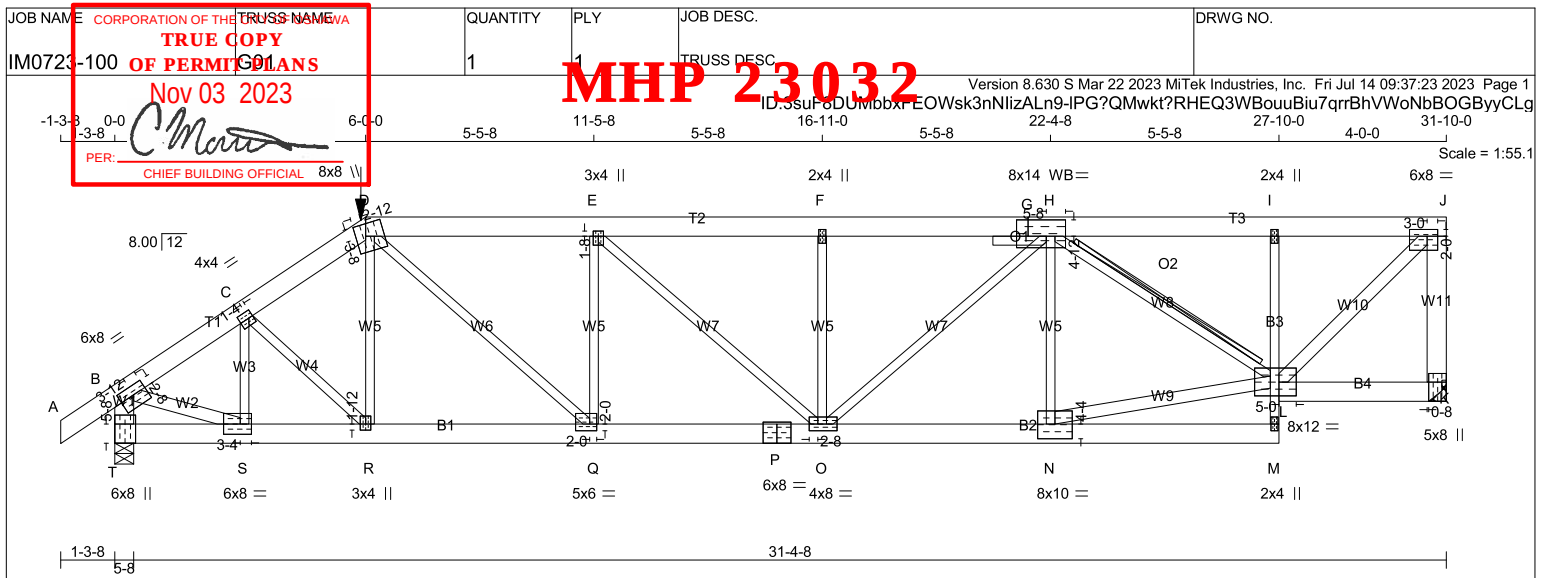




TOTAL WEIGHT = 188 lb

**LUMBER**

| N. L. G. A. RULES | CHORDS | SIZE | LUMBER | DESCR. |
|-------------------|--------|------|--------|--------|
| A - D             | 2x6    | DRY  | No.2   | SPF    |
| D - G             | 2x6    | DRY  | No.2   | SPF    |
| G - J             | 2x6    | DRY  | No.2   | SPF    |
| K - J             | 2x6    | DRY  | No.2   | SPF    |
| T - B             | 2x6    | DRY  | No.2   | SPF    |
| T - P             | 2x6    | DRY  | No.2   | SPF    |
| P - M             | 2x6    | DRY  | No.2   | SPF    |
| M - I             | 2x3    | DRY  | No.2   | SPF    |
| L - K             | 2x6    | DRY  | No.2   | SPF    |

| ALL WEBS EXCEPT | SIZE | LUMBER | DESCR.     |
|-----------------|------|--------|------------|
| N - L           | 2x4  | DRY    | 2100F 1.8E |
| L - J           | 2x4  | DRY    | No.2       |
| B - S           | 2x4  | DRY    | No.2       |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT TYPE    | PLATES | W   | LEN  | Y    | X    |
|------------|--------|-----|------|------|------|
| B TMVW-t   | MT20   | 6.0 | 8.0  | 2.50 | 3.75 |
| C TMVW-t   | MT20   | 4.0 | 4.0  | 2.00 | 1.25 |
| D TTWW+m   | MT20   | 8.0 | 8.0  | 3.50 | 2.75 |
| E TMVW-t   | MT20   | 3.0 | 4.0  | 1.50 | 1.50 |
| F TMVW-w   | MT20   | 2.0 | 4.0  |      |      |
| G          |        |     |      |      |      |
| G TSWWW-I  | MT20   | 8.0 | 14.0 | 4.75 | 5.50 |
| H          |        |     |      |      |      |
| I TMV+p    | MT20   | 2.0 | 4.0  |      |      |
| J TMVW-t   | MT20   | 6.0 | 8.0  | 2.00 | 3.00 |
| K BMV1+t   | MT20   | 5.0 | 8.0  | Edge | 0.50 |
| L BVMMWW-I | MT20   | 8.0 | 12.0 | 4.00 | 5.00 |
| M BMV+p    | MT20   | 2.0 | 4.0  |      |      |
| N BMVW-t   | MT20   | 8.0 | 10.0 | 4.25 | 5.00 |
| O BMVWW-t  | MT20   | 4.0 | 8.0  | 2.00 | 2.50 |
| P BS-I     | MT20   | 6.0 | 8.0  |      |      |
| Q BMVW-t   | MT20   | 5.0 | 6.0  | 2.00 | 2.00 |
| R BMVWW-t  | MT20   | 3.0 | 4.0  | 1.75 | 1.50 |
| S BMVW-t   | MT20   | 6.0 | 8.0  | 3.00 | 3.25 |
| T BMV1+t   | MT20   | 6.0 | 8.0  | 5.50 |      |

Edge - INDICATES REFERENCE CORNER OF PLATE TOUCHES EDGE OF CHORD.

WB - INDICATES BLOCKING REQUIRED

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQD BRG |
|----|-------------------------|---------------------------------|-----------|----------|
| JT | VERT                    | HORZ                            | DOWN      | UPLIFT   |
| K  | 4173                    | 0                               | 4173      | 0        |
| T  | 4163                    | 0                               | 4163      | 0        |

A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED AT JOINT K. MINIMUM BEARING LENGTH AT JOINT K = 5-0.

**UNFACTORED REACTIONS**

| JT | 1ST LCASE COMBINED | MAX./MIN. SNOW | MIN. LIVE | PERM. LIVE | WIND  | DEAD    | SOIL  |
|----|--------------------|----------------|-----------|------------|-------|---------|-------|
| K  | 2916               | 2113 / 0       | 0 / 0     | 0 / 0      | 0 / 0 | 802 / 0 | 0 / 0 |
| T  | 2909               | 2107 / 0       | 0 / 0     | 0 / 0      | 0 / 0 | 801 / 0 | 0 / 0 |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) T  
BEARING SIZE FACTOR = 1.15 AT JNT(S) T (BASED ON SUPPORT DEPTH = 1-8)**BRACING**TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 2.45 FT.  
MAX. UNBRACED BOTTOM CHORD LENGTH = 6.29 FT. OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE LATERALLY RESTRAINED.

2x4 DRY SPF No.2 T-BRACE AT H-L

FASTEN T AND I-BRACES TO NARROW EDGE OF WEB WITH ONE ROW PER PLY OF 3" COMMON WIRE NAILS @ 6" O.C. WITH 3" MINIMUM END DISTANCE. BRACE MUST COVER 90% OF WEB LENGTH.

END VERTICAL(S) MUST BE SHEATHED OR HAVE BRACES AS INDICATED IN THE MAX. UNBRACED LENGTH COLUMN OF THE TABLE BELOW

**LOADING**

TOTAL LOAD CASES: (4)

| CHORDS |                           |                           |               | WEBS     |                           |                      |               |
|--------|---------------------------|---------------------------|---------------|----------|---------------------------|----------------------|---------------|
| MEMB.  | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | MAX. LC1 (LC) | MEMB.    | MAX. FACTORED FORCE (LBS) | MAX. UNBRACED LENGTH | MAX. LC1 (LC) |
| FR-TO  |                           | FROM                      | TO            | FR-TO    |                           |                      |               |
| A-B    | 0 / 47                    | -119.4                    | -119.4        | 0.09 (1) | 10.00                     | S-C                  | -1122 / 0     |
| B-C    | -4688 / 0                 | -119.4                    | -119.4        | 0.21 (1) | 3.80                      | C-R                  | 0 / 608       |
| C-D    | -5235 / 0                 | -119.4                    | -119.4        | 0.23 (1) | 3.60                      | R-D                  | -195 / 90     |
| D-E    | -6426 / 0                 | -225.2                    | -225.2        | 0.79 (1) | 2.60                      | D-Q                  | 0 / 2820      |
| E-F    | -6828 / 0                 | -225.2                    | -225.2        | 0.83 (1) | 2.45                      | Q-E                  | -1716 / 0     |
| F-G    | -6828 / 0                 | -225.2                    | -225.2        | 0.79 (1) | 2.55                      | E-O                  | 0 / 542       |
| G-H    | -6828 / 0                 | -225.2                    | -225.2        | 0.79 (1) | 2.55                      | O-F                  | -1163 / 0     |
| H-I    | -3881 / 0                 | -225.2                    | -225.2        | 0.54 (1) | 3.72                      | O-H                  | 0 / 1436      |
| I-J    | -3890 / 0                 | -225.2                    | -225.2        | 0.40 (1) | 3.91                      | N-H                  | -854 / 0      |
| K-J    | -4103 / 0                 | 0.0                       | 0.0           | 0.69 (1) | 5.18                      | N-L                  | 0 / 5828      |
| T-B    | -4078 / 0                 | 0.0                       | 0.0           | 0.29 (1) | 5.20                      | H-L                  | -2339 / 0     |
|        |                           |                           |               |          |                           | L-J                  | 0 / 5393      |
|        |                           |                           |               |          |                           | B-S                  | 0 / 4063      |
| T-S    | 0 / 0                     | -34.4                     | -34.4         | 0.08 (1) | 10.00                     |                      |               |
| S-R    | 0 / 3904                  | -34.4                     | -34.4         | 0.59 (1) | 10.00                     |                      |               |
| R-Q    | 0 / 4332                  | -34.4                     | -34.4         | 0.64 (1) | 10.00                     |                      |               |
| Q-P    | 0 / 6426                  | -34.4                     | -34.4         | 0.94 (1) | 10.00                     |                      |               |
| P-O    | 0 / 6426                  | -34.4                     | -34.4         | 0.94 (1) | 10.00                     |                      |               |
| O-N    | 0 / 5764                  | -34.4                     | -34.4         | 0.83 (1) | 10.00                     |                      |               |
| N-M    | 0 / 35                    | -34.4                     | -34.4         | 0.12 (4) | 10.00                     |                      |               |
| M-L    | 0 / 84                    | 0.0                       | 0.0           | 0.12 (1) | 10.00                     |                      |               |
| L-I    | -1130 / 0                 | 0.0                       | 0.0           | 0.40 (1) | 6.29                      |                      |               |
| L-K    | 0 / 0                     | -34.4                     | -34.4         | 0.09 (4) | 10.00                     |                      |               |

**SPECIFIED CONCENTRATED LOADS (LBS)**

| JT | LOC.  | LC1  | MAX. | FACE | DIR.  | TYPE | HEEL | CONN. |
|----|-------|------|------|------|-------|------|------|-------|
| D  | 6-0-0 | -367 | -367 | ---  | FRONT | VERT | ---  | C1    |

**CONNECTION REQUIREMENTS**

1) C1: A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED.

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |    |      |      |     |
|------------|----|------|------|-----|
| TOP CH.    | LL | =    | 34.8 | PSF |
|            | DL | =    | 6.0  | PSF |
| BOT CH.    | LL | =    | 0.0  | PSF |
|            | DL | =    | 7.3  | PSF |
| TOTAL LOAD | =  | 48.1 | PSF  |     |

**SPACING = 24.0 IN. C/C**

LOADING IN FLAT SECTION BASED ON A SLOPE OF 2.00/12 MINIMUM

GIRDER TYPE: CPrimeHip  
LEFT SETBACK = 6-0-0  
RIGHT SETBACK = 0-0  
END SETBACK = 6-0-0  
END WALL WIDTH = 5-8  
CORNER FRAMING TYPE: CONVENTIONAL  
END JACK TYPE: CONVENTIONAL  
APPLIED TO FRONT SIDE  
- ADD'L LOADS BASED ON 55 % OF GSL.

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBC 2015

THIS DESIGN COMPLIES WITH:  
- PART 9 OF CBC 2018, NBC-2019AE  
- PART 9 OF OBC 2012 (2019 AMENDMENT)  
- CSA 086-14  
- TPIC 2014

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (1.06")  
CALCULATED VERT. DEFL.(LL)= L/999 (0.26")  
ALLOWABLE DEFL.(TL)= L/360 (1.06")  
CALCULATED VERT. DEFL.(TL)= L/871 (0.44")CSI: TC=0.83/0.97 (E-F:1), BC=0.94/0.97 (O-Q:1)  
WB=0.95/0.97 (J-L:1), SSI=0.48/1.00 (D-E:1)DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.00  
COMP=1.00 SHEAR=1.00 TENS=1.00

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT.

NAIL VALUES  
PLATE GRIP(DRY) SHEAR SECTION  
(PSI) (PLI) (PLI)  
MAX MIN MAX MIN MAX MIN  
MT20 650 371 1747 788 1987 1873

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.90 (S) (INPUT = 0.90)  
JSI METAL= 0.97 (P) (INPUT = 1.00)

JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.



JOB NAMECORPORATION OF THE TRUSS NAMEWA  
IM0723-100 OF PERMIT G2ANS  
Nov 03 2023  
  
CHIEF BUILDING OFFICIAL

QUANTITYPLYJOB DESC.  
12TRUSS DESC  
Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:24 2023 Page 1  
ID:k8BaHzj6TdQ8JC9gNSa3d6z92M6-DbgNdiwNeJZ8raeiVP7jvRP9FCkQyXxbFwxoeyyCLf

MHP 23032

Scale = 1:58.2

TOTAL WEIGHT = 2 X 105 = 209 lb [M]

LUMBER  
N. L. G. A. RULES  
CHORDS SIZE LUMBER DESCR.  
A - F 2x4 DRY 2100F 1.8E SPF  
F - I 2x4 DRY 2100F 1.8E SPF  
S - B 2x6 DRY No.2 SPF  
J - I 2x6 DRY No.2 SPF  
S - Q 2x6 DRY 2100F 1.8E SPF  
Q - D 2x3 DRY No.2 SPF  
P - M 2x8 DRY 1950F 1.7E SPF  
L - G 2x4 DRY No.2 SPF  
L - J 2x6 DRY 2100F 1.8E SPF  
  
ALL WEBS 2x3 DRY No.2 SPF  
EXCEPT  
R - P 2x4 DRY No.2 SPF  
C - P 2x4 DRY No.2 SPF  
N - F 2x4 DRY 2100F 1.8E SPF  
M - K 2x4 DRY No.2 SPF  
M - H 2x4 DRY No.2 SPF  
K - I 2x4 DRY No.2 SPF  
  
DRY: SEASONED LUMBER.

DESIGN CONSISTS OF 2 TRUSSES BUILT SEPARATELY THEN FASTENED TOGETHER AS FOLLOWS:  
  
CHORDS #ROWS SURFACE SPACING (IN) LOAD(PLF)  
TOP CHORDS : (0.122"x3") SPIRAL NAILS  
A-F 1 12 SIDE(49.7)  
F-I 1 12 TOP  
S-B 2 12 TOP  
J-I 2 12 TOP  
BOTTOM CHORDS : (0.122"x3") SPIRAL NAILS  
S-Q 2 12 SIDE(10.2)  
L-J 2 6 SIDE(505.5)  
Q-D 1 12 TOP  
P-M 2 5 SIDE(505.5)  
G-L 1 12 TOP  
WEBS : (0.122"x3") SPIRAL NAILS  
2x3 1 6  
2x4 1 6  
  
NAILS TO BE DRIVEN FROM ONE SIDE ONLY.  
  
GIRDER NAILING ASSUMES NAILED HANGERS ARE FASTENED WITH MIN. 3-0 INCH NAILS.  
  
TOP - COMPONENTS ARE LOADED FROM THE TOP AND MUST BE PLACED ON TOP EDGE OF ALL PLIES FOR THE LOAD TO BE TRANSFERRED TO EACH PLY.

JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.

DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER  
BEARINGS  
FACTORED MAXIMUM FACTORED INPUT REQD  
GROSS REACTION GROSS REACTION BRG BRG  
JT VERT HORZ DOWN HORZ UPLIFT IN-SX IN-SX  
S 8262 0 8262 0 0 5-8 5-7  
J 10308 0 10308 0 0 5-8 5-8  
  
ALLOW FOR 0.3" OF HORIZONTAL MOVEMENT DUE TO TOTAL LOAD  
  
UNFACTORED REACTIONS  
1ST LCASE MAX./MIN. COMPONENT REACTIONS  
JT COMBINED SNOW LIVE PERM.LIVE WIND DEAD SOIL  
S 5771 4190 / 0 0 / 0 0 / 0 1581 / 0 0 / 0  
J 7204 5212 / 0 0 / 0 0 / 0 1992 / 0 0 / 0  
  
BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) S, J  
BEARING SIZE FACTOR = 1.15 AT JNT(S) S, J ( BASED ON SUPPORT DEPTH = 1-8 )  
  
BRACING  
TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 2.69 FT.  
MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.  
  
ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.  
  
2x4 DRY SPF No.2 T-BRACE AT G-N  
  
FASTEN T AND I-BRACES TO NARROW EDGE OF WEB WITH ONE ROW PER PLY OF 3" COMMON WIRE NAILS @ 6" O.C. WITH 3" MINIMUM END DISTANCE. BRACE MUST COVER 90% OF WEB LENGTH.  
  
END VERTICAL(S) MUST BE SHEATHED OR HAVE BRACES AS INDICATED IN THE MAX. UNBRACED LENGTH COLUMN OF THE TABLE BELOW  
  
LOADING  
TOTAL LOAD CASES: (4)

| CHORDS |                  |                           |               | WEBS  |                  |               |  |
|--------|------------------|---------------------------|---------------|-------|------------------|---------------|--|
| MEMB.  | MAX. FORCE (LBS) | FACTORED VERT. LOAD (PLF) | MAX. CS1 (LC) | MEMB. | MAX. FORCE (LBS) | MAX. CS1 (LC) |  |
| FR-TO  |                  | FROM TO                   |               | FR-TO |                  |               |  |
| A-B    | 0 / 45           | -119.4 -119.4             | 0.06 (1)      | R-C   | -8971 / 0        | 0.78 (1)      |  |
| B-C    | -7916 / 0        | -238.9 -238.9             | 0.18 (1)      | P-R   | 0 / 8491         | 0.75 (1)      |  |
| C-D    | -16614 / 0       | -238.9 -238.9             | 0.41 (1)      | C-P   | 0 / 8218         | 0.73 (1)      |  |
| D-E    | -12916 / 0       | -238.9 -238.9             | 0.30 (1)      | O-C   | -4467 / 0        | 0.49 (1)      |  |
| E-F    | -10420 / 0       | -119.4 -119.4             | 0.16 (1)      | O-E   | 0 / 4340         | 0.54 (1)      |  |
| F-G    | -10416 / 0       | -119.4 -119.4             | 0.32 (1)      | E-N   | -4031 / 0        | 0.70 (1)      |  |
| G-H    | -17005 / 0       | -119.4 -119.4             | 0.41 (1)      | N-F   | 0 / 11162        | 0.46 (1)      |  |
| H-I    | -9825 / 0        | -119.4 -119.4             | 0.21 (1)      | K-G   | -6701 / 0        | 0.88 (1)      |  |
| S-B    | -8102 / 0        | 0.0 0.0                   | 0.29 (1)      | M-K   | 0 / 9988         | 0.88 (1)      |  |
| J-I    | -9234 / 0        | 0.0 0.0                   | 0.33 (1)      | M-H   | 0 / 6895         | 0.61 (1)      |  |
|        |                  |                           |               | K-H   | -7361 / 0        | 0.67 (1)      |  |
|        |                  |                           |               | B-R   | 0 / 7305         | 0.90 (1)      |  |
|        |                  |                           |               | K-I   | 0 / 8887         | 0.79 (1)      |  |
| S-R    | 0 / 0            | -36.5 -36.5               | 0.05 (1)      |       |                  |               |  |
| R-Q    | 0 / 97           | -36.5 -36.5               | 0.05 (1)      |       |                  |               |  |
| Q-P    | 0 / 177          | 0.0 0.0                   | 0.23 (1)      |       |                  |               |  |
| P-D    | 0 / 4778         | 0.0 0.0                   | 0.80 (1)      |       |                  |               |  |
| P-O    | 0 / 14180        | -36.5 -36.5               | 0.49 (1)      |       |                  |               |  |
| O-N    | 0 / 10777        | -1029.3 -1029.3           | 0.53 (1)      |       |                  |               |  |
| N-M    | 0 / 14365        | -1029.3 -1029.3           | 0.62 (1)      |       |                  |               |  |
| L-M    | 0 / 875          | 0.0 0.0                   | 0.34 (1)      |       |                  |               |  |
| M-G    | 0 / 6746         | 0.0 0.0                   | 0.86 (1)      |       |                  |               |  |
| L-K    | 0 / 235          | -1029.3 -1029.3           | 0.08 (1)      |       |                  |               |  |
| K-J    | 0 / 0            | -1029.3 -1029.3           | 0.11 (1)      |       |                  |               |  |

| SPECIFIED CONCENTRATED LOADS (LBS) |        |       |       |      |            |           |            |          |          |
|------------------------------------|--------|-------|-------|------|------------|-----------|------------|----------|----------|
| JT                                 | LOC.   | LC1   | MAX-  | MAX+ | FACE FRONT | DIR. VERT | TYPE TOTAL | HEEL --- | CONN. C1 |
| O                                  | 6-0-12 | -2916 | -2916 | ---  |            |           |            |          |          |

CONNECTION REQUIREMENTS  
1) C1: A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED.

DESIGN CRITERIA  
\*\*\* SPECIAL LOADS ANALYSIS \*\*\*  
GEOMETRY AND/OR BASIC LOADS CHANGED BY USER.  
LOADS WERE DERIVED FROM USER INPUT NO FURTHER MODIFICATIONS WERE MADE  
  
SPECIFIED LOADS:  
TOP CH. LL = 34.8 PSF  
DL = 6.0 PSF  
BOT CH. LL = 0.0 PSF  
DL = 7.3 PSF  
TOTAL LOAD = 48.1 PSF  
  
SPACING = 24.0 IN./C/C  
  
GIRDER TYPE: CStdGirder  
START DISTANCE = 6-0-12  
START SPAN CARRIED = 31-10-0  
END DISTANCE = 17-0-0  
END SPAN CARRIED = 31-10-0  
END WALL WIDTH = 5-8  
APPLIED TO FRONT SIDE OF BOTTOM CHORD.  
- ADDTL LOADS BASED ON 55 % OF GSL.  
  
GIRDER TYPE: CPriHip  
SIDE SETBACK = 0-0  
END SETBACK = 6-0-0  
END WALL WIDTH = 0-0  
CORNER FRAMING TYPE: CONVENTIONAL  
END JACK TYPE: CONVENTIONAL  
APPLIED TO FRONT SIDE  
- ADDTL LOADS BASED ON 55 % OF GSL.  
LOADS APPLIED TO FIRST 6-0-12 OF SPAN MEASURED FROM THE LEFT.  
  
\*\*\* NON STANDARD GIRDER \*\*\*  
ADDTL USER-DEFINED LOADS APPLIED TO ALL LOAD CASES.  
  
THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015  
  
THIS DESIGN COMPLIES WITH:  
- PART 9 OF CBC 2018 , NBC-2019AE  
- PART 9 OF OBC 2012 (2019 AMENDMENT)  
- CSA 086-14  
- TPIC 2014  
  
(55 % OF 48.1 P.S.F. G.S.L PLUS 8.4 P.S.F. RAIN LOAD)

|            |                                                 |          |     |             |          |
|------------|-------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                   | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMIT<br>NO. 02<br>Nov 03 2023 | 1        | 2   | TRUSS DESC. |          |

MHP 23032

Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:24 2023 Page 2

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**PLATES** (table 1)

| JT | TYPE    | PLATES | BUILDING | OFF  | ONLY | X    |
|----|---------|--------|----------|------|------|------|
| B  | TMVW+p  | MT20   | 6.0      | 8.0  | 1.75 | 3.50 |
| C  | TMWW-t  | MT20   | 6.0      | 8.0  | 2.25 | 3.50 |
| D  | TMVW+p  | MT20   | 4.0      | 6.0  | 1.75 | 1.75 |
| E  | TMWW-t  | MT20   | 5.0      | 5.0  | 2.00 | 1.25 |
| F  | TTW-h   | MT20   | 8.0      | 8.0  | 2.50 | 5.25 |
| G  | TMVW-t  | MT20   | 6.0      | 6.0  | 2.25 | 1.75 |
| H  | TMWW-t  | MT20   | 6.0      | 6.0  | 1.75 | 2.25 |
| I  | TMVW-t  | MT20   | 6.0      | 8.0  | 2.00 | 3.75 |
| J  | BMV1+t  | MT20   | 6.0      | 8.0  | Edge | 0.50 |
| K  | BMWWW-t | MT20   | 6.0      | 16.0 | 3.00 | 7.50 |
| L  | BMV+p   | MT20   | 2.0      | 4.0  |      |      |
| M  | BVMWW-w | MT20   | 10.0     | 14.0 | 4.00 | 9.50 |
| N  | BMWWW+t | MT20   | 10.0     | 10.0 | 5.50 | 5.00 |
| O  | BMWW+t  | MT20   | 5.0      | 6.0  | 2.75 | 2.25 |
| P  | BVMWW-w | MT20   | 8.0      | 14.0 | 2.50 | 9.00 |
| Q  | BMV+p   | MT20   | 2.0      | 4.0  |      |      |
| R  | BMWWW-t | MT20   | 6.0      | 12.0 | 2.50 | 6.00 |
| S  | BMV1+p  | MT20   | 3.0      | 5.0  | 2.75 | 1.50 |

Edge - INDICATES REFERENCE CORNER OF PLATE TOUCHES EDGE OF CHORD.

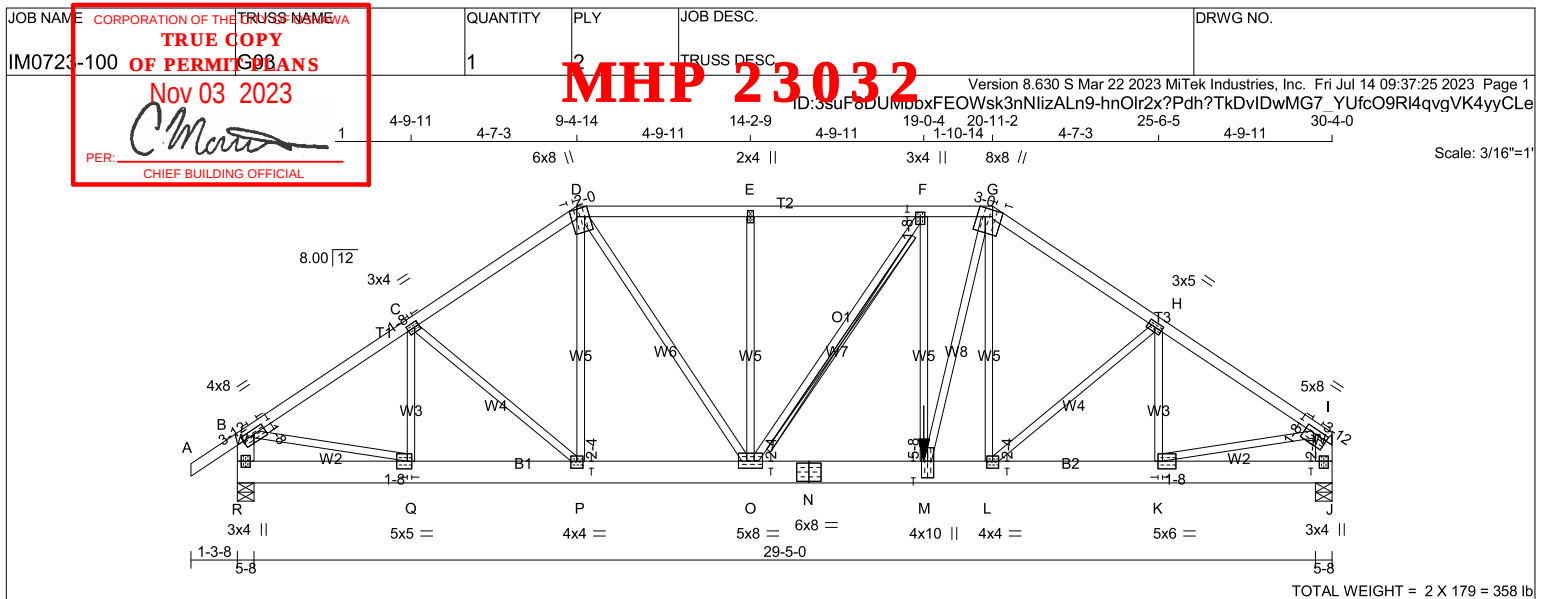
NAIL VALUES  
 PLATE GRIP(DRY) SHEAR SECTION  
 (PSI) (PLI) (PLI)  
 MAX MIN MAX MIN MAX MIN  
 MT20 650 371 1747 788 1987 1873  
 PLATE PLACEMENT TOL. = 0.250 inches  
 PLATE ROTATION TOL. = 5.0 Deg.  
 JSI GRIP= 0.90 (K) (INPUT = 0.90 )  
 JSI METAL= 0.88 (I) (INPUT = 1.00 )



JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE  
 ENGINEERING NOTES: TRUSSES. THE NOTE PAGE  
 IS AN INTEGRAL PART OF THIS DRAWING AS IT  
 CONTAINS SPECIFICATIONS AND CRITERIA USED  
 IN THE DESIGN OF THIS COMPONENT.





| LUMBER            |        |      |        |
|-------------------|--------|------|--------|
| N. L. G. A. RULES | CHORDS | SIZE | LUMBER |
| A - D             | 2x4    | DRY  | No.2   |
| D - G             | 2x4    | DRY  | No.2   |
| G - I             | 2x4    | DRY  | No.2   |
| R - B             | 2x6    | DRY  | No.2   |
| J - I             | 2x6    | DRY  | No.2   |
| R - N             | 2x8    | DRY  | No.2   |
| N - J             | 2x8    | DRY  | No.2   |
| ALL WEBS          | 2x3    | DRY  | No.2   |
| EXCEPT            |        |      | SPF    |

DRY: SEASONED LUMBER.

DESIGN CONSISTS OF 2 TRUSSES BUILT SEPARATELY THEN FASTENED TOGETHER AS FOLLOWS:

| CHORDS #ROWS                             | SURFACE SPACING (IN) | LOAD (PLF) |
|------------------------------------------|----------------------|------------|
| TOP CHORDS : (0.122"x3") SPIRAL NAILS    |                      |            |
| A-D 1                                    | 12                   | TOP        |
| D-G 1                                    | 12                   | TOP        |
| G-I 1                                    | 12                   | TOP        |
| R-B 2                                    | 12                   | TOP        |
| J-I 2                                    | 12                   | TOP        |
| BOTTOM CHORDS : (0.122"x3") SPIRAL NAILS |                      |            |
| R-N 2                                    | 12                   | TOP        |
| N-J 2                                    | 12                   | SIDE(0.0)  |
| WEBS : (0.122"x3") SPIRAL NAILS          |                      |            |
| 2x3 1                                    | 6                    |            |

NAILS TO BE DRIVEN FROM ONE SIDE ONLY.

GIRDER NAILING ASSUMES NAILED HANGERS ARE FASTENED WITH MIN. 3-0 INCH NAILS.

TOP - COMPONENTS ARE LOADED FROM THE TOP AND MUST BE PLACED ON TOP EDGE OF ALL PLIES FOR THE LOAD TO BE TRANSFERRED TO EACH PLY.

SIDE - PLF SHOWN IS THE EQUIVALENT UDL APPLIED TO ONE SIDE THAT THE CORRESPONDING NAILING PATTERN SHALL BE CAPABLE OF TRANSFERING. REMAINING PLF MUST BE APPLIED ON THE OPPOSITE SIDE OR ON THE TOP.

#### PLATES (table is in inches)

| JT | TYPE   | PLATES | W   | LEN | Y    | X    |
|----|--------|--------|-----|-----|------|------|
| B  | TMVW-t | MT20   | 4.0 | 8.0 | 1.50 | 3.75 |
| C  | TMWW-t | MT20   | 3.0 | 4.0 | 1.50 | 1.50 |
| D  | TTWW+m | MT20   | 6.0 | 8.0 | Edge | 2.00 |

#### DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER

##### BEARINGS

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQRD BRG |
|----|-------------------------|---------------------------------|-----------|-----------|
| JT | VERT                    | HORZ                            | DOWN      | HORZ      |
| R  | 4394                    | 0                               | 4394      | 0         |
| J  | 5689                    | 0                               | 5689      | 0         |

##### UNFACTORED REACTIONS

| JT | 1ST LCASE | MAX./MIN. | COMPONENT REACTIONS |
|----|-----------|-----------|---------------------|
|    | COMBINED  | SNOW      | LIVE                |
| R  | 3066      | 2246 / 0  | 0 / 0               |
| J  | 3972      | 2897 / 0  | 0 / 0               |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) R, J

##### BRACING

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 3.05 FT. MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

2x4 DRY SPF No.2 T-BRACE AT F-O

FASTEN T AND I-BRACES TO NARROW EDGE OF WEB WITH ONE ROW PER PLY OF 3" COMMON WIRE NAILS @ 6" O.C. WITH 3" MINIMUM END DISTANCE. BRACE MUST COVER 90% OF WEB LENGTH.

END VERTICAL(S) MUST BE SHEATHED OR HAVE BRACES AS INDICATED IN THE MAX. UNBRACED LENGTH COLUMN OF THE TABLE BELOW

##### LOADING

TOTAL LOAD CASES: (4)

| C H O R D S |                           |                           |                      | W E B S |                           |                      |  |
|-------------|---------------------------|---------------------------|----------------------|---------|---------------------------|----------------------|--|
| MEMB.       | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | MAX. UNBRACED LENGTH | MEMB.   | MAX. FACTORED FORCE (LBS) | MAX. UNBRACED LENGTH |  |
| FR-TO       |                           | FROM TO                   | CSI (LC)             | FR-TO   |                           | CSI (LC)             |  |
| A-B         | 0 / 45                    | -119.4 -119.4             | 0.09 (1)             | Q-C     | -952 / 0                  | 0.14 (1)             |  |
| B-C         | -5413 / 0                 | -119.4 -119.4             | 0.41 (1)             | C-P     | 0 / 215                   | 0.03 (1)             |  |
| C-D         | -5685 / 0                 | -119.4 -119.4             | 0.41 (1)             | P-D     | 0 / 81                    | 0.02 (4)             |  |
| D-E         | -6447 / 0                 | -119.4 -119.4             | 0.42 (1)             | D-O     | 0 / 3159                  | 0.39 (1)             |  |
| E-F         | -6447 / 0                 | -119.4 -119.4             | 0.42 (1)             | O-E     | -657 / 0                  | 0.32 (1)             |  |
| F-G         | -7572 / 0                 | -119.4 -119.4             | 0.24 (1)             | O-F     | -2030 / 0                 | 0.76 (1)             |  |
| G-H         | -8042 / 0                 | -119.4 -119.4             | 0.57 (1)             | M-F     | 0 / 1343                  | 0.17 (1)             |  |
| H-I         | -7396 / 0                 | -119.4 -119.4             | 0.53 (1)             | M-G     | 0 / 3554                  | 0.44 (1)             |  |
| R-B         | -4282 / 0                 | 0.0 0.0                   | 0.15 (1)             | L-G     | 0 / 681                   | 0.08 (1)             |  |
| J-I         | -5537 / 0                 | 0.0 0.0                   | 0.20 (1)             | L-H     | 0 / 629                   | 0.08 (1)             |  |
| R-Q         | 0 / 0                     | -18.2 -18.2               | 0.08 (1)             | K-H     | -1432 / 0                 | 0.21 (1)             |  |
| Q-P         | 0 / 4532                  | -18.2 -18.2               | 0.32 (1)             | B-Q     | 0 / 4615                  | 0.57 (1)             |  |
| P-O         | 0 / 4695                  | -18.2 -18.2               | 0.29 (1)             | K-I     | 0 / 6294                  | 0.78 (1)             |  |
| O-N         | 0 / 7572                  | -18.2 -18.2               | 0.64 (1)             |         |                           |                      |  |
| N-M         | 0 / 7572                  | -18.2 -18.2               | 0.64 (1)             |         |                           |                      |  |
| M-L         | 0 / 6663                  | -18.2 -18.2               | 0.59 (1)             |         |                           |                      |  |
| L-K         | 0 / 6181                  | -18.2 -18.2               | 0.46 (1)             |         |                           |                      |  |
| K-J         | 0 / 0                     | -18.2 -18.2               | 0.13 (1)             |         |                           |                      |  |

##### SPECIFIED CONCENTRATED LOADS (LBS)

| JT | LOC.   | LC1   | MAX-  | MAX+ | FACE  | DIR. | TYPE | HEEL | CONN. |
|----|--------|-------|-------|------|-------|------|------|------|-------|
| M  | 19-0-4 | -1071 | -1071 | ---  | FRONT | VERT | DEAD | ---  | C1    |
| M  | 19-0-4 | -2936 | -2936 | ---  | FRONT | VERT | SNOW | ---  | C1    |

##### CONNECTION REQUIREMENTS

1) C1: A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED.

#### DESIGN CRITERIA

\*\*\* SPECIAL LOADS ANALYSIS \*\*\*  
GEOMETRY AND/OR BASIC LOADS CHANGED BY USER.  
LOADS WERE DERIVED FROM USER INPUT  
NO FURTHER MODIFICATIONS WERE MADE

##### SPECIFIED LOADS:

|            |   |      |     |
|------------|---|------|-----|
| TOP CH. LL | = | 34.8 | PSF |
| DL         | = | 6.0  | PSF |
| BOT CH. LL | = | 0.0  | PSF |
| DL         | = | 7.3  | PSF |
| TOTAL LOAD | = | 48.1 | PSF |

##### SPACING = 24.0 IN. C/C

LOADING IN FLAT SECTION BASED ON A SLOPE OF 2.00/12 MINIMUM

##### \*\*\* NON STANDARD GIRDER \*\*\*

ADDTL USER-DEFINED LOADS APPLIED TO ALL LOAD CASES.

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

THIS DESIGN COMPLIES WITH:  
- PART 9 OF CBC 2018 , NBC-2019AE  
- PART 9 OF OBC 2012 (2019 AMENDMENT)  
- CSA 086-14  
- TPIC 2014

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (1.01")  
CALCULATED VERT. DEFL.(LL)= L/ 999 (0.14")  
ALLOWABLE DEFL.(TL)= L/360 (1.01")  
CALCULATED VERT. DEFL.(TL)= L/ 999 (0.24")

CSI: TC=0.57/0.97 (G-H:1) , BC=0.64/0.97 (M-O:1)  
WB=0.78/0.97 (I-K:1) , SSI=0.24/1.00 (L-M:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.00  
COMP=1.00 SHEAR=1.00 TENS= 1.00

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .

NAIL VALUES  
PLATE GRIP(DRY) SHEAR SECTION  
(PSI) (PLI) (PLI)  
MAX MIN MAX MIN MAX MIN  
MT20 650 371 1747 788 1987 1873

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.89 (K) (INPUT = 0.90 )  
JSI METAL= 0.70 (K) (INPUT = 1.00 )

CONTINUED ON PAGE 2



JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.

|            |                                        |          |     |             |          |
|------------|----------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME          | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMITS<br>Nov 03 2023 | 1        | 2   | TRUSS DESC. |          |

MHP 23032

Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:25 2023 Page 2  
ID:3suF6DUmbpxFEOWsk3nNliziALn9-hnOlr2x?Pdh?TkDvIDwMG7\_YUfcO9RI4qvgVK4yyCLe

PLATES (table 1)

| JT | TYPE    | PLATES | BUILDING | OFF  | ONLY | X    |
|----|---------|--------|----------|------|------|------|
| E  | TMW+w   | MT20   | 2.0      | 4.0  |      |      |
| F  | TMWW+t  | MT20   | 3.0      | 4.0  | 1.50 | 1.50 |
| G  | TTWW+m  | MT20   | 8.0      | 8.0  | Edge | 3.00 |
| H  | TMWW-t  | MT20   | 3.0      | 5.0  |      |      |
| I  | TMVW-t  | MT20   | 5.0      | 8.0  | 1.50 | 3.75 |
| J  | BMV1+p  | MT20   | 3.0      | 4.0  | 2.25 | 1.50 |
| K  | BMVW-t  | MT20   | 5.0      | 6.0  | 2.50 | 1.50 |
| L  | BMVW-t  | MT20   | 4.0      | 4.0  | 2.25 | 2.00 |
| M  | BMVW+t  | MT20   | 4.0      | 10.0 | 5.50 | 2.00 |
| N  | BS-t    | MT20   | 6.0      | 8.0  |      |      |
| O  | BMVWW-t | MT20   | 5.0      | 8.0  | 2.25 | 4.00 |
| P  | BMVW-t  | MT20   | 4.0      | 4.0  | 2.25 | 2.00 |
| Q  | BMVW-t  | MT20   | 5.0      | 5.0  | 2.50 | 1.50 |
| R  | BMV1+p  | MT20   | 3.0      | 4.0  |      |      |

Edge - INDICATES REFERENCE CORNER OF PLATE  
TOUCHES EDGE OF CHORD.



JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE  
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IN THE DESIGN OF THIS COMPONENT.



JOB NAME

CORPORATION OF THE TRUSS NAME

IM0723-100

OF PERMITS

Nov 03 2023

CHIEF BUILDING OFFICIAL

QUANTITY

PLY

TRUSS DESC.

MHP 23032

Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:26 2023 Page 1

DRWG NO.

Scale = 1:42.5

0-0

3-0-0

3-0-0

3-0-0

6-0-0

2x4 || C

8.00 | 12'

4x4 //

4x4 //

W5

W3

W4

W2

2x4 //

5x6 //

6x8 //

5-8'

5-6-8'

A

B

C

D

E

F

LUMBER

N. L. G. A. RULES

CHORDS SIZE LUMBER DESCR.

F - A 2x4 DRY No.2 SPF

A - C 2x4 DRY No.2 SPF

D - C 2x4 DRY No.2 SPF

F - D 2x6 DRY No.2 SPF

ALL WEBS 2x3 DRY No.2 SPF

DRY: SEASONED LUMBER.

PLATES (table is in inches)

JT TYPE PLATES W LEN Y X

A TMVW-p MT20 4.0 4.0 1.25 2.00

B TMVW-t MT20 4.0 4.0 1.75 1.00

C TMV+p MT20 2.0 4.0

D BMVW1+t MT20 6.0 8.0 Edge 2.50

E BMWW+t MT20 5.0 6.0 3.50 2.25

F BMV1+p MT20 2.0 4.0

Edge - INDICATES REFERENCE CORNER OF PLATE TOUCHES EDGE OF CHORD.

DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER

BEARINGS

FACTORED MAXIMUM FACTORED INPUT REQRD

GROSS REACTION GROSS REACTION BRG BRG

DOWN DOWN IN-SX IN-SX

VERT HORZ UPLIFT

JT 1519 0 1519 0 0 5-8 1-10

F 1519 0 1519 0 0 MECHANICAL

D 1519 0 1519 0 0

A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED AT JOINT D. MINIMUM BEARING LENGTH AT JOINT D = 3-8.

UNFACTORED REACTIONS

1ST LCASE MAX/MIN COMPONENT REACTIONS

COMBINED SNOW LIVE PERM.LIVE WIND DEAD SOIL

JT 1061 768 / 0 0 / 0 0 / 0 0 / 0 293 / 0 0 / 0

F 1061 768 / 0 0 / 0 0 / 0 0 / 0 293 / 0 0 / 0

D 1061 768 / 0 0 / 0 0 / 0 0 / 0 293 / 0 0 / 0

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) F

BRACING

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 5.81 FT.

MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

LOADING

TOTAL LOAD CASES: (4)

CHORDS MEMB. MAX. FACTORED FORCE (LBS) FACTORED VERT. LOAD (PLF) FROM TO MAX CSI (LC) WEBS MEMB. MAX. FACTORED FORCE (LBS) MAX CSI (LC)

F-A -1038 / 0 0.0 0.0 0.12 (1) 7.59 A-E 0 / 947 0.23 (1)

A-B -1059 / 0 -119.4 -119.4 0.20 (1) 5.81 E-B 0 / 1061 0.26 (1)

B-C -22 / 0 -119.4 -119.4 0.18 (1) 6.25 B-D -1271 / 0 0.37 (1)

D-C -140 / 0 0.0 0.0 0.07 (1) 7.81

F-E 0 / 0 -386.8 -386.8 0.22 (1) 10.00

E-D 0 / 899 -386.8 -386.8 0.34 (1) 10.00

DESIGN CRITERIA

SPECIFIED LOADS:

TOP CH. LL = 34.8 PSF

DL = 6.0 PSF

BOT CH. LL = 0.0 PSF

DL = 7.3 PSF

TOTAL LOAD = 48.1 PSF

SPACING = 24.0 IN./C

GIRDER TYPE: CStd Girder

START DISTANCE = 0-0

START SPAN CARRIED = 13-2-0

END DISTANCE = 6-0-0

END SPAN CARRIED = 13-2-0

END WALL WIDTH = 5-8

APPLIED TO FRONT SIDE OF BOTTOM CHORD.

- ADDTL LOADS BASED ON 55 % OF GSL.

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBC 2015

THIS DESIGN COMPLIES WITH:

- PART 9 OF CBC 2018 , NBC-2019AE

- PART 9 OF OBC 2012 (2019 AMENDMENT)

- CSA 086-14

- TPIC 2014

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.20")

CALCULATED VERT. DEFL.(LL) = L/ 999 (0.01")

ALLOWABLE DEFL.(TL)= L/360 (0.20")

CALCULATED VERT. DEFL.(TL) = L/ 999 (0.02")

CSI: TC=0.20/0.97 (A-B:1) , BC=0.34/0.97 (D-E:1) , WB=0.37/0.97 (B-D:1) , SSI=0.45/1.00 (E-F:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.00 COMP=1.00 SHEAR=1.00 TENS= 1.00

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .

NAIL VALUES

PLATE GRIP(DRY) SHEAR SECTION (PSI) (PLI) (PLI)

MAX MIN MAX MIN MAX MIN

MT20 650 371 1747 788 1987 1873

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.83 (A) (INPUT = 0.90 )

JSI METAL= 0.32 (E) (INPUT = 1.00 )

LICENSED PROFESSIONAL ENGINEER

I.MATUEVIC

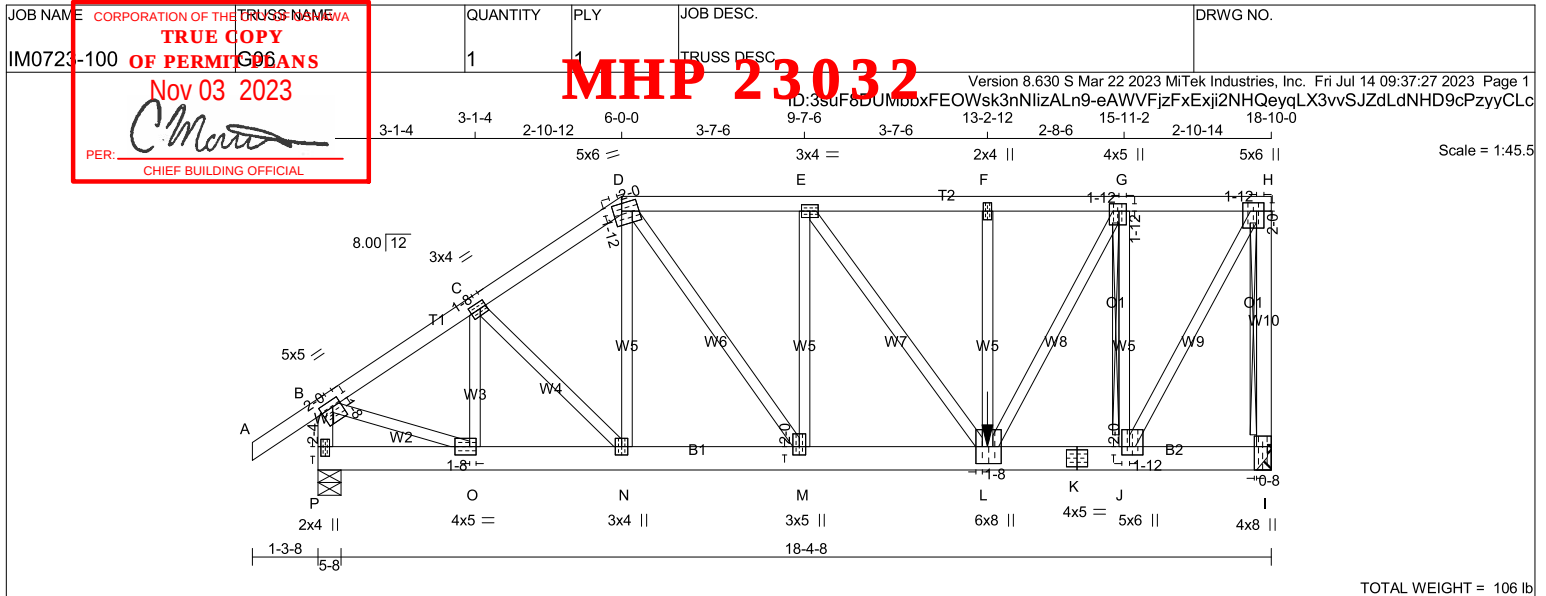
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PROVINCE OF ONTARIO

JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.

KOTT

**LUMBER**

| N. L. G. A. RULES | CHORDS | SIZE | LUMBER | DESCR. |
|-------------------|--------|------|--------|--------|
| A - D             | 2x4    | DRY  | No.2   | SPF    |
| D - H             | 2x4    | DRY  | No.2   | SPF    |
| I - H             | 2x4    | DRY  | No.2   | SPF    |
| P - B             | 2x4    | DRY  | No.2   | SPF    |
| P - K             | 2x6    | DRY  | No.2   | SPF    |
| K - I             | 2x6    | DRY  | No.2   | SPF    |
| ALL WEBS          | 2x3    | DRY  | No.2   | SPF    |
| EXCEPT            |        |      |        |        |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT | TYPE    | PLATES | W   | LEN | Y    | X    |
|----|---------|--------|-----|-----|------|------|
| B  | TMVW-t  | MT20   | 5.0 | 5.0 | 1.50 | 2.00 |
| C  | TMVW-t  | MT20   | 3.0 | 4.0 | 1.50 | 1.50 |
| D  | TTWW-m  | MT20   | 5.0 | 6.0 | 1.75 | 2.00 |
| E  | TMVW-t  | MT20   | 3.0 | 4.0 |      |      |
| F  | TMVW-w  | MT20   | 2.0 | 4.0 |      |      |
| G  | TMVW-t  | MT20   | 4.0 | 5.0 | 1.75 | 1.75 |
| H  | TMVW-p  | MT20   | 5.0 | 6.0 | 2.00 | 1.75 |
| I  | BMV1-t  | MT20   | 4.0 | 8.0 | Edge | 0.50 |
| J  | BMVW-t  | MT20   | 5.0 | 6.0 | 2.00 | 1.75 |
| K  | BS-t    | MT20   | 4.0 | 5.0 |      |      |
| L  | BMVWW-t | MT20   | 6.0 | 8.0 | 4.00 | 1.50 |
| M  | BMVW-t  | MT20   | 3.0 | 5.0 | 2.00 | 1.50 |
| N  | BMVW-t  | MT20   | 3.0 | 4.0 |      |      |
| O  | BMVW-t  | MT20   | 4.0 | 5.0 | 2.00 | 1.50 |
| P  | BMV1-p  | MT20   | 2.0 | 4.0 | 2.25 | 1.00 |

Edge - INDICATES REFERENCE CORNER OF PLATE TOUCHES EDGE OF CHORD.

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQD BRG |
|----|-------------------------|---------------------------------|-----------|----------|
| JT | VERT                    | HORZ                            | DOWN      | HORZ     |
| I  | 2944                    | 0                               | 2944      | 0        |
| P  | 2014                    | 0                               | 2014      | 0        |

A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED AT JOINT I. MINIMUM BEARING LENGTH AT JOINT I = 3-8.

**UNFACTORED REACTIONS**

| JT | 1ST LCASE COMBINED | MAX./MIN. SNOW | MIN. LIVE | PERM. LIVE | WIND  | DEAD    | SOIL  |
|----|--------------------|----------------|-----------|------------|-------|---------|-------|
| I  | 2058               | 1489 / 0       | 0 / 0     | 0 / 0      | 0 / 0 | 569 / 0 | 0 / 0 |
| P  | 1405               | 1031 / 0       | 0 / 0     | 0 / 0      | 0 / 0 | 374 / 0 | 0 / 0 |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) P

**BRACING**

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 3.97 FT. MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

2x4 DRY SPF No.2 T-BRACE AT H-I, G-J

FASTEN T AND I-BRACES TO NARROW EDGE OF WEB WITH ONE ROW PER PLY OF 3" COMMON WIRE NAILS @ 6" O.C. WITH 3" MINIMUM END DISTANCE. BRACE MUST COVER 90% OF WEB LENGTH.

END VERTICAL(S) MUST BE SHEATHED OR HAVE BRACES AS INDICATED IN THE MAX. UNBRACED LENGTH COLUMN OF THE TABLE BELOW

**LOADING**

TOTAL LOAD CASES: (4)

| CHORDS |                                 |                                 |                           | WEBS  |                                 |                           |          |
|--------|---------------------------------|---------------------------------|---------------------------|-------|---------------------------------|---------------------------|----------|
| MEMB.  | MAX. FACTORED<br>FORCE<br>(LBS) | FACTORED<br>VERT. LOAD<br>(PLF) | MAX. UNBRACED<br>CSI (LC) | MEMB. | MAX. FACTORED<br>FORCE<br>(LBS) | MAX. UNBRACED<br>CSI (LC) |          |
| FR-TO  |                                 | FROM TO                         | LENGTH                    | FR-TO |                                 |                           |          |
| A-B    | 0 / 45                          | -119.4 -119.4                   | 0.18 (1)                  | 10.00 | O-C                             | -531 / 0                  | 0.11 (1) |
| B-C    | -1990 / 0                       | -119.4 -119.4                   | 0.24 (1)                  | 4.49  | C-N                             | 0 / 74                    | 0.02 (1) |
| C-D    | -2100 / 0                       | -119.4 -119.4                   | 0.24 (1)                  | 4.38  | N-D                             | 0 / 54                    | 0.02 (4) |
| D-E    | -2312 / 0                       | -119.4 -119.4                   | 0.33 (1)                  | 4.10  | D-M                             | 0 / 1002                  | 0.25 (1) |
| E-F    | -2443 / 0                       | -119.4 -119.4                   | 0.34 (1)                  | 3.99  | M-E                             | -672 / 0                  | 0.28 (1) |
| F-G    | -2443 / 0                       | -225.2 -225.2                   | 0.34 (1)                  | 3.97  | E-L                             | 0 / 225                   | 0.06 (1) |
| G-H    | -1525 / 0                       | -225.2 -225.2                   | 0.29 (1)                  | 4.91  | L-F                             | -462 / 0                  | 0.19 (1) |
| I-H    | -2907 / 0                       | 0.0 0.0                         | 0.51 (1)                  | 7.81  | L-G                             | 0 / 1940                  | 0.48 (1) |
| P-B    | -1965 / 0                       | 0.0 0.0                         | 0.22 (1)                  | 5.88  | J-G                             | -2432 / 0                 | 0.56 (1) |
|        |                                 |                                 |                           |       | J-H                             | 0 / 3047                  | 0.75 (1) |
| P-O    | 0 / 0                           | -18.2 -18.2                     | 0.05 (1)                  | 10.00 | B-O                             | 0 / 1757                  | 0.43 (1) |
| O-N    | 0 / 1673                        | -18.2 -18.2                     | 0.26 (1)                  | 10.00 |                                 |                           |          |
| N-M    | 0 / 1726                        | -18.2 -18.2                     | 0.25 (1)                  | 10.00 |                                 |                           |          |
| M-L    | 0 / 2312                        | -18.2 -18.2                     | 0.46 (1)                  | 10.00 |                                 |                           |          |
| L-K    | 0 / 1525                        | -34.4 -34.4                     | 0.36 (1)                  | 10.00 |                                 |                           |          |
| K-J    | 0 / 1525                        | -34.4 -34.4                     | 0.36 (1)                  | 10.00 |                                 |                           |          |
| J-I    | 0 / 0                           | -34.4 -34.4                     | 0.04 (4)                  | 10.00 |                                 |                           |          |

**SPECIFIED CONCENTRATED LOADS (LBS)**

| JT | LOC.    | LC1   | MAX-  | MAX+ | FACE  | DIR. | TYPE  | HEEL | CONN. |
|----|---------|-------|-------|------|-------|------|-------|------|-------|
| L  | 13-2-12 | -1061 | -1061 | ---  | FRONT | VERT | TOTAL | ---  | C1    |

**CONNECTION REQUIREMENTS**

1) C1: A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED.

**DESIGN CRITERIA**

\*\*\* SPECIAL LOADS ANALYSIS \*\*\*  
GEOMETRY AND/OR BASIC LOADS CHANGED BY USER.  
LOADS WERE DERIVED FROM USER INPUT  
NO FURTHER MODIFICATIONS WERE MADE

**SPECIFIED LOADS:**

|            |    |      |      |     |
|------------|----|------|------|-----|
| TOP CH.    | LL | =    | 34.8 | PSF |
|            | DL | =    | 6.0  | PSF |
| BOT CH.    | LL | =    | 0.0  | PSF |
|            | DL | =    | 7.3  | PSF |
| TOTAL LOAD | =  | 48.1 | PSF  |     |

**SPACING = 24.0 IN. C/C**

LOADING IN FLAT SECTION BASED ON A SLOPE OF 2.00/12 MINIMUM

GIRDER TYPE: CPrimeHip  
LEFT SETBACK = 6-0-0  
RIGHT SETBACK = 0-0  
END SETBACK = 6-0-0  
END WALL WIDTH = 5-8  
CORNER FRAMING TYPE: CONVENTIONAL  
END JACK TYPE: CONVENTIONAL  
APPLIED TO FRONT SIDE  
- ADDTL LOADS BASED ON 55 % OF GSL.  
LOADS APPLIED TO FIRST 5-7-4 OF SPAN MEASURED FROM THE RIGHT.

**\*\*\* NON STANDARD GIRDER \*\*\***

ADDTL USER-DEFINED LOADS APPLIED TO ALL LOAD CASES.

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBC 2015

**THIS DESIGN COMPLIES WITH:**

- PART 9 OF BCBC 2018 , NBC-2019AE  
- PART 9 OF OBC 2012 (2019 AMENDMENT)  
- CSA 086-14  
- TPIC 2014

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.63")  
CALCULATED VERT. DEFL.(LL)= L/999 (0.08")  
ALLOWABLE DEFL.(TL)= L/360 (0.63")  
CALCULATED VERT. DEFL.(TL)= L/999 (0.14")

CSI: TC=0.51/0.97 (H-I:1) , BC=0.46/0.97 (L-M:1) , WB=0.75/0.97 (H-J:1) , SSI=0.33/1.00 (G-H:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.00  
COMP=1.00 SHEAR=1.00 TENS= 1.00

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .

CONTINUED ON PAGE 2



READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.



JULY 14, 2023

|            |                                                                                               |          |     |             |          |
|------------|-----------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                                 | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMITS<br>NOV 03 2023<br>PER: <i>C. Matijevic</i><br>CHIEF BUILDING OFFICIAL | 1        | 1   | TRUSS DESC. |          |

**MHP 23032**

Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:27 2023 Page 2  
ID:3suF6dUMb0xFEOWsk3nNlIZALn9-eAWVFjzFxExji2NHQeyqLX3vvSJZdLdNHD9cPzyyCLc

NAIL VALUES  
 PLATE GRIP(DRY) SHEAR SECTION  
 (PSI) (PLI) (PLI)  
 MAX MIN MAX MIN MAX MIN  
 MT20 650 371 1747 788 1987 1873  
 PLATE PLACEMENT TOL. = 0.250 inches  
 PLATE ROTATION TOL. = 5.0 Deg.  
 JSI GRIP= 0.89 (C) (INPUT = 0.90 )  
 JSI METAL= 0.62 (B) (INPUT = 1.00 )



JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE  
 ENGINEERING NOTES: TRUSSES. THE NOTE PAGE  
 IS AN INTEGRAL PART OF THIS DRAWING AS IT  
 CONTAINS SPECIFICATIONS AND CRITERIA USED  
 IN THE DESIGN OF THIS COMPONENT.



|                                                                                                                                                          |                       |                                                                                                                         |                                                                                                                                                                                                                                                                                           |
|----------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------|-------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| JOB NAME: CORPORATION OF THE TRUSS NAME<br><b>TRUE COPY</b><br><b>OF PERMITS</b><br><b>NOV 03 2023</b><br>PER: <i>C. M...</i><br>CHIEF BUILDING OFFICIAL | QUANTITY: 1<br>PLY: 1 | JOB DESC: TRUSS DESC<br><div style="font-size: 2em; color: red; text-align: center; font-weight: bold;">MHP 23032</div> | DRWG NO.<br><div style="text-align: right; font-size: 0.8em;">Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:28 2023 Page 1</div> <div style="text-align: right; font-size: 0.7em;">ID: R8BzHzp7dQ8jC9gNSa3d6z92M6-6M4IT3 tiY3aKByU_LU3ulc6Msg?MtGXWtu9xPyyCLb</div> |
|----------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------|-------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|

Scale = 1:57.7

TOTAL WEIGHT = 94 lb

| <b>LUMBER</b><br>N. L. G. A. RULES<br><table border="1" style="width:100%; border-collapse: collapse; font-size: 0.8em;"> <tr> <th>CHORDS</th> <th>SIZE</th> <th>LUMBER</th> <th>DESCR.</th> </tr> <tr> <td>A - E</td> <td>2x4</td> <td>DRY</td> <td>No.2</td> </tr> <tr> <td>E - H</td> <td>2x4</td> <td>DRY</td> <td>No.2</td> </tr> <tr> <td>Q - B</td> <td>2x4</td> <td>DRY</td> <td>No.2</td> </tr> <tr> <td>I - H</td> <td>2x4</td> <td>DRY</td> <td>No.2</td> </tr> <tr> <td>Q - O</td> <td>2x4</td> <td>DRY</td> <td>No.2</td> </tr> <tr> <td>O - D</td> <td>2x3</td> <td>DRY</td> <td>No.2</td> </tr> <tr> <td>N - L</td> <td>2x4</td> <td>DRY</td> <td>No.2</td> </tr> <tr> <td>K - F</td> <td>2x3</td> <td>DRY</td> <td>No.2</td> </tr> <tr> <td>K - I</td> <td>2x4</td> <td>DRY</td> <td>No.2</td> </tr> </table><br>ALL WEBS EXCEPT 2x3 DRY<br>ALL GABLE WEBS 2x3 DRY<br>DRY: SEASONED LUMBER.<br>GABLE STUDS SPACED AT 2-0-0 OC. | CHORDS                  | SIZE                            | LUMBER         | DESCR.               | A - E | 2x4     | DRY   | No.2 | E - H | 2x4 | DRY | No.2 | Q - B | 2x4 | DRY | No.2 | I - H | 2x4 | DRY | No.2 | Q - O | 2x4 | DRY | No.2 | O - D | 2x3 | DRY | No.2 | N - L | 2x4 | DRY | No.2 | K - F | 2x3 | DRY | No.2 | K - I | 2x4 | DRY | No.2 | <b>DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER</b><br><b>BEARINGS</b><br><table border="1" style="width:100%; border-collapse: collapse; font-size: 0.8em;"> <tr> <th></th> <th>FACTORED GROSS REACTION</th> <th>MAXIMUM FACTORED GROSS REACTION</th> <th>INPUT BRG</th> <th>REQD BRG</th> </tr> <tr> <td>JT</td> <td>VERT</td> <td>HORZ</td> <td>UP/LIFT</td> <td>IN-SX</td> </tr> <tr> <td>Q</td> <td>1435</td> <td>0</td> <td>1435</td> <td>0</td> </tr> <tr> <td>I</td> <td>1271</td> <td>0</td> <td>1271</td> <td>0</td> </tr> </table><br><b>UNFACTORED REACTIONS</b><br><table border="1" style="width:100%; border-collapse: collapse; font-size: 0.8em;"> <tr> <th>JT</th> <th>1ST CASE COMBINED</th> <th>MAX./MIN. SNOW</th> <th>MAX./MIN. LIVE</th> <th>MAX./MIN. PERM. LIVE</th> <th>WIND</th> <th>DEAD</th> <th>SOIL</th> </tr> <tr> <td>Q</td> <td>1011</td> <td>687 / 0</td> <td>0 / 0</td> <td>0 / 0</td> <td>0 / 0</td> <td>323 / 0</td> <td>0 / 0</td> </tr> <tr> <td>I</td> <td>899</td> <td>592 / 0</td> <td>0 / 0</td> <td>0 / 0</td> <td>0 / 0</td> <td>307 / 0</td> <td>0 / 0</td> </tr> </table><br>BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) Q, I<br><b>BRACING</b><br>TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 4.52 FT.<br>MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.<br>ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED. |  | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQD BRG | JT | VERT | HORZ | UP/LIFT | IN-SX | Q | 1435 | 0 | 1435 | 0 | I | 1271 | 0 | 1271 | 0 | JT | 1ST CASE COMBINED | MAX./MIN. SNOW | MAX./MIN. LIVE | MAX./MIN. PERM. LIVE | WIND | DEAD | SOIL | Q | 1011 | 687 / 0 | 0 / 0 | 0 / 0 | 0 / 0 | 323 / 0 | 0 / 0 | I | 899 | 592 / 0 | 0 / 0 | 0 / 0 | 0 / 0 | 307 / 0 | 0 / 0 | <b>DESIGN CRITERIA</b><br>*** SPECIAL LOADS ANALYSIS ***<br>GEOMETRY AND/OR BASIC LOADS CHANGED BY USER.<br>LOADS WERE DERIVED FROM USER INPUT<br>NO FURTHER MODIFICATIONS WERE MADE<br><br>SPECIFIED LOADS:<br>TOP CH. LL = 34.8 PSF<br>DL = 6.0 PSF<br>BOT CH. LL = 0.0 PSF<br>DL = 7.3 PSF<br>TOTAL LOAD = 48.1 PSF<br><br><b>SPACING = 24.0 IN. C/C</b><br>*** NON STANDARD GIRDER ***<br>ADDTL USER-DEFINED LOADS APPLIED TO ALL LOAD CASES.<br><br>THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015<br><br>THIS DESIGN COMPLIES WITH:<br>- PART 9 OF CBC 2018 , NBC-2019AE<br>- PART 9 OF OBC 2012 (2019 AMENDMENT)<br>- CSA 086-14<br>- TPIC 2014<br><br>(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD<br><br>ALLOWABLE DEFL.(LL)= L/360 (0.57")<br>CALCULATED VERT. DEFL.(LL) = L/ 999 (0.04")<br>ALLOWABLE DEFL.(TL)= L/360 (0.57")<br>CALCULATED VERT. DEFL.(TL) = L/ 999 (0.10")<br><br>CSI: TC=0.33/0.97 (D-E-1) , BC=0.39/0.97 (M-N-1) , WB=0.41/0.97 (D-M-1) , SSI=0.22/1.00 (D-E-1)<br><br>DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10<br>COMP=1.10 SHEAR=1.10 TENS= 1.10<br><br>COMPANION LIVE LOAD FACTOR = 1.00<br><br>TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .<br><br><b>NAIL VALUES</b><br><table border="1" style="width:100%; border-collapse: collapse; font-size: 0.8em;"> <tr> <th>PLATE</th> <th>GRIP(DRY) (PSI)</th> <th>SHEAR (PLI)</th> <th>SECTION (PLI)</th> </tr> <tr> <td>MT20</td> <td>650</td> <td>371</td> <td>1747</td> </tr> <tr> <td></td> <td>788</td> <td>1987</td> <td>1873</td> </tr> </table><br>PLATE PLACEMENT TOL. = 0.250 inches<br>PLATE ROTATION TOL. = 5.0 Deg.<br>JSI GRIP= 0.90 (Z) (INPUT = 0.90 )<br>JSI METAL= 0.35 (H) (INPUT = 1.00 ) | PLATE | GRIP(DRY) (PSI) | SHEAR (PLI) | SECTION (PLI) | MT20 | 650 | 371 | 1747 |  | 788 | 1987 | 1873 |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|---------------------------------|----------------|----------------------|-------|---------|-------|------|-------|-----|-----|------|-------|-----|-----|------|-------|-----|-----|------|-------|-----|-----|------|-------|-----|-----|------|-------|-----|-----|------|-------|-----|-----|------|-------|-----|-----|------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|-------------------------|---------------------------------|-----------|----------|----|------|------|---------|-------|---|------|---|------|---|---|------|---|------|---|----|-------------------|----------------|----------------|----------------------|------|------|------|---|------|---------|-------|-------|-------|---------|-------|---|-----|---------|-------|-------|-------|---------|-------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------|-----------------|-------------|---------------|------|-----|-----|------|--|-----|------|------|
| CHORDS                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | SIZE                    | LUMBER                          | DESCR.         |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| A - E                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 2x4                     | DRY                             | No.2           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| E - H                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 2x4                     | DRY                             | No.2           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| Q - B                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 2x4                     | DRY                             | No.2           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| I - H                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 2x4                     | DRY                             | No.2           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| Q - O                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 2x4                     | DRY                             | No.2           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| O - D                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 2x3                     | DRY                             | No.2           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| N - L                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 2x4                     | DRY                             | No.2           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| K - F                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 2x3                     | DRY                             | No.2           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| K - I                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 2x4                     | DRY                             | No.2           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG      | REQD BRG             |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| JT                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | VERT                    | HORZ                            | UP/LIFT        | IN-SX                |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| Q                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 1435                    | 0                               | 1435           | 0                    |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| I                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 1271                    | 0                               | 1271           | 0                    |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| JT                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | 1ST CASE COMBINED       | MAX./MIN. SNOW                  | MAX./MIN. LIVE | MAX./MIN. PERM. LIVE | WIND  | DEAD    | SOIL  |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| Q                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 1011                    | 687 / 0                         | 0 / 0          | 0 / 0                | 0 / 0 | 323 / 0 | 0 / 0 |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| I                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 899                     | 592 / 0                         | 0 / 0          | 0 / 0                | 0 / 0 | 307 / 0 | 0 / 0 |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| PLATE                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | GRIP(DRY) (PSI)         | SHEAR (PLI)                     | SECTION (PLI)  |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
| MT20                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 650                     | 371                             | 1747           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 788                     | 1987                            | 1873           |                      |       |         |       |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |       |     |     |      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |                         |                                 |           |          |    |      |      |         |       |   |      |   |      |   |   |      |   |      |   |    |                   |                |                |                      |      |      |      |   |      |         |       |       |       |         |       |   |     |         |       |       |       |         |       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |       |                 |             |               |      |     |     |      |  |     |      |      |

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.

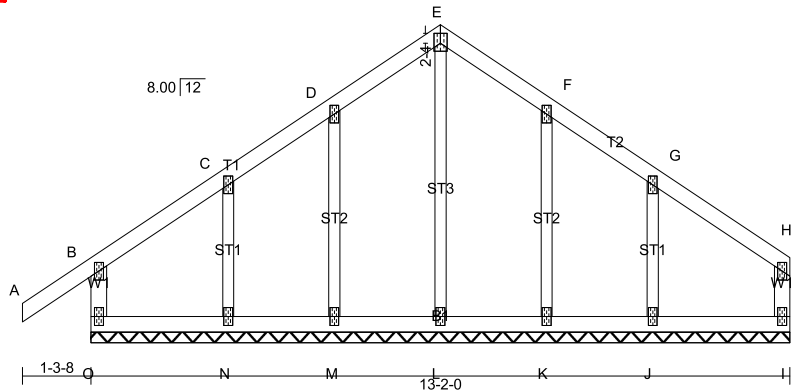
|            |                                                                                                     |          |     |             |          |
|------------|-----------------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                                       | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMIT<br>NO. 02<br>Nov 03 2023<br>PER: <i>C. M. ...</i><br>CHIEF BUILDING OFFICIAL | 1        | 1   | TRUSS DESC. |          |

MHP 23032

Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:29 2023 Page 1

ID: 3suPcdUmmbxFEOWsk3nNlIZALn9-aZeGgP VTrBryLXgX3?lQy8KpG6j5PHglXeIUryyCLa

Scale = 1:43.4



TOTAL WEIGHT = 52 lb

| LUMBER                          |         |        |        |
|---------------------------------|---------|--------|--------|
| N. L. G. A. RULES               |         |        |        |
| CHORDS                          | SIZE    | LUMBER | DESCR. |
| O - B                           | 2x4 DRY | No.2   | SPF    |
| A - E                           | 2x4 DRY | No.2   | SPF    |
| E - H                           | 2x4 DRY | No.2   | SPF    |
| I - H                           | 2x4 DRY | No.2   | SPF    |
| O - I                           | 2x4 DRY | No.2   | SPF    |
| ALL WEBS                        | 2x3 DRY | No.2   | SPF    |
| ALL GABLE WEBS                  | 2x3 DRY | No.2   | SPF    |
| DRY: SEASONED LUMBER.           |         |        |        |
| GABLE STUDS SPACED AT 2-0-0 OC. |         |        |        |

**PLATES (table is in inches)**

| JT TYPE       | PLATES | W   | LEN | Y    | X    |
|---------------|--------|-----|-----|------|------|
| B TMV+p       | MT20   | 2.0 | 4.0 |      |      |
| C, D, F, G    |        |     |     |      |      |
| C TMW+w       | MT20   | 2.0 | 4.0 |      |      |
| E TTW+p       | MT20   | 3.0 | 4.0 | 2.25 | 1.50 |
| H TMV+p       | MT20   | 2.0 | 4.0 |      |      |
| I BMV1+p      | MT20   | 2.0 | 4.0 |      |      |
| J, K, L, M, N |        |     |     |      |      |
| J BMW1+w      | MT20   | 2.0 | 4.0 |      |      |
| O BMV1+p      | MT20   | 2.0 | 4.0 |      |      |

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

THIS TRUSS DESIGNED FOR CONTINUOUS BEARINGS.

THIS TRUSS REQUIRES RIGID SHEATHING ON EXPOSED FACE.

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S)

**BRACING**

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 6.25 FT.

MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (4)

| CHORDS |                           |                           |                 | WEBS  |                           |                           |              |
|--------|---------------------------|---------------------------|-----------------|-------|---------------------------|---------------------------|--------------|
| MEMB.  | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | LC1 MAX (LC)    | MEMB. | MAX. FACTORED FORCE (LBS) | MAX. UNBRACED LENGTH (FT) | LC1 MAX (LC) |
| FR-TO  |                           | FROM TO                   |                 | FR-TO |                           |                           |              |
| O-B    | -354 / 0                  | 0.0                       | 0.05 (1)        | L-E   | -206 / 0                  | 7.81                      | 0.10 (1)     |
| A-B    | 0 / 45                    | -119.4                    | -119.4 0.16 (1) | M-D   | -232 / 0                  | 10.00                     | 0.07 (1)     |
| B-C    | -64 / 0                   | -119.4                    | -119.4 0.10 (1) | N-C   | -262 / 0                  | 6.25                      | 0.05 (1)     |
| C-D    | -53 / 0                   | -119.4                    | -119.4 0.07 (1) | K-F   | -227 / 0                  | 6.25                      | 0.07 (1)     |
| D-E    | -43 / 0                   | -119.4                    | -119.4 0.06 (1) | J-G   | -278 / 0                  | 6.25                      | 0.05 (1)     |
| E-F    | -42 / 0                   | -119.4                    | -119.4 0.06 (1) |       |                           |                           |              |
| F-G    | -55 / 0                   | -119.4                    | -119.4 0.08 (1) |       |                           |                           |              |
| G-H    | -57 / 0                   | -119.4                    | -119.4 0.08 (1) |       |                           |                           |              |
| I-H    | -178 / 0                  | 0.0                       | 0.0 0.06 (1)    |       |                           |                           |              |
| O-N    | 0 / 49                    | -18.2                     | -18.2 0.04 (1)  |       |                           |                           |              |
| N-M    | 0 / 42                    | -18.2                     | -18.2 0.02 (4)  |       |                           |                           |              |
| M-L    | 0 / 37                    | -18.2                     | -18.2 0.02 (4)  |       |                           |                           |              |
| L-K    | 0 / 37                    | -18.2                     | -18.2 0.02 (4)  |       |                           |                           |              |
| K-J    | 0 / 41                    | -18.2                     | -18.2 0.03 (4)  |       |                           |                           |              |
| J-I    | 0 / 50                    | -18.2                     | -18.2 0.03 (4)  |       |                           |                           |              |

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |    |      |      |     |
|------------|----|------|------|-----|
| TOP CH.    | LL | =    | 34.8 | PSF |
|            | DL | =    | 6.0  | PSF |
| BOT CH.    | LL | =    | 0.0  | PSF |
|            | DL | =    | 7.3  | PSF |
| TOTAL LOAD | =  | 48.1 | PSF  |     |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

THIS DESIGN COMPLIES WITH:

- PART 9 OF BCBC 2018, NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

**DESIGN ASSUMPTIONS**

-OVERHANG NOT TO BE ALTERED OR CUT OFF.

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

CSI: TC=0.16/0.97 (A-B:1), BC=0.04/0.97 (N-O:1), WB=0.10/0.97 (E-L:1), SSI=0.11/1.00 (A-B:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10 COMP=1.10 SHEAR=1.10 TENS=1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT.

**NAIL VALUES**

| PLATE | GRIP(DRY) | SHEAR | SECTION            |
|-------|-----------|-------|--------------------|
|       | (PSI)     | (PLI) | (PLI)              |
|       | MAX       | MIN   | MAX MIN            |
| MT20  | 650       | 371   | 1747 788 1987 1873 |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.26 (B) (INPUT = 0.90)

JSI METAL= 0.22 (H) (INPUT = 1.00)



JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.



|            |                                                                                                |          |     |             |          |
|------------|------------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                                  | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMIT PLANS<br>Nov 03 2023<br>PER: <i>C. Mante</i><br>CHIEF BUILDING OFFICIAL | 1        | 1   | TRUSS DESC. |          |

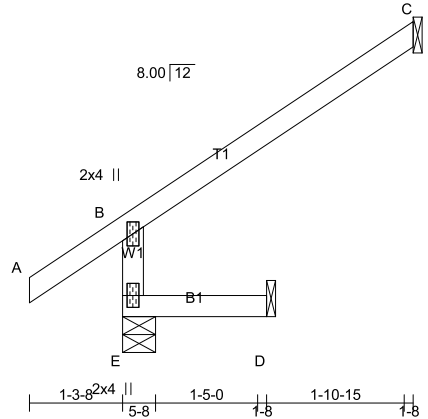
MHP 23032

Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:29 2023 Page 1

ID: 35uF6DUMbpxFEOWsk3nNliZALn9-aZeGgP\_VTrBRyLXgX3?IqY8H9G6?5QuglXeIUryyCLa

-1-3-8 1-3-8 0-0 2-0-0 2-0-0 2-0-7 4-0-7

Scale: 3/8"=1'



TOTAL WEIGHT = 11 lb

| LUMBER            | CHORDS | SIZE | LUMBER | DESCR. |
|-------------------|--------|------|--------|--------|
| N. L. G. A. RULES |        |      |        |        |
| E - B             | 2x4    | DRY  | No.2   | SPF    |
| A - C             | 2x4    | DRY  | No.2   | SPF    |
| E - D             | 2x4    | DRY  | No.2   | SPF    |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT | TYPE   | PLATES | W   | LEN | Y | X |
|----|--------|--------|-----|-----|---|---|
| B  | TMV+p  | MT20   | 2.0 | 4.0 |   |   |
| E  | BMV1+p | MT20   | 2.0 | 4.0 |   |   |

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQRD BRG |
|----|-------------------------|---------------------------------|-----------|-----------|
| JT | VERT                    | HORZ                            | DOWN      | HORZ      |
| E  | 485                     | 0                               | 485       | 0         |
| C  | 181                     | 0                               | 181       | 0         |
| D  | 17                      | 0                               | 18        | 0         |

SEE MITEK STANDARD DETAIL MSD2015-H FOR CONNECTION TO JOINT(S) C , D

**UNFACTORED REACTIONS**

| JT | 1ST LCASE | MAX./MIN. | COMPONENT REACTIONS |           |       |        |       |
|----|-----------|-----------|---------------------|-----------|-------|--------|-------|
|    | COMBINED  | SNOW      | LIVE                | PERM.LIVE | WIND  | DEAD   | SOIL  |
| E  | 334       | 271 / 0   | 0 / 0               | 0 / 0     | 0 / 0 | 63 / 0 | 0 / 0 |
| C  | 124       | 105 / 0   | 0 / 0               | 0 / 0     | 0 / 0 | 18 / 0 | 0 / 0 |
| D  | 13        | 0 / 0     | 0 / 0               | 0 / 0     | 0 / 0 | 13 / 0 | 0 / 0 |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) E

**BRACING**TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 6.25 FT.  
MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (4)

| C H O R D S |                           |                           |         | W E B S              |       |                           |                      |
|-------------|---------------------------|---------------------------|---------|----------------------|-------|---------------------------|----------------------|
| MEMB.       | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | LC1 MAX | MAX. UNBRACED LENGTH | MEMB. | MAX. FACTORED FORCE (LBS) | MAX. UNBRACED LENGTH |
| FR-TO       |                           | FROM TO                   |         |                      | FR-TO |                           |                      |
| E-B         | -465 / 0                  | 0.0                       | 0.0     | 0.01 (4)             | 7.81  |                           |                      |
| A-B         | 0 / 45                    | -119.4                    | -119.4  | 0.16 (1)             | 10.00 |                           |                      |
| B-C         | -33 / 0                   | -119.4                    | -119.4  | 0.33 (1)             | 6.25  |                           |                      |
| E-D         | 0 / 0                     | -18.2                     | -18.2   | 0.02 (4)             | 10.00 |                           |                      |

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |    |      |      |     |
|------------|----|------|------|-----|
| TOP CH.    | LL | =    | 34.8 | PSF |
|            | DL | =    | 6.0  | PSF |
| BOT CH.    | LL | =    | 0.0  | PSF |
|            | DL | =    | 7.3  | PSF |
| TOTAL LOAD | =  | 48.1 | PSF  |     |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

**THIS DESIGN COMPLIES WITH:**

- PART 9 OF BCBC 2018 , NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

**DESIGN ASSUMPTIONS**

-OVERHANG NOT TO BE ALTERED OR CUT OFF.

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.19")  
CALCULATED VERT. DEFL.(LL) = L/ 999 (0.00")  
ALLOWABLE DEFL.(TL)= L/360 (0.19")  
CALCULATED VERT. DEFL.(TL) = L/ 999 (0.00")CSI: TC=0.33/0.97 (B-C:1) , BC=0.02/0.97 (D-E:4) ,  
WB=0.00/0.97 (n/a:0) , SSI=0.20/1.00 (B-C:1)DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .

**NAIL VALUES**

| PLATE | GRIP(DRY) | SHEAR | SECTION |
|-------|-----------|-------|---------|
|       | (PSI)     | (PLI) | (PLI)   |
|       | MAX       | MIN   | MAX     |
| MT20  | 650       | 371   | 1747    |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.29 (B) (INPUT = 0.90 )  
JSI METAL= 0.24 (B) (INPUT = 1.00 )

JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.

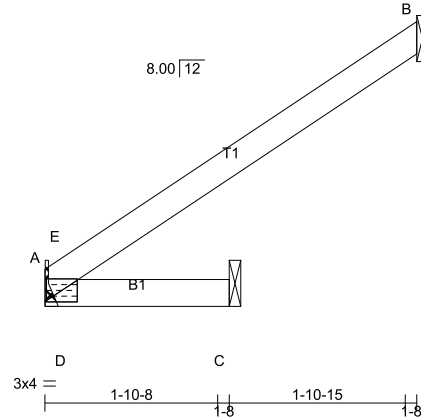


|            |                                                                                           |          |     |             |          |
|------------|-------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                             | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMITS<br>NOV 03 2023<br>PER: <i>C. Morte</i><br>CHIEF BUILDING OFFICIAL | 1        | 1   | TRUSS DESC. |          |

MHP 23032

Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:30 2023 Page 1  
ID:3sdF6DUMboxFEOWsk3nNlZALn9-2lBeul?7E9JlZV6s5mWXzAhUggPoqt8q\_BNG0HyyCLZ

Scale = 1:25.0



TOTAL WEIGHT = 8 lb

| LUMBER            | CHORDS | SIZE | LUMBER | DESCR. |
|-------------------|--------|------|--------|--------|
| N. L. G. A. RULES |        |      |        |        |
| A - B             | 2x4    | DRY  | No.2   | SPF    |
| A - C             | 2x4    | DRY  | No.2   | SPF    |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT | TYPE   | PLATES | W   | LEN | Y | X |
|----|--------|--------|-----|-----|---|---|
| A  | TMB1-I | MT20   | 3.0 | 4.0 |   |   |

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

| JT | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG  | REQRD BRG |
|----|-------------------------|---------------------------------|------------|-----------|
|    | VERT                    | DOWN                            | IN-SX      | IN-SX     |
| A  | 210                     | 0                               | MECHANICAL |           |
| B  | 192                     | 0                               | 1-8        | 1-8       |
| C  | 117                     | 0                               | 1-8        | 1-8       |

A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED AT JOINT A. MINIMUM BEARING LENGTH AT JOINT A = 1-12.

SEE MITEK STANDARD DETAIL MSD2015-H FOR CONNECTION TO JOINT(S) B , C

**UNFACTORED REACTIONS**

| JT | 1ST LCASE | MAX./MIN. | COMPONENT REACTIONS |           |       |        |       |
|----|-----------|-----------|---------------------|-----------|-------|--------|-------|
|    | COMBINED  | SNOW      | LIVE                | PERM.LIVE | WIND  | DEAD   | SOIL  |
| A  | 145       | 111 / 0   | 0 / 0               | 0 / 0     | 0 / 0 | 34 / 0 | 0 / 0 |
| B  | 131       | 112 / 0   | 0 / 0               | 0 / 0     | 0 / 0 | 20 / 0 | 0 / 0 |
| C  | 82        | 58 / 0    | 0 / 0               | 0 / 0     | 0 / 0 | 23 / 0 | 0 / 0 |

**BRACING**TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 6.25 FT.  
MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (4)

| MEMB. | CHORDS | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | MAX. FACTORED VERT. LOAD (PLF) | MAX. FACTORED VERT. LOAD (PLF) | MAX. FACTORED VERT. LOAD (PLF) | MAX. FACTORED VERT. LOAD (PLF) |
|-------|--------|---------------------------|---------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|
|       |        |                           |                           |                                |                                |                                |                                |
| FR-TO |        |                           |                           |                                |                                |                                |                                |
| A-E   |        | 0 / 313                   | -119.4                    | -119.4                         | 0.22 (1)                       | 10.00                          |                                |
| E-B   |        | -18 / 0                   | -119.4                    | -119.4                         | 0.20 (1)                       | 6.25                           |                                |
| A-D   |        | 0 / 0                     | -18.2                     | -18.2                          | 0.24 (1)                       | 10.00                          |                                |
| D-C   |        | 0 / 0                     | -18.2                     | -18.2                          | 0.24 (1)                       | 10.00                          |                                |

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |    |      |      |     |
|------------|----|------|------|-----|
| TOP CH.    | LL | =    | 34.8 | PSF |
|            | DL | =    | 6.0  | PSF |
| BOT CH.    | LL | =    | 0.0  | PSF |
|            | DL | =    | 7.3  | PSF |
| TOTAL LOAD | =  | 48.1 | PSF  |     |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

**THIS DESIGN COMPLIES WITH:**

- PART 9 OF BCBC 2018 , NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.19")  
CALCULATED VERT. DEFL.(LL) = L/999 (0.01")  
ALLOWABLE DEFL.(TL)= L/360 (0.19")  
CALCULATED VERT. DEFL.(TL) = L/999 (0.01")CSI: TC=0.22/0.97 (A-E:1) , BC=0.24/0.97 (A-D:1) ,  
WB=0.00/0.97 (D-E:1) , SSI=0.50/1.00 (A-D:1)DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .

**NAIL VALUES**

| PLATE | GRIP(DRY) | SHEAR | SECTION |
|-------|-----------|-------|---------|
|       | (PSI)     | (PLI) | (PLI)   |
|       | MAX       | MIN   | MAX     |
| MT20  | 650       | 371   | 1747    |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.18 (A) (INPUT = 0.90 )  
JSI METAL= 0.04 (A) (INPUT = 1.00 )

JULY 14, 2023

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|            |                                                                                                    |          |     |             |          |
|------------|----------------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                                      | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMIT PLANS<br>Nov 03 2023<br>PER: <i>C. Matijevic</i><br>CHIEF BUILDING OFFICIAL | 1        | 1   | TRUSS DESC. |          |

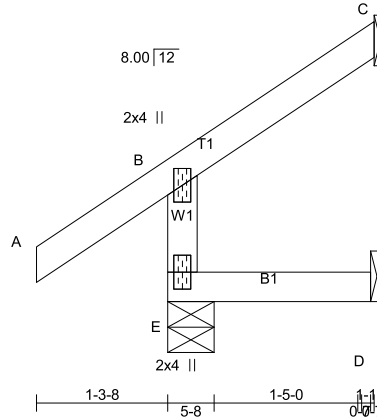
MHP 23032

Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:31 2023 Page 1

ID:3suF8LUMbXFEOWsk3nNlIZALn9-Wxl0550m?TS9Bfg3fU1mVNEgJ4oTZKozCr7pYkyyCLY

-1-3-8 1-3-8 0-0 2-0-0 2-0-0 2-0-7

Scale = 1:22.7



TOTAL WEIGHT = 8 lb

| LUMBER | N. L. G. A. RULES | CHORDS | SIZE | LUMBER | DESCR. |
|--------|-------------------|--------|------|--------|--------|
| E - B  | 2x4               | DRY    | No.2 | SPF    |        |
| A - C  | 2x4               | DRY    | No.2 | SPF    |        |
| E - D  | 2x4               | DRY    | No.2 | SPF    |        |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT | TYPE   | PLATES | W   | LEN | Y | X |
|----|--------|--------|-----|-----|---|---|
| B  | TMV+p  | MT20   | 2.0 | 4.0 |   |   |
| E  | BMV1+p | MT20   | 2.0 | 4.0 |   |   |

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQRD BRG |
|----|-------------------------|---------------------------------|-----------|-----------|
| JT | VERT                    | HORZ                            | DOWN      | HORZ      |
| E  | 335                     | 0                               | 335       | 0         |
| C  | 92                      | 0                               | 92        | 0         |
| D  | 17                      | 0                               | 18        | 0         |

SEE MITEK STANDARD DETAIL MSD2015-H FOR CONNECTION TO JOINT(S) C, D

**UNFACTORED REACTIONS**

| JT | 1ST LCASE COMBINED | SNOW    | LIVE  | PERM.LIVE | WIND  | DEAD   | SOIL  |
|----|--------------------|---------|-------|-----------|-------|--------|-------|
| E  | 231                | 184 / 0 | 0 / 0 | 0 / 0     | 0 / 0 | 48 / 0 | 0 / 0 |
| C  | 63                 | 54 / 0  | 0 / 0 | 0 / 0     | 0 / 0 | 9 / 0  | 0 / 0 |
| D  | 13                 | 0 / 0   | 0 / 0 | 0 / 0     | 0 / 0 | 13 / 0 | 0 / 0 |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) E

**BRACING**

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 6.25 FT.  
 MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (5)

| MEMB. | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | LC1 MAX | MAX. UNBRACED LENGTH | MEMB. | MAX. FACTORED FORCE (LBS) | MAX. UNBRACED LENGTH |
|-------|---------------------------|---------------------------|---------|----------------------|-------|---------------------------|----------------------|
| FR-TO |                           | FROM TO                   |         |                      | FR-TO |                           |                      |
| E-B   | -315 / 0                  | 0.0                       | 0.0     | 0.01 (4)             | 7.81  |                           |                      |
| A-B   | 0 / 45                    | -119.4                    | -119.4  | 0.16 (1)             | 10.00 |                           |                      |
| B-C   | -16 / 0                   | -119.4                    | -119.4  | 0.08 (1)             | 6.25  |                           |                      |
| E-D   | 0 / 0                     | -18.2                     | -18.2   | 0.02 (4)             | 10.00 |                           |                      |

CANTILEVER ANALYSIS HAS BEEN CONSIDERED IN THIS DESIGN

PATTERN-LOADING CHECK APPLIED TO THIS TRUSS.

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |      |      |     |
|------------|------|------|-----|
| TOP CH.    | LL = | 34.8 | PSF |
|            | DL = | 6.0  | PSF |
| BOT CH.    | LL = | 0.0  | PSF |
|            | DL = | 7.3  | PSF |
| TOTAL LOAD | =    | 48.1 | PSF |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

**THIS DESIGN COMPLIES WITH:**

- PART 9 OF BCBC 2018, NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

**DESIGN ASSUMPTIONS**

-OVERHANG NOT TO BE ALTERED OR CUT OFF.

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.19")  
 CALCULATED VERT. DEFL.(LL) = L/ 999 (0.00")  
 ALLOWABLE DEFL.(TL)= L/360 (0.19")  
 CALCULATED VERT. DEFL.(TL) = L/ 999 (0.00")

CSI: TC=0.16/0.97 (A-B:1), BC=0.02/0.97 (D-E:4),  
 WB=0.00/0.97 (n/a:0), SSI=0.11/1.00 (A-B:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
 COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT.

**NAIL VALUES**

| PLATE | GRIP(DRY) (PSI) | SHEAR (PLI) | SECTION (PLI) |
|-------|-----------------|-------------|---------------|
|       | MAX             | MIN         | MAX           |
| MT20  | 650             | 371         | 1747          |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.19 (B) (INPUT = 0.90 )  
 JSI METAL= 0.16 (B) (INPUT = 1.00 )



JULY 14, 2023

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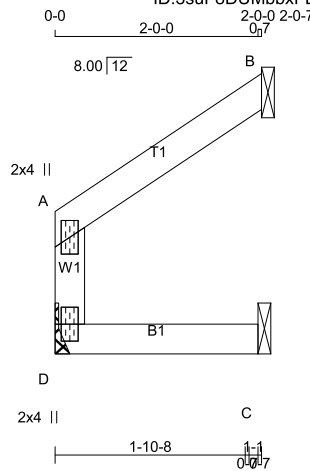


|            |                                                                                                     |          |     |             |          |
|------------|-----------------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                                       | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMIT<br>NO. 00A<br>Nov 03 2023<br>PER: <i>C. Morte</i><br>CHIEF BUILDING OFFICIAL | 1        | 1   | TRUSS DESC. |          |

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ID: 3sur8DumbbxEOWsk3nNlizALn9-7JOJR1Omma0ppFFDBY?2bmtbT7Zlne6RVsN4AyyCLX



TOTAL WEIGHT = 6 lb

| LUMBER            | SIZE | LUMBER | DESCR. |
|-------------------|------|--------|--------|
| N. L. G. A. RULES |      |        |        |
| CHORDS            | 2x4  | No.2   | SPF    |
| D - A             | 2x4  | DRY    | No.2   |
| A - B             | 2x4  | DRY    | No.2   |
| D - C             | 2x4  | DRY    | No.2   |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT | TYPE   | PLATES | W   | LEN | Y | X |
|----|--------|--------|-----|-----|---|---|
| A  | TMV+p  | MT20   | 2.0 | 4.0 |   |   |
| D  | BMV1+p | MT20   | 2.0 | 4.0 |   |   |

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

| JT | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQRD BRG |
|----|-------------------------|---------------------------------|-----------|-----------|
|    | VERT                    | HORZ                            | DOWN      | HORZ      |
| D  | 140                     | 0                               | 140       | 0         |
| B  | 113                     | 0                               | 113       | 0         |
| C  | 27                      | 0                               | 27        | 0         |

A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED AT JOINT D. MINIMUM BEARING LENGTH AT JOINT D = 1-8.

SEE MITEK STANDARD DETAIL MSD2015-H FOR CONNECTION TO JOINT(S) B , C

**UNFACTORED REACTIONS**

| JT | 1ST LCASE | MAX./MIN. | COMPONENT REACTIONS | WIND      | DEAD   | SOIL  |
|----|-----------|-----------|---------------------|-----------|--------|-------|
|    | COMBINED  | SNOW      | LIVE                | PERM.LIVE |        |       |
| D  | 98        | 71 / 0    | 0 / 0               | 0 / 0     | 27 / 0 | 0 / 0 |
| B  | 77        | 65 / 0    | 0 / 0               | 0 / 0     | 12 / 0 | 0 / 0 |
| C  | 20        | 6 / 0     | 0 / 0               | 0 / 0     | 15 / 0 | 0 / 0 |

**BRACING**

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 10.00 FT.  
MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (4)

| MEMB. | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | MAX. FACTORED VERT. LOAD (PLF) | MAX. FACTORED VERT. LOAD (PLF) | MAX. FACTORED VERT. LOAD (PLF) | MAX. FACTORED VERT. LOAD (PLF) |
|-------|---------------------------|---------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|
| FR-TO |                           | FROM                      | TO                             | LENGTH                         | FR-TO                          |                                |
| D-A   | -130 / 0                  | 0.0                       | 0.0                            | 0.02 (1)                       | 7.81                           |                                |
| A-B   | -5 / 0                    | -119.4                    | -119.4                         | 0.06 (1)                       | 10.00                          |                                |
| D-C   | 0 / 0                     | -18.2                     | -18.2                          | 0.03 (1)                       | 10.00                          |                                |

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |    |      |      |     |
|------------|----|------|------|-----|
| TOP CH.    | LL | =    | 34.8 | PSF |
|            | DL | =    | 6.0  | PSF |
| BOT CH.    | LL | =    | 0.0  | PSF |
|            | DL | =    | 7.3  | PSF |
| TOTAL LOAD | =  | 48.1 | PSF  |     |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

**THIS DESIGN COMPLIES WITH:**

- PART 9 OF BCBC 2018 , NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.19")  
CALCULATED VERT. DEFL.(LL)= L/ 999 (0.00")  
ALLOWABLE DEFL.(TL)= L/360 (0.19")  
CALCULATED VERT. DEFL.(TL)= L/ 999 (0.00")

CSI: TC=0.06/0.97 (A-B:1) , BC=0.03/0.97 (C-D:1) ,  
WB=0.00/0.97 (n/a:0) , SSI=0.08/1.00 (A-B:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .

**NAIL VALUES**

| PLATE | GRIP(DRY) | SHEAR | SECTION |
|-------|-----------|-------|---------|
|       | (PSI)     | (PLI) | (PLI)   |
| MT20  | 650       | 371   | 1747    |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

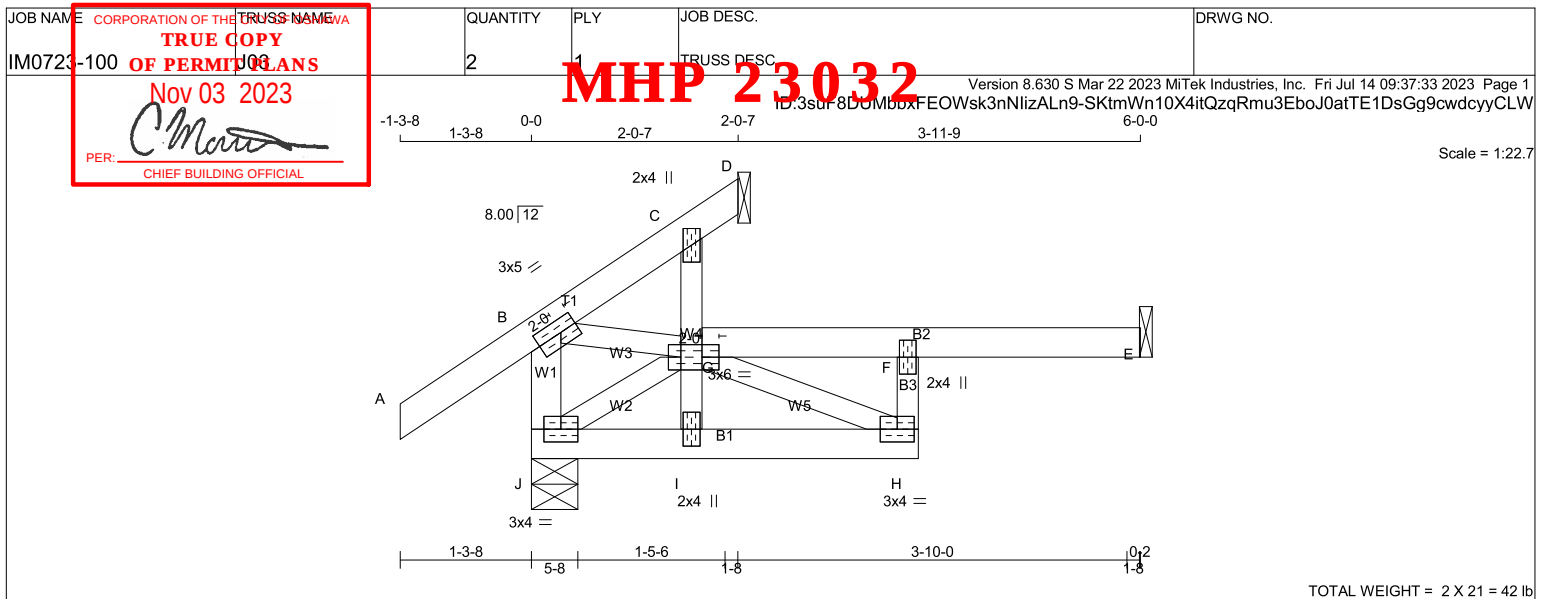
JSI GRIP= 0.08 (A) (INPUT = 0.90 )  
JSI METAL= 0.07 (A) (INPUT = 1.00 )



JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.





TOTAL WEIGHT = 2 X 21 = 42 lb

**LUMBER**

N. L. G. A. RULES

CHORDS SIZE

J - B 2x4 DRY No.2

A - D 2x4 DRY No.2

J - H 2x4 DRY No.2

H - F 2x3 DRY No.2

G - E 2x4 DRY No.2

ALL WEBS 2x3 DRY No.2

DRY: SEASONED LUMBER.

LUMBER

No.2

No.2

No.2

No.2

No.2

DESCR.

SPF

SPF

SPF

SPF

SPF

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQD BRG |
|----|-------------------------|---------------------------------|-----------|----------|
| JT | VERT                    | HORZ                            | DOWN      | HORZ     |
| J  | 339                     | 0                               | 339       | 0        |
| D  | 185                     | 0                               | 185       | 0        |
| E  | 32                      | 0                               | 35        | 0        |

SEE MITEK STANDARD DETAIL MSD2015-H FOR CONNECTION TO JOINT(S) D, E

**UNFACTORED REACTIONS**

| JT | 1ST LCASE COMBINED | MAX./MIN. SNOW | MAX./MIN. LIVE | PERM. LIVE | WIND  | DEAD    | SOIL  |
|----|--------------------|----------------|----------------|------------|-------|---------|-------|
| J  | 231                | 199 / 0        | 0 / 0          | 0 / 0      | 0 / 0 | 32 / 0  | 0 / 0 |
| D  | 140                | 38 / 0         | 0 / 0          | 0 / 0      | 0 / 0 | 102 / 0 | 0 / 0 |
| E  | 25                 | 0 / 0          | 0 / 0          | 0 / 0      | 0 / 0 | 25 / 0  | 0 / 0 |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) J, D

**BRACING**TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 6.25 FT.  
MAX. UNBRACED BOTTOM CHORD LENGTH = 6.25 FT. OR RIGID CEILING DIRECTLY APPLIED.

MAX. UNBRACED INTERIOR CHORD LENGTH = 10.00 FT

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (6)

| CHORDS |                           |                           |                      | WEBS  |                           |                      |  |
|--------|---------------------------|---------------------------|----------------------|-------|---------------------------|----------------------|--|
| MEMB.  | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | MAX. UNBRACED LENGTH | MEMB. | MAX. FACTORED FORCE (LBS) | MAX. UNBRACED LENGTH |  |
| FR-TO  |                           | FROM TO                   |                      | FR-TO |                           |                      |  |
| J-B    | -369 / 0                  | 0.0 0.0                   | 0.04 (1)             | I-G   | 0 / 53                    | 0.03 (4)             |  |
| A-B    | 0 / 45                    | -119.4 -119.4             | 0.16 (1)             | G-C   | 0 / 169                   | 0.07 (4)             |  |
| B-C    | -48 / 0                   | -119.4 -119.4             | 0.16 (4)             | B-G   | -22 / 0                   | 0.00 (4)             |  |
| C-D    | 0 / 85                    | -119.4 -119.4             | 0.18 (4)             | J-G   | 0 / 83                    | 0.03 (4)             |  |
|        |                           |                           |                      | G-H   | 0 / 83                    | 0.03 (4)             |  |
| J-I    | -71 / 0                   | -18.2 -18.2               | 0.03 (4)             |       |                           |                      |  |
| I-H    | -75 / 0                   | -18.2 -18.2               | 0.03 (4)             |       |                           |                      |  |
| H-F    | -21 / 0                   | 0.0 0.0                   | 0.00 (4)             |       |                           |                      |  |
| G-F    | 0 / 0                     | -18.2 -18.2               | 0.06 (4)             |       |                           |                      |  |
| F-E    | 0 / 0                     | -18.2 -18.2               | 0.06 (4)             |       |                           |                      |  |

PATTERN-LOADING CHECK APPLIED TO THIS TRUSS.**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |      |      |     |
|------------|------|------|-----|
| TOP CH.    | LL = | 34.8 | PSF |
|            | DL = | 6.0  | PSF |
| BOT CH.    | LL = | 0.0  | PSF |
|            | DL = | 7.3  | PSF |
| TOTAL LOAD | =    | 48.1 | PSF |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

THIS DESIGN COMPLIES WITH:

- PART 9 OF BCBC 2018, NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

**DESIGN ASSUMPTIONS**

-OVERHANG NOT TO BE ALTERED OR CUT OFF.

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.20")  
CALCULATED VERT. DEFL.(LL) = L/ 999 (0.00")  
ALLOWABLE DEFL.(TL)= L/360 (0.20")  
CALCULATED VERT. DEFL.(TL) = L/ 999 (0.01")CSI: TC=0.18/0.97 (C-D-4), BC=0.06/0.97 (E-F-4),  
WB=0.07/0.97 (C-G-4), SSI=0.14/1.00 (C-D-4)DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

AUTOSOLVE RIGHT HEEL ONLY

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .

**NAIL VALUES**

| PLATE | GRIP(DRY) (PSI) | SHEAR (PLI) | SECTION (PLI)      |
|-------|-----------------|-------------|--------------------|
| MT20  | 650             | 371         | 1747 788 1987 1873 |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.35 (J) (INPUT = 0.90 )  
JSI METAL= 0.10 (C) (INPUT = 1.00 )

JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.



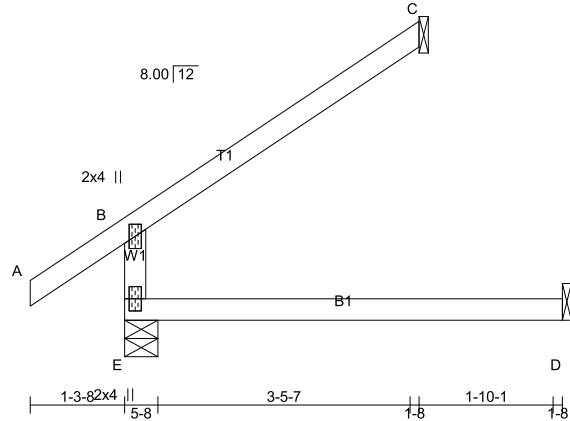
|            |                                                                                                |          |     |             |          |
|------------|------------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                                  | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMIT PLANS<br>Nov 03 2023<br>PER: <i>C. Mante</i><br>CHIEF BUILDING OFFICIAL | 2        | 1   | TRUSS DESC. |          |

**MHP 23032**

Version 8.630 S Mar 22 2023 MiTek Industries, Inc. Fri Jul 14 09:37:33 2023 Page 1

ID: 3sur-8DUMboxFEOWsk3nNizALn9-SKtmWn10X4itQzqRmu3EboJz9tR51EuGg9cwcyyCLW

Scale = 1:31.6



TOTAL WEIGHT = 2 X 15 = 31 lb

| LUMBER            |      |        |        |
|-------------------|------|--------|--------|
| N. L. G. A. RULES | SIZE | LUMBER | DESCR. |
| E - B             | 2x4  | DRY    | No.2   |
| A - C             | 2x4  | DRY    | No.2   |
| E - D             | 2x4  | DRY    | No.2   |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT | TYPE   | PLATES | W   | LEN | Y | X |
|----|--------|--------|-----|-----|---|---|
| B  | TMV+p  | MT20   | 2.0 | 4.0 |   |   |
| E  | BMV1+p | MT20   | 2.0 | 4.0 |   |   |

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQD BRG |
|----|-------------------------|---------------------------------|-----------|----------|
| JT | VERT                    | HORZ                            | DOWN      | HORZ     |
| E  | 529                     | 0                               | 529       | 0        |
| C  | 181                     | 0                               | 181       | 0        |
| D  | 46                      | 0                               | 46        | 0        |

SEE MITEK STANDARD DETAIL MSD2015-H FOR CONNECTION TO JOINT(S) C, D

**UNFACTORED REACTIONS**

| JT | 1ST LCASE | MAX./MIN. COMPONENT REACTIONS | SNOW  | LIVE  | PERM. LIVE | WIND  | DEAD   | SOIL  |
|----|-----------|-------------------------------|-------|-------|------------|-------|--------|-------|
| E  | 369       | 271 / 0                       | 0 / 0 | 0 / 0 | 0 / 0      | 0 / 0 | 98 / 0 | 0 / 0 |
| C  | 124       | 105 / 0                       | 0 / 0 | 0 / 0 | 0 / 0      | 0 / 0 | 18 / 0 | 0 / 0 |
| D  | 37        | 0 / 0                         | 0 / 0 | 0 / 0 | 0 / 0      | 0 / 0 | 37 / 0 | 0 / 0 |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) E, C

**BRACING**

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 6.25 FT.  
 MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE LATERALLY RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (4)

| C H O R D S |                           |                           |         | W E B S              |       |                           |                      |
|-------------|---------------------------|---------------------------|---------|----------------------|-------|---------------------------|----------------------|
| MEMB.       | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | LC1 MAX | MAX. UNBRACED LENGTH | MEMB. | MAX. FACTORED FORCE (LBS) | MAX. UNBRACED LENGTH |
| FR-TO       |                           | FROM TO                   |         |                      | FR-TO |                           |                      |
| E-B         | -465 / 0                  | 0.0                       | 0.0     | 0.13 (4)             | 7.81  |                           |                      |
| A-B         | 0 / 45                    | -119.4                    | -119.4  | 0.16 (1)             | 10.00 |                           |                      |
| B-C         | -33 / 0                   | -119.4                    | -119.4  | 0.33 (1)             | 6.25  |                           |                      |
| E-D         | 0 / 0                     | -18.2                     | -18.2   | 0.14 (4)             | 10.00 |                           |                      |

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |    |      |      |     |
|------------|----|------|------|-----|
| TOP CH.    | LL | =    | 34.8 | PSF |
|            | DL | =    | 6.0  | PSF |
| BOT CH.    | LL | =    | 0.0  | PSF |
|            | DL | =    | 7.3  | PSF |
| TOTAL LOAD | =  | 48.1 | PSF  |     |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

**THIS DESIGN COMPLIES WITH:**

- PART 9 OF BCBC 2018, NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

**DESIGN ASSUMPTIONS**

-OVERHANG NOT TO BE ALTERED OR CUT OFF.

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.20")  
 CALCULATED VERT. DEFL.(LL) = L/ 999 (0.00")  
 ALLOWABLE DEFL.(TL)= L/360 (0.20")  
 CALCULATED VERT. DEFL.(TL) = L/ 999 (0.04")

CSI: TC=0.33/0.97 (B-C:1), BC=0.14/0.97 (D-E:4),  
 WB=0.00/0.97 (n/a:0), SSI=0.20/1.00 (B-C:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
 COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT.

**NAIL VALUES**

| PLATE | GRIP(DRY) (PSI) | SHEAR (PLI) | SECTION (PLI)      |
|-------|-----------------|-------------|--------------------|
|       | MAX             | MIN         | MAX MIN            |
| MT20  | 650             | 371         | 1747 788 1987 1873 |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.29 (B) (INPUT = 0.90 )  
 JSI METAL= 0.24 (B) (INPUT = 1.00 )

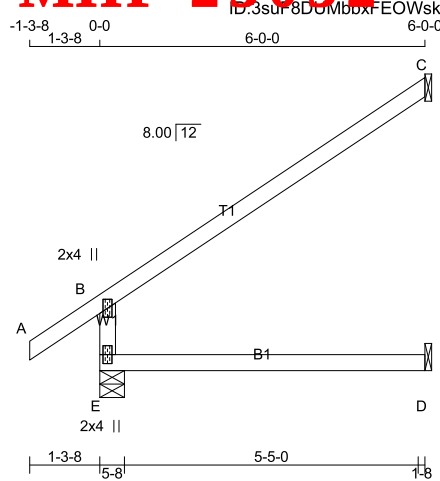


JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.



|            |                                                                                                |          |     |             |          |
|------------|------------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                                  | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMIT PLANS<br>Nov 03 2023<br>PER: <i>C. Mante</i><br>CHIEF BUILDING OFFICIAL | 6        | 1   | TRUSS DESC. |          |



TOTAL WEIGHT = 6 X 18 = 109 lb

| LUMBER            |      |        |      | DESCR. |
|-------------------|------|--------|------|--------|
| N. L. G. A. RULES | SIZE | LUMBER |      |        |
| E - B             | 2x4  | DRY    | No.2 | SPF    |
| A - C             | 2x4  | DRY    | No.2 | SPF    |
| E - D             | 2x4  | DRY    | No.2 | SPF    |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT | TYPE   | PLATES | W   | LEN | Y | X |
|----|--------|--------|-----|-----|---|---|
| B  | TMV+p  | MT20   | 2.0 | 4.0 |   |   |
| E  | BMV1+p | MT20   | 2.0 | 4.0 |   |   |

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQRD BRG |
|----|-------------------------|---------------------------------|-----------|-----------|
| JT | VERT                    | HORZ                            | DOWN      | HORZ      |
| E  | 675                     | 0                               | 675       | 0         |
| C  | 269                     | 0                               | 269       | 0         |
| D  | 46                      | 0                               | 51        | 0         |

SEE MITEK STANDARD DETAIL MSD2015-H FOR CONNECTION TO JOINT(S) C, D

**UNFACTORED REACTIONS**

| JT | 1ST LCASE | MAX./MIN. | COMPONENT REACTIONS |           |       |         |       |
|----|-----------|-----------|---------------------|-----------|-------|---------|-------|
|    | COMBINED  | SNOW      | LIVE                | PERM.LIVE | WIND  | DEAD    | SOIL  |
| E  | 469       | 357 / 0   | 0 / 0               | 0 / 0     | 0 / 0 | 112 / 0 | 0 / 0 |
| C  | 184       | 157 / 0   | 0 / 0               | 0 / 0     | 0 / 0 | 27 / 0  | 0 / 0 |
| D  | 37        | 0 / 0     | 0 / 0               | 0 / 0     | 0 / 0 | 37 / 0  | 0 / 0 |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) E

**BRACING**

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 6.25 FT.  
 MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (4)

| C H O R D S |                           |                           |         | W E B S              |       |                           |                        |
|-------------|---------------------------|---------------------------|---------|----------------------|-------|---------------------------|------------------------|
| MEMB.       | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | LC1 MAX | MAX. UNBRACED LENGTH | MEMB. | MAX. FACTORED FORCE (LBS) | MAX. FACTORED CSI (LC) |
| FR-TO       |                           | FROM TO                   |         |                      | FR-TO |                           |                        |
| E-B         | -612 / 0                  | 0.0                       | 0.0     | 0.13 (4)             | 7.81  |                           |                        |
| A-B         | 0 / 45                    | -119.4                    | -119.4  | 0.16 (1)             | 10.00 |                           |                        |
| B-C         | -50 / 0                   | -119.4                    | -119.4  | 0.73 (1)             | 6.25  |                           |                        |
| E-D         | 0 / 0                     | -18.2                     | -18.2   | 0.14 (4)             | 10.00 |                           |                        |

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |      |      |     |
|------------|------|------|-----|
| TOP CH.    | LL = | 34.8 | PSF |
|            | DL = | 6.0  | PSF |
| BOT CH.    | LL = | 0.0  | PSF |
|            | DL = | 7.3  | PSF |
| TOTAL LOAD | =    | 48.1 | PSF |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

**THIS DESIGN COMPLIES WITH:**

- PART 9 OF BCBC 2018, NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

**DESIGN ASSUMPTIONS**

-OVERHANG NOT TO BE ALTERED OR CUT OFF.

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.20")  
 CALCULATED VERT. DEFL.(LL) = L/ 999 (0.00")  
 ALLOWABLE DEFL.(TL)= L/360 (0.20")  
 CALCULATED VERT. DEFL.(TL) = L/ 999 (0.04")

CSI: TC=0.73/0.97 (B-C:1), BC=0.14/0.97 (D-E:4),  
 WB=0.00/0.97 (n/a:0), SSI=0.29/1.00 (B-C:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
 COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT.

**NAIL VALUES**

| PLATE | GRIP(DRY) (PSI) | SHEAR (PLI) | SECTION (PLI) |
|-------|-----------------|-------------|---------------|
|       | MAX             | MIN         | MAX           |
| MT20  | 650             | 371         | 1747          |
|       | 788             | 1987        | 1873          |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.38 (B) (INPUT = 0.90 )  
 JSI METAL= 0.31 (B) (INPUT = 1.00 )



JULY 14, 2023

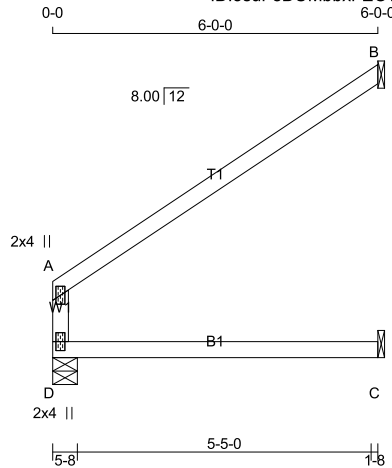
READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.



|            |                                                                                                                                                                             |          |     |             |          |
|------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                                                                                                               | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMITS<br>NOVA<br>J05A<br>Nov 03 2023<br>PER: <br>CHIEF BUILDING OFFICIAL | 7        | 1   | TRUSS DESC. |          |

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ID:3str8DUMbXFEOWsk3nNlIZALn9-wWR9k62elOqk26PdKcaT70s4VHlqmh8PupLT93yyCLV

Scale = 1:42.5



TOTAL WEIGHT = 7 X 16 = 115 lb

| LUMBER            |         |        |        |
|-------------------|---------|--------|--------|
| N. L. G. A. RULES |         |        |        |
| CHORDS            | SIZE    | LUMBER | DESCR. |
| D - A             | 2x4 DRY | No.2   | SPF    |
| A - B             | 2x4 DRY | No.2   | SPF    |
| D - C             | 2x4 DRY | No.2   | SPF    |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT | TYPE   | PLATES | W   | LEN | Y | X |
|----|--------|--------|-----|-----|---|---|
| A  | TMV+p  | MT20   | 2.0 | 4.0 |   |   |
| D  | BMV1+p | MT20   | 2.0 | 4.0 |   |   |

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED       | MAXIMUM FACTORED | INPUT | REQD |
|----|----------------|------------------|-------|------|
|    | GROSS REACTION | GROSS REACTION   | BRG   | BRG  |
| JT | VERT           | HORZ             | DOWN  | HORZ |
| D  | 413            | 0                | 413   | 0    |
| B  | 324            | 0                | 324   | 0    |
| C  | 89             | 0                | 89    | 0    |

SEE MITEK STANDARD DETAIL MSD2015-H FOR CONNECTION TO JOINT(S) B , C

**UNFACTORED REACTIONS**

| JT | 1ST LCASE | MAX./MIN. | COMPONENT REACTIONS |
|----|-----------|-----------|---------------------|
| JT | COMBINED  | SNOW      | LIVE                |
| D  | 289       | 209 / 0   | 0 / 0               |
| B  | 222       | 186 / 0   | 0 / 0               |
| C  | 67        | 23 / 0    | 0 / 0               |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) D

**BRACING**

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 6.25 FT.  
MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (4)

| C H O R D S |               |            |            | W E B S  |        |       |               |
|-------------|---------------|------------|------------|----------|--------|-------|---------------|
| MEMB.       | MAX. FACTORED | FACTORED   | VERT. LOAD | MAX      | MAX.   | MEMB. | MAX. FACTORED |
|             | FORCE         | VERT. LOAD | LC1        | MAX      | MAX.   |       | FORCE         |
|             | (LBS)         | (PLF)      | CSI        | (LC)     | UNBRAC |       | (LBS)         |
| FR-TO       | FROM          | TO         | LENGTH     | FR-TO    |        |       |               |
| D-A         | -393 / 0      | 0.0        | 0.0        | 0.24 (1) | 7.81   |       |               |
| A-B         | -19 / 0       | -119.4     | -119.4     | 0.61 (1) | 6.25   |       |               |
| D-C         | 0 / 0         | -18.2      | -18.2      | 0.30 (1) | 10.00  |       |               |

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |    |      |      |     |
|------------|----|------|------|-----|
| TOP CH.    | LL | =    | 34.8 | PSF |
|            | DL | =    | 6.0  | PSF |
| BOT CH.    | LL | =    | 0.0  | PSF |
|            | DL | =    | 7.3  | PSF |
| TOTAL LOAD | =  | 48.1 | PSF  |     |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

**THIS DESIGN COMPLIES WITH:**

- PART 9 OF BCBC 2018 , NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.20")  
CALCULATED VERT. DEFL.(LL)= L/ 971 (0.07")  
ALLOWABLE DEFL.(TL)= L/360 (0.20")  
CALCULATED VERT. DEFL.(TL)= L/ 463 (0.16")

CSI: TC=0.61/0.97 (A-B:1) , BC=0.30/0.97 (C-D:1) ,  
WB=0.00/0.97 (n/a:0) , SSI=0.25/1.00 (A-B:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .

**NAIL VALUES**

| PLATE | GRIP(DRY) | SHEAR | SECTION |
|-------|-----------|-------|---------|
| (PSI) | (PLI)     | (PLI) | (PLI)   |
| MAX   | MIN       | MAX   | MIN     |
| MT20  | 650       | 371   | 1747    |
|       | 788       | 1987  | 1873    |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.24 (A) (INPUT = 0.90 )  
JSI METAL= 0.20 (A) (INPUT = 1.00 )



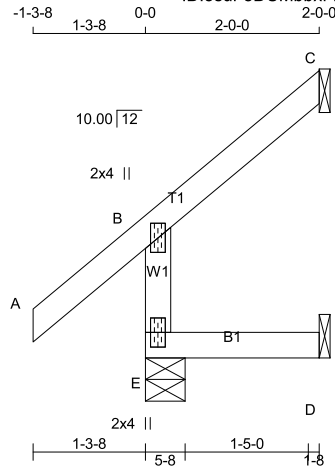
JULY 14, 2023

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|            |                                                                                                    |          |     |             |          |
|------------|----------------------------------------------------------------------------------------------------|----------|-----|-------------|----------|
| JOB NAME   | CORPORATION OF THE TRUSS NAME                                                                      | QUANTITY | PLY | JOB DESC.   | DRWG NO. |
| IM0723-100 | TRUE COPY<br>OF PERMIT PLANS<br>Nov 03 2023<br>PER: <i>C. Matijevic</i><br>CHIEF BUILDING OFFICIAL | 6        | 1   | TRUSS DESC. |          |

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Scale = 1:26.5

TOTAL WEIGHT = 6 X 9 = 53 lb

| LUMBER | N. L. G. A. RULES | CHORDS | SIZE | LUMBER | DESCR. |
|--------|-------------------|--------|------|--------|--------|
| E - B  | 2x4               | DRY    | No.2 | SPF    |        |
| A - C  | 2x4               | DRY    | No.2 | SPF    |        |
| E - D  | 2x4               | DRY    | No.2 | SPF    |        |

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT | TYPE   | PLATES | W   | LEN | Y | X |
|----|--------|--------|-----|-----|---|---|
| B  | TMV+p  | MT20   | 2.0 | 4.0 |   |   |
| E  | BMV1+p | MT20   | 2.0 | 4.0 |   |   |

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQD BRG |
|----|-------------------------|---------------------------------|-----------|----------|
| JT | VERT                    | HORZ                            | DOWN      | HORZ     |
| E  | 334                     | 0                               | 334       | 0        |
| C  | 90                      | 0                               | 90        | 0        |
| D  | 17                      | 0                               | 17        | 0        |

SEE MITEK STANDARD DETAIL MSD2015-H FOR CONNECTION TO JOINT(S) C, D

**UNFACTORED REACTIONS**

| JT | 1ST LCASE COMBINED | SNOW    | LIVE  | PERM.LIVE | WIND  | DEAD   | SOIL  |
|----|--------------------|---------|-------|-----------|-------|--------|-------|
| E  | 230                | 183 / 0 | 0 / 0 | 0 / 0     | 0 / 0 | 47 / 0 | 0 / 0 |
| C  | 62                 | 53 / 0  | 0 / 0 | 0 / 0     | 0 / 0 | 9 / 0  | 0 / 0 |
| D  | 13                 | 0 / 0   | 0 / 0 | 0 / 0     | 0 / 0 | 13 / 0 | 0 / 0 |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) E

**BRACING**

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 6.25 FT.  
 MAX. UNBRACED BOTTOM CHORD LENGTH = 10.00 FT OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

**LOADING**

TOTAL LOAD CASES: (5)

| C H O R D S |                           |                           |                  | W E B S              |       |                           |                      |
|-------------|---------------------------|---------------------------|------------------|----------------------|-------|---------------------------|----------------------|
| MEMB.       | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | MAX LC1 MAX (LC) | MAX. UNBRACED LENGTH | MEMB. | MAX. FACTORED FORCE (LBS) | MAX. UNBRACED LENGTH |
| FR-TO       |                           | FROM TO                   |                  |                      | FR-TO |                           |                      |
| E-B         | -314 / 0                  | 0.0                       | 0.0              | 0.01 (4)             | 7.81  |                           |                      |
| A-B         | 0 / 53                    | -119.4                    | -119.4           | 0.16 (1)             | 10.00 |                           |                      |
| B-C         | -19 / 0                   | -119.4                    | -119.4           | 0.08 (1)             | 6.25  |                           |                      |
| E-D         | 0 / 0                     | -18.2                     | -18.2            | 0.02 (4)             | 10.00 |                           |                      |

CANTILEVER ANALYSIS HAS BEEN CONSIDERED IN THIS DESIGN

PATTERN-LOADING CHECK APPLIED TO THIS TRUSS.

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |      |      |     |
|------------|------|------|-----|
| TOP CH.    | LL = | 34.8 | PSF |
|            | DL = | 6.0  | PSF |
| BOT CH.    | LL = | 0.0  | PSF |
|            | DL = | 7.3  | PSF |
| TOTAL LOAD | =    | 48.1 | PSF |

**SPACING = 24.0 IN. C/C**

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

**THIS DESIGN COMPLIES WITH:**

- PART 9 OF BCBC 2018, NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

**DESIGN ASSUMPTIONS**

-OVERHANG NOT TO BE ALTERED OR CUT OFF.

(55 % OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (0.19")  
 CALCULATED VERT. DEFL.(LL) = L/ 999 (0.00")  
 ALLOWABLE DEFL.(TL)= L/360 (0.19")  
 CALCULATED VERT. DEFL.(TL) = L/ 999 (0.00")

CSI: TC=0.16/0.97 (A-B:1), BC=0.02/0.97 (D-E:4),  
 WB=0.00/0.97 (n/a:0), SSI=0.10/1.00 (A-B:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
 COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT .

**NAIL VALUES**

| PLATE | GRIP(DRY) (PSI) | SHEAR (PLI) | SECTION (PLI) |
|-------|-----------------|-------------|---------------|
|       | MAX             | MIN         | MAX           |
| MT20  | 650             | 371         | 1747          |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

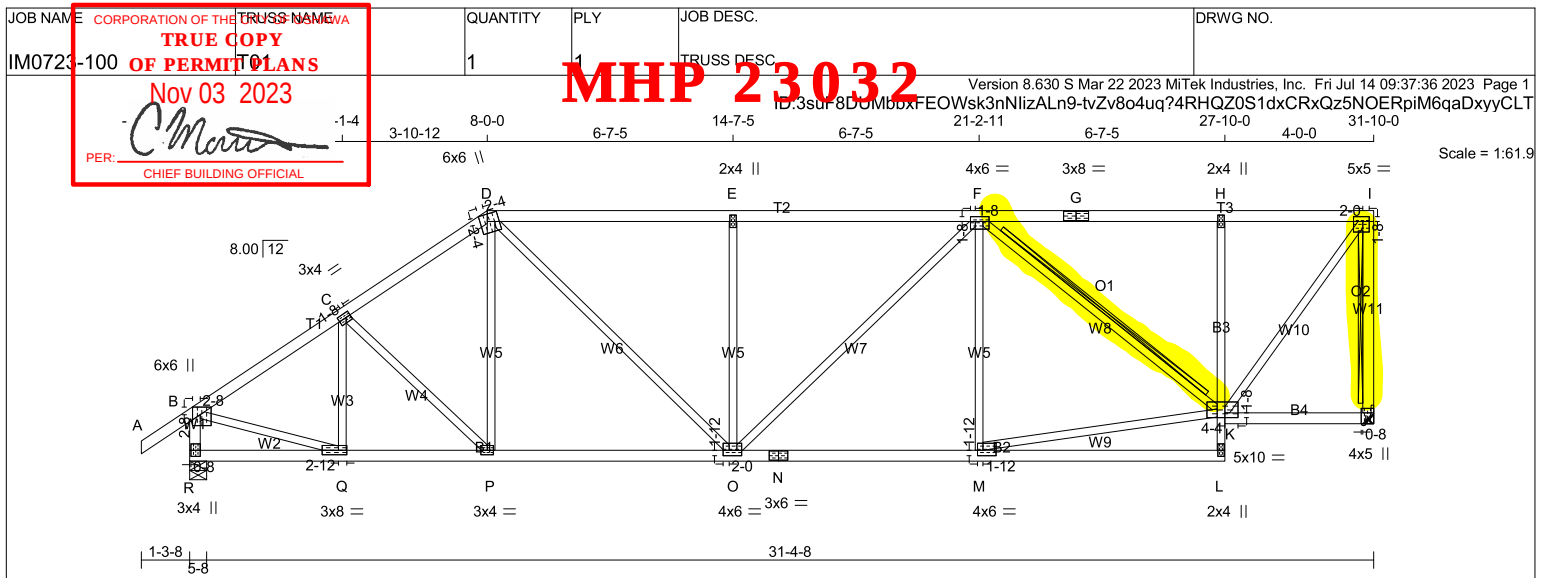
JSI GRIP= 0.22 (B) (INPUT = 0.90 )  
 JSI METAL= 0.17 (B) (INPUT = 1.00 )



JULY 14, 2023

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**LUMBER**

| N. L. G. A. RULES | CHORDS | SIZE | LUMBER     | DESCR. |
|-------------------|--------|------|------------|--------|
| A - D             | 2x4    | DRY  | 2100F 1.8E | SPF    |
| D - G             | 2x4    | DRY  | 2100F 1.8E | SPF    |
| G - I             | 2x4    | DRY  | 2100F 1.8E | SPF    |
| J - I             | 2x4    | DRY  | No.2       | SPF    |
| R - B             | 2x4    | DRY  | 2100F 1.8E | SPF    |
| R - N             | 2x4    | DRY  | No.2       | SPF    |
| N - L             | 2x4    | DRY  | No.2       | SPF    |
| L - H             | 2x3    | DRY  | No.2       | SPF    |
| K - J             | 2x4    | DRY  | No.2       | SPF    |

ALL WEBS 2x3 DRY No.2 SPF  
EXCEPT

DRY: SEASONED LUMBER.

**PLATES (table is in inches)**

| JT TYPE   | PLATES | W   | LEN  | Y    | X    |
|-----------|--------|-----|------|------|------|
| B TMVW+p  | MT20   | 6.0 | 6.0  | Edge | 2.50 |
| C TMVW-t  | MT20   | 3.0 | 4.0  | 1.50 | 1.50 |
| D TTVW+m  | MT20   | 6.0 | 6.0  | 2.25 | 2.25 |
| E TMV+w   | MT20   | 2.0 | 4.0  |      |      |
| F TMVW-t  | MT20   | 4.0 | 6.0  | 1.50 | 1.50 |
| G TS-t    | MT20   | 3.0 | 8.0  |      |      |
| H TMV+p   | MT20   | 2.0 | 4.0  |      |      |
| I TMV-t   | MT20   | 5.0 | 5.0  | 1.50 | 2.00 |
| J BMV1+t  | MT20   | 4.0 | 5.0  | Edge | 0.50 |
| K BVWVW-t | MT20   | 5.0 | 10.0 | 1.50 | 4.25 |
| L BMV+p   | MT20   | 2.0 | 4.0  |      |      |
| M BMVW-t  | MT20   | 4.0 | 6.0  | 1.75 | 1.75 |
| N BS-t    | MT20   | 3.0 | 6.0  |      |      |
| O BMVW-t  | MT20   | 4.0 | 6.0  | 1.75 | 2.00 |
| P BMVW-t  | MT20   | 3.0 | 4.0  |      |      |
| Q BMVW-t  | MT20   | 3.0 | 8.0  | 1.50 | 2.75 |
| R BMV1+p  | MT20   | 3.0 | 4.0  | 2.00 | 0.50 |

Edge - INDICATES REFERENCE CORNER OF PLATE TOUCHES EDGE OF CHORD.

**DIMENSIONS, SUPPORTS AND LOADINGS SPECIFIED BY FABRICATOR TO BE VERIFIED BY BUILDING DESIGNER****BEARINGS**

|    | FACTORED GROSS REACTION | MAXIMUM FACTORED GROSS REACTION | INPUT BRG | REQRD BRG |
|----|-------------------------|---------------------------------|-----------|-----------|
| JT | VERT                    | HORZ                            | DOWN      | HORZ      |
| J  | 2191                    | 0                               | 2191      | 0         |
| R  | 2355                    | 0                               | 2355      | 0         |

A SUITABLE HANGER/MECHANICAL CONNECTION IS REQUIRED AT JOINT J. MINIMUM BEARING LENGTH AT JOINT J = 3-8.

**UNFACTORED REACTIONS**

| JT | 1ST LCASE COMBINED | MAX./MIN. SNOW | MIN. COMPONENT LIVE | PERM. LIVE | WIND  | DEAD    | SOIL  |
|----|--------------------|----------------|---------------------|------------|-------|---------|-------|
| J  | 1531               | 1108 / 0       | 0 / 0               | 0 / 0      | 0 / 0 | 423 / 0 | 0 / 0 |
| R  | 1643               | 1204 / 0       | 0 / 0               | 0 / 0      | 0 / 0 | 440 / 0 | 0 / 0 |

BEARING MATERIAL TO BE SPF NO.2 OR BETTER AT JOINT(S) R

**BRACING**

TOP CHORD TO BE SHEATHED OR MAX. PURLIN SPACING = 4.28 FT.  
MAX. UNBRACED BOTTOM CHORD LENGTH = 7.68 FT. OR RIGID CEILING DIRECTLY APPLIED.

ALL PITCH BREAKS AND PERIMETER CORNER JOINTS MUST BE Laterally RESTRAINED.

2x4 DRY SPF No.2 T-BRACE AT I-J, F-K

FASTEN T AND I-BRACES TO NARROW EDGE OF WEB WITH ONE ROW PER PLY OF 3" COMMON WIRE NAILS @ 6" O.C. WITH 3" MINIMUM END DISTANCE. BRACE MUST COVER 90% OF WEB LENGTH.

END VERTICAL(S) MUST BE SHEATHED OR HAVE BRACES AS INDICATED IN THE MAX. UNBRACED LENGTH COLUMN OF THE TABLE BELOW

**LOADING**

TOTAL LOAD CASES: (4)

| C H O R D S |                           |                           |                           | W E B S |                           |                           |  |
|-------------|---------------------------|---------------------------|---------------------------|---------|---------------------------|---------------------------|--|
| MEMB.       | MAX. FACTORED FORCE (LBS) | FACTORED VERT. LOAD (PLF) | MAX. UNBRACED LENGTH (LC) | MEMB.   | MAX. FACTORED FORCE (LBS) | MAX. UNBRACED LENGTH (LC) |  |
| FR-TO       |                           | FROM TO                   |                           | FR-TO   |                           |                           |  |
| A-B         | 0 / 45                    | -119.4 -119.4             | 0.10 (1)                  | Q-C     | -493 / 0                  | 0.13 (1)                  |  |
| B-C         | -2506 / 0                 | -119.4 -119.4             | 0.24 (1)                  | C-P     | -84 / 0                   | 0.04 (1)                  |  |
| C-D         | -2497 / 0                 | -119.4 -119.4             | 0.23 (1)                  | P-D     | 0 / 167                   | 0.04 (4)                  |  |
| D-E         | -2778 / 0                 | -119.4 -119.4             | 0.61 (1)                  | D-O     | 0 / 1015                  | 0.23 (1)                  |  |
| E-F         | -2779 / 0                 | -119.4 -119.4             | 0.61 (1)                  | O-E     | -880 / 0                  | 0.67 (1)                  |  |
| F-G         | -1497 / 0                 | -119.4 -119.4             | 0.42 (1)                  | O-F     | 0 / 415                   | 0.09 (1)                  |  |
| G-H         | -1497 / 0                 | -119.4 -119.4             | 0.42 (1)                  | M-F     | -244 / 48                 | 0.18 (1)                  |  |
| H-I         | -1501 / 0                 | -119.4 -119.4             | 0.32 (1)                  | M-K     | 0 / 2485                  | 0.56 (1)                  |  |
| J-I         | -2154 / 0                 | 0.0 0.0                   | 0.40 (1)                  | F-K     | -1284 / 0                 | 0.69 (1)                  |  |
| R-B         | -2318 / 0                 | 0.0 0.0                   | 0.14 (1)                  | K-I     | 0 / 2494                  | 0.56 (1)                  |  |
|             |                           |                           |                           | B-Q     | 0 / 2181                  | 0.49 (1)                  |  |
| R-Q         | 0 / 0                     | -18.2 -18.2               | 0.07 (4)                  |         |                           |                           |  |
| Q-P         | 0 / 2109                  | -18.2 -18.2               | 0.41 (1)                  |         |                           |                           |  |
| P-O         | 0 / 2051                  | -18.2 -18.2               | 0.40 (1)                  |         |                           |                           |  |
| O-N         | 0 / 2482                  | -18.2 -18.2               | 0.50 (1)                  |         |                           |                           |  |
| N-M         | 0 / 2482                  | -18.2 -18.2               | 0.50 (1)                  |         |                           |                           |  |
| M-L         | 0 / 25                    | -18.2 -18.2               | 0.19 (4)                  |         |                           |                           |  |
| L-K         | 0 / 53                    | 0.0 0.0                   | 0.08 (1)                  |         |                           |                           |  |
| K-H         | -704 / 0                  | 0.0 0.0                   | 0.55 (1)                  |         |                           |                           |  |
| K-J         | 0 / 0                     | -18.2 -18.2               | 0.09 (4)                  |         |                           |                           |  |

**DESIGN CRITERIA****SPECIFIED LOADS:**

|            |    |      |      |     |
|------------|----|------|------|-----|
| TOP CH.    | LL | =    | 34.8 | PSF |
|            | DL | =    | 6.0  | PSF |
| BOT CH.    | LL | =    | 0.0  | PSF |
|            | DL | =    | 7.3  | PSF |
| TOTAL LOAD | =  | 48.1 | PSF  |     |

**SPACING = 24.0 IN. C/C**

LOADING IN FLAT SECTION BASED ON A SLOPE OF 2.00/12 MINIMUM

THIS TRUSS IS DESIGNED FOR RESIDENTIAL OR SMALL BUILDING REQUIREMENTS OF PART 9, NBCC 2015

THIS DESIGN COMPLIES WITH:

- PART 9 OF BCBC 2018, NBC-2019AE
- PART 9 OF OBC 2012 (2019 AMENDMENT)
- CSA 086-14
- TPIC 2014

(55% OF 48.1 P.S.F. G.S.L. PLUS 8.4 P.S.F. RAIN LOAD) EQUALS 34.8 P.S.F. SPECIFIED ROOF LIVE LOAD

ALLOWABLE DEFL.(LL)= L/360 (1.06")  
CALCULATED VERT. DEFL.(LL)= L/ 999 (0.13")  
ALLOWABLE DEFL.(TL)= L/360 (1.06")  
CALCULATED VERT. DEFL.(TL)= L/ 999 (0.23")

CSI: TC=0.61/0.97 (E-F:1), BC=0.55/0.97 (H-K:1), WB=0.69/0.97 (F-K:1), SS=0.37/1.00 (D-E:1)

DOL LUMBER=1.00 NAIL=1.00 LS BEND=1.10  
COMP=1.10 SHEAR=1.10 TENS= 1.10

COMPANION LIVE LOAD FACTOR = 1.00

TRUSS PLATE MANUFACTURER IS NOT RESPONSIBLE FOR QUALITY CONTROL IN THE TRUSS MANUFACTURING PLANT.

**NAIL VALUES**

| PLATE | GRIP(DRY) | SHEAR (PSI) | SECTION (PLI) |
|-------|-----------|-------------|---------------|
|       | MAX       | MIN         | MAX           |
| MT20  | 650       | 371         | 1747          |
|       | 788       | 1987        | 1873          |

PLATE PLACEMENT TOL. = 0.250 inches

PLATE ROTATION TOL. = 5.0 Deg.

JSI GRIP= 0.88 (I) (INPUT = 0.90)  
JSI METAL= 0.72 (K) (INPUT = 1.00)



JULY 14, 2023

READ ALL NOTES ON THIS PAGE AND ON THE ENGINEERING NOTES: TRUSSES. THE NOTE PAGE IS AN INTEGRAL PART OF THIS DRAWING AS IT CONTAINS SPECIFICATIONS AND CRITERIA USED IN THE DESIGN OF THIS COMPONENT.

