NBC 2010, and OBC 2012.

^{6.} Joists shall be laterally supported at supports and continuously along the compression edge. Refer to technical documentation for installation guidelines and construction details. Nordic I-joists are listed in CCMC evaluation report 13032-R and APA Product Report PR-L274C.



Live Load = 40 psf, Dead Load = 30 psf Simple Spans, L/480 Deflection Limit 3/4" OSB G&N Sheathing







			В	are		1/2" Gypsum Ceiling On Centre Spacing				
Depth	Series		On Centi	re Spacing						
		12"	16"	19.2"	24"	12"	16"	19.2"	24"	
	NI-20	15'-7"	14'-2"	13'-4"	12'-4"	15'-7"	14'-2"	13'-4"	12'-4"	
	NI-40x	17'-0"	16'-0"	15'-1"	13'-11"	17'-5"	16'-1"	15'-1"	13'-11"	
9-1/2"	NI-60	17'-2"	16'-2"	15'-5"	14'-3"	17'-6"	16'-5"	15'-5"	14'-3"	
	NI-70	18'-0"	16'-11"	16'-3"	15'-6"	18'-5"	17'-3"	16'-7"	15'-6"	
	NI-80	18'-3"	17'-1"	16'-5"	15'-9"	18'-8"	17'-5"	16'-9"	15'-10"	
	NI-20	17'-10"	16'-10"	16'-0."	14'-10"	18'-6"	17'-1"	16'-0"	14'-10"	
	NI-40x	19'-4"	17'-11"	17'-3"	15'-10"	19'-11"	18'-6"	17'-9"	15'-10"	
11 7/01	NI-60	19'-7"	18'-2"	17'-5"	16'-9"	20'-2"	18'-9"	17'-11"	17'-1"	
11-7/8"	NI-70	20'-9"	19'-2"	18'-3"	17'-5"	21'-4"	19'-9"	18'-10"	17'-10"	
	NI-80	21'-1"	19'-5"	18'-6"	17'-7"	21'-7"	20'-0"	19'-0"	18'-0"	
	NI-90x	21'-8"	20'-0"	19'-1"	18'-0"	22'-2"	20'-6"	19'-6"	18'-6"	
	N1-40x	21'-5"	19'-10"	18'-11"	17'-5"	22'-1"	20'-6"	19'-6"	17'-5"	
	NI-60	21'-10"	20'-2"	19'-3"	18'-2"	22'-5"	20'-10"	19'-11"	18'-10"	
14"	NI-70	23'-0"	21'-3"	20'-3"	19'-2"	23'-8"	21'-11"	20'-10"	19'-9"	
	NI-80	23'-5"	21'-7"	20'-7"	19'-5"	24'-0"	22'-3"	21'-2"	20'-0"	
	NI-90x	24'-1"	22'-3"	21'-2"	20'-0"	24'-8"	22'-10"	21'-9"	20'-7"	
	NI-60	23'-9"	22'-0"	20'-11"	19'-10"	24'-6"	22'-9"	21'-8"	20'-6"	
1.0"	NI-70	25'-1"	23'-2"	22'-0"	20'-10"	25'-9"	23'-10"	22'-9"	21'-6"	
16"	NI-80	25'-6"	23'-6"	22'-4"	21'-2"	26'-1"	24'-2"	23'-1"	21'-10"	
	NI-90x	26'-4"	24'-3"	23'-1"	21'-10"	26'-11"	24'-11"	23'-8"	22'-5"	

Depth	Series		Mid-Spar	n Blocking		Mid-Span Blocking and 1/2" Gypsum Ceiling On Centre Spacing				
			On Centr	e Spacing						
•		12"	16"	19.2"	24"	12"	16"	19.2"	24"	
	NI-20	15'-7"	14'-2"	13'-4"	12'-4"	15'-7"	14'-2"	13'-4"	12'-4"	
	NI-40x	17'-9"	16'-1"	15'-1"	13'-11"	17'-9"	16'-1"	15'-1"	13'-11"	
9-1/2"	NI-60	18'-1"	16'-5"	15'-5"	14'-3"	18'-1"	16'-5"	15'-5"	14'-3"	
	NI-70	19'-10"	17'-11"	16'-9"	15'-6"	19'-10"	17'-11"	16'-9"	15'-6"	
	N1-80	20'-2"	18'-3"	17'-1"	15'-10"	20'-2"	18'-3"	17'-1"	15'-10"	
	NI-20	18'-10"	17'-1"	16'-0"	14'-10"	18'-10"	17'-1"	16'-0"	14'-10"	
	NI-40x	21'-3"	19'-3"	17'-9"	15'-10"	21'-3"	19'-3"	17'-9"	15'-10"	
4.4.7.(0)!	N1-60	21'-9"	19'-8"	18'-5"	17'-1"	21'-9"	19'-8"	18'-5"	17'-1"	
11-7/8"	NI-70	23'-4"	21'-5"	20'-1"	18'-6"	23'-8"	21'-5"	20'-1"	18'-6"	
	NI-80	23'-7"	21'-10"	20'-5"	18'-11"	24'-1"	21'-10"	20'-5"	18'-11"	
	NI-90x	24'-3"	22'-6"	21'-3"	19'-7"	24'-8"	22'-7"	21'-3"	19'-7"	
	NI-40x	24'-2"	21'-5"	19'-6"	17'-5"	24'-2"	21'-5"	19'-6"	17'-5"	
	NI-60	24'-9"	22'-5"	21'-0"	19'-6"	24'-9"	22'-5"	21'-0"	19'-6"	
14"	NI-70	26'-1"	24'-3"	22'-9"	21'-0"	26'-8"	24'-3"	22'-9"	21'-0"	
	NI-80	26'-6"	24'-7"	23'-3"	21'-6"	27'-1"	24'-10"	23'-3"	21'-6"	
	NI-90x	27'-3"	25'-4"	24'-1"	22'-4"	27'-9"	25'-10"	24'-3"	22'-4"	
	NI-60	27'-3"	24'-11"	23'-5"	21'-7"	27'-6"	24'-11"	23'-5"	21'-7"	
4.68	NI-70	28'-8"	26'-8"	25'-3"	23'-4"	29'-3"	26'-11"	25'-3"	23'-4"	
16"	NI-80	29'-1"	27'-0"	25'-9"	23'-10"	29'-8"	27'-6"	25'-10"	23'-10"	
	NI-90x	29'-11"	27'-10"	26'-6"	24'-10"	30 ' -6"	28'-5"	26'-11"	24'-10"	

^{1.} Maximum clear span applicable to simple-span residential floor construction with a design live load of 40 psf and dead load of 30 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration for floor vibration, a live load deflection limit of L/480 and a total load deflection limit of L/240.

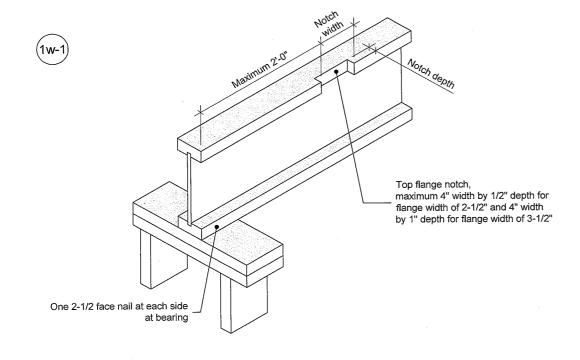
^{2.} Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum thickness of 3/4 inch for a joist spacing of 24 inches or less. The composite floor may include 1/2 inch gypsum ceiling and/or one row of blocking at mid-span with strapping. Strapping shall be minimum 1x4 inch strap applied to underside of joists at blocking line or 1/2 inch gypsum ceiling attached to joists.

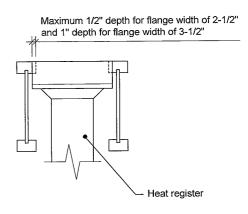
^{3.} Minimum bearing length shall be 1-3/4 inches for the end bearings.

^{4.} Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.

^{5.} This span chart is based on uniform loads. For applications with other than uniformly distributed loads, an engineering analysis may be required based on the use of the design properties. Tables are based on Limit States Design per CSA O86-09, NBC 2010, and OBC 2012.

^{6.} Joists shall be laterally supported at supports and continuously along the compression edge. Refer to technical documentation for installation guidelines and construction details. Nordic I-joists are listed in CCMC evaluation report 13032-R and APA Product Report PR-L274C.





- 1. Blocking required at bearing for lateral support, not shown for clarity.
- 2. The maximum dimensions for a notch on the side of the top flange are 4-inch width by 1/2-inch depth for flange width of 2-1/2 inches, and 4-inch width by 1-inch depth for flange width of 3-1/2 inches.
- 3. This detail applies to simple-span joists and multiple-span joists where the notch is located at the end half-span.
- 4. For other applications, contact Nordic Structures.

This document supersedes all previous versions. If the document has been in effect for more than one year, consult nordic.ca or contact Nordic Structures. All nails shown in the details are assumed to be common nails unless otherwise noted. Nails shall have a diameter not less than 0.128 inch for 2-1/2-inch nails, or 0.144 inch for 3-inch nails. Individual components not shown to scale for clarity.



T 514-871-8526 1 866 817-3418

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Notch in I-joist for Heat Register

CATEGORY

I-joist - Typical Floor Framing and Construction Details

DOCUMENT

NUMBER

2018-04-10

1w-1

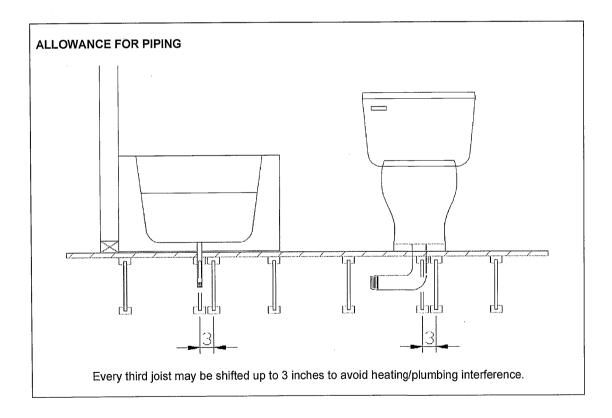


Allowance for Piping (Installation Notes)

The floor layouts have usually not been checked for heating and/or plumbing interference. On-site adjustment of joists of up to 3 inches is permitted to avoid interferences. When moving a joist, the subfloor thickness shall be checked with code requirements when the joist spacing exceeds 19.2 inches. Except for cutting to length, I-joist flanges should never be cut, drilled, or notched.

Installation of Nordic I-joists shall be as per *Nordic Joist Installation Guide for Residential Floors*. Refer to Tables 1 and 2 for maximum web hole and duct chase openings, respectively. These tables are based on the I-joists being used at their maximum spans. The minimum distance given may be reduced for shorter spans; contact your distributor for additional information.

The detail below shows the 3-inch allowance for piping. Every third joist may be shifted up to 3 inches to avoid heating/plumbing interference. For other applications, please contact your distributor.



Revised April 12, 2012